

Insulated Concrete Masonry Below-Grade Walls

A report prepared by

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Preface and acknowledgements

This report is the result of the laboratory study on basements recently conducted by the Pennsylvania Housing Research Center (PHRC). The project addresses the issues related to insulated concrete masonry below-grade walls with reference to structures built mostly in cold and mild climates.

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This report is primarily intended for decision-makers in the building industry as well as others who are interested in the sub-grade aspects of home construction – especially hygro-thermal performance of below-grade walls. Current practice, recent development, and methods of insulating of basement walls are discussed.

The report identifies materials used in basement wall construction according to their physical properties and not commercial names.

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1. Introduction

Basement construction and use of basement spaces have changed dramatically over time. Basements were traditionally designed and used as inhabitable spaces but today's market favors the use of basements as living areas. This represents significant changes in expectations of the space performance, which are expected to provide the same level of comfort and environment as the above-grade structure. Basements represent extremely challenging environments where issues of temperature, relative humidity, and water intrusion must be addressed in a complete system that can function over time.

1.1 Background

A large number of moisture-related building problems have occurred during the last few years, with adverse effects on health, building costs, and confidence.

In the United States basement wall insulation started to be implemented in the 1960's due to the market demand and subsequent energy crisis of the 70's. The energy codes require insulation of the below-grade construction designated as conditioned space. From the past research, it is evident that locating the insulation layer on the exterior surface of the wall offers thermal and other advantages. However, there are also some serious practical disadvantages to an exterior location. The two main disadvantages are that the insulation is exposed and vulnerable to damage both during construction (e.g., equipment, people, etc.) and in-service (e.g., people, equipment, animals, termites, etc.)

Significant numbers of below-grade walls, especially in residential buildings, are constructed with concrete masonry units (CMU) with a nominal thickness of 8 in. The CMU units and mortar used in wall construction are moisture permeable and allow penetration of the wall by moisture in liquid or gaseous form. The processes of water penetration, absorption, storage, accumulation, and drying for CMU wall construction are complex and are not fully understood.

The significant drawbacks to below-grade wall research are the experimental difficulty of modeling the soil including the amount of soil, the soil thermal properties (both short and long terms), moisture effects (amount, movement, etc.), and scale. The fact that climate, ground, and groundwater conditions present a large number of undefined variables is another drawback.

Most recently performance guidelines for basements in cold climates were published in Canada [1-5]. The guidelines address exterior and interior insulations for most common walls (cast-in-place concrete, CMU, and permanent wood foundation (PWS)). While the Canadian work shows the effectiveness of the exterior insulation, it does it only for cast-in-place concrete walls and does not give a direct comparison between exterior and interior insulation in the same test. In addition, the tests conducted by Canadians were performed in-situ, therefore, specific "on site" impacts occurred. Concrete masonry units (CMU) are significantly different from the cast-in-place concrete foundations, in that it does not contain large quantities of water after construction.

The cavity in the CMU adds additional parameter that needs to be considered. Therefore, the results from the cast-in-place basement walls are not valid for CMU walls.

In addition, soil represents a specific heat and mass transfer phenomenon. Studies on soil mass under slab and around below-grade structures showed that the soil is warm and moist enough to cause a water vapor flow from the moist base soil toward the relatively dry indoor air [1]. Ground (soil) properties and heat transfer through ground can also account for up to 40% of the heat loss.

The behavior of the above-grade portion of the wall is different from the below-grade portion. Although these two parts of the wall are connected, each structure faces different boundary conditions such as various thermal lags, forces which induce moisture intrusion, physical properties of walls, condition of the surroundings, etc. As a result, the below-grade envelopes are subjected to higher structural, water, and moisture loads than above-grade portions. This often represents challenging issues for the whole below-grade structure and materials participating in the system.

1.2 Objective

The experimental work described in this report focused on the development and documentation of a better understanding of the hygro-thermal performance of wall systems below grade.

Specifically, the following objectives were to be accomplished:

1. Monitoring and development of effective methods of insulating basement walls in cold climates with respect to moisture intrusion.
2. Monitoring and development of effective methods of insulating basement walls in mild climates with respect to moisture intrusion.
3. Monitoring of absorption and mass movement through the CMU components with respect to the whole basement system's performance

1.3 Scope

The project focuses on the evaluation of various insulation strategies applicable to below-grade CMU wall systems. Final conclusions in the project are stated, based on conducted experimental measurements and available and related literature.

1.3.1 Climate conditions

Two steady state climate conditions were simulated: cold climate representing 5 °C (41 °F), and mild climate representing 20 °C (68 °F). The test results are applicable to structures located in similar climates. The boundary conditions were fully controlled during the experiments.

1.3.2 Damp-proofing

The experimental design included two fundamentally different conditions: (1) walls without damp-proofing, and (2) walls with damp-proofing.

1.3.3 Soil conditions

Because the site conditions for basement construction can vary, the project identified two soil conditions: (1) clay, and (2) sand. These two materials differ in their physical properties. While sand is representing a well-draining soil (water in the soil around the basement percolates downward and has smaller sorption capability), clay may be practically impervious to water (requires efficient foundation drainage system and has higher sorption capability).

1.3.4 Moisture variations

For each test, different external and internal relative water vapor pressure and temperature conditions (see 1.3.1) were simulated in the climate chamber to study and accommodate different moisture migration variations. Relative humidity (RH) of the exterior varied in the range from 50 % to >95 % and the RH of the interior varied between 30 % and 60 %.

1.4 Report organization

The report is divided into six sections. The description of the experiment is presented first, followed by the description of the boundary conditions, measurement of moisture contents, and finally experimental results, conclusions, and recommendations are discussed.

2. Description of the experiment

The experiments were conducted in the climate chamber at the Building Enclosure Testing Laboratory (BeTL) of the PHRC.

2.1 Experimental program

In total four series of tests were conducted. The focus of the project was the performance of the below-grade wall structures under various hygro-thermal conditions.

2.1.1 Experimental parameters

Nine different wall specimens were constructed, instrumented, and tested simultaneously. Four series of tests (cycles) were conducted under preset steady state conditions to monitor the hygro-thermal behavior of the wall specimens. To better understand the behavioral and quantitative aspects, the test parameters were defined as:

- Membrane variations:
 1. Specimens no damp-proofing layer simulating direct contact of the below-grade wall with the surrounding soil. The parged CMU's were in direct contact with the soil.
 2. Specimens with damp-proofing conforming to the building code requirements.

Table 2-1: Test cycles

| Test cycle number | Soil type | Exterior coating | Design alternatives |
|-------------------|-----------|--------------------|---------------------|
| 1. | Sand | No damp-proofing | 8 |
| 2. | Clay | No damp-proofing | 8 |
| 3. | Sand | With damp-proofing | 4 |
| 4. | Clay | With damp-proofing | 4 |

- Soil variations:
 1. Sand representing well-drained soil.
 2. Clay representing a low permeance soil.

Table 2-1 represents the test matrix. The tests started with cycles without damp-proofing. The bare wall was tested for both soil conditions (sand and clay). Then, the specimens were coated on the exterior surface and the tests were repeated.

2.1.2 Climate parameters

In contrast to in-situ measurements, the lab experiments conducted in the climate chamber ensured desired steady state conditions. Such uniform conditions permitted comparing and objectively evaluating the hygro-thermal behavior within each test cycle for different designs.

Table 2-2 summarizes the temperature and relative humidity settings for each experiment during the first and second test run. 8 different designs were studied as shown in the Table 2-1.

Table 2-2: Tested designs during the first and second test runs

| Design | Temperature | | Relative Humidity | | Materials moisture gain |
|--------|-------------------------|--------------------------|--------------------------|--------------------------|-------------------------|
| | Interior T _I | *Exterior T _E | Interior RH _I | Exterior RH _E | |
| | °C, (°F) | °C, (°F) | (%) | (%) | |
| Alt 1 | 20 (68) | 5 (41) | 30 | 70 | Sorption |
| Alt 2 | 20 (68) | 5 (41) | 60 | 70 | Sorption |
| Alt 3 | 20 (68) | 5 (41) | 60 | >95 | Sorption |
| Alt 4 | 20 (68) | 5 (41) | 30 | >95 | Desorption |
| Alt 5 | 20 (68) | 20 (68) | 30 | 50 | Sorption |
| Alt 6 | 20 (68) | 20 (68) | 60 | 50 | Sorption |
| Alt 7 | 20 (68) | 20 (68) | 60 | >95 | Sorption |
| Alt 8 | 20 (68) | 20 (68) | 30 | >95 | Desorption |

* Exterior air temperature was set to 3 °C to ensure a soil temperature of around 5 °C, which represents cold climate soil condition.

Table 2-3 summarizes the temperature and relative humidity settings for each design alternative during the third and fourth test runs. Because no significant differences between test runs with various exterior relative humidity were observed, the number of settings in the last two runs was

reduced to represent the most significant conditions.

Table 2-3: Tested designs during the third and fourth test runs

| Design | Temperature | | Relative Humidity | | Materials moisture gain |
|--------|-------------------------|--------------------------|--------------------------|--------------------------|-------------------------|
| | Interior T _I | *Exterior T _E | Interior RH _I | Exterior RH _E | |
| | °C, (°F) | °C, (°F) | (%) | (%) | |
| Alt 1 | 20 (68) | 5 (41) | 30 | >95 | Sorption |
| Alt 2 | 20 (68) | 5 (41) | 60 | >95 | Sorption |
| Alt 3 | 20 (68) | 20 (68) | 60 | >95 | Sorption |
| Alt 4 | 20 (68) | 20 (68) | 30 | >95 | Desorption |

* Exterior air temperature was set to 3 °C to ensure a soil temperature of around 5 °C, which represents cold climate soil condition.

Figure 2-1 shows the mean annual earth temperature. The soil temperature is relatively constant, and corresponds roughly to the water temperature measured in groundwater wells 30 to 50 feet deep.

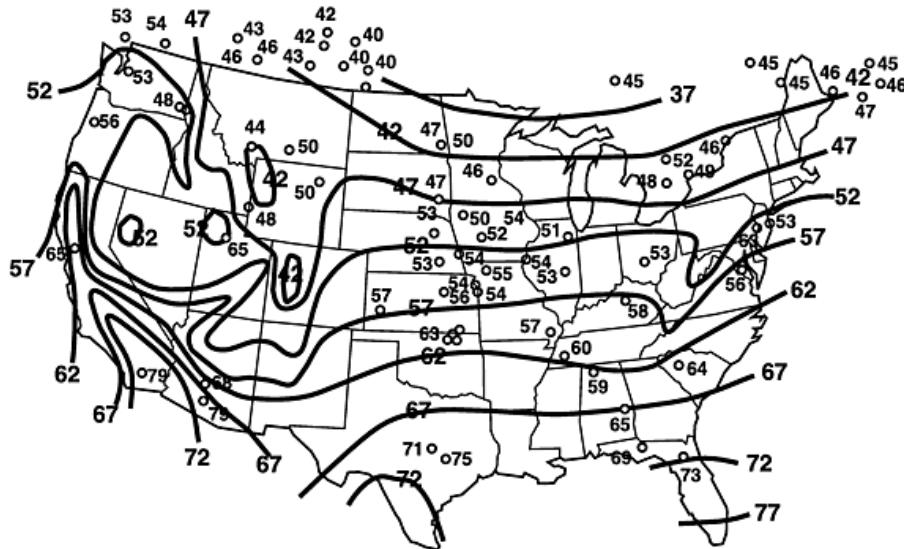


Figure 2-1: Mean annual earth temperature at individual stations, superimposed on well-water temperature contours (°F) [Virginia Department of Mines, Minerals, and Energy]

Since backfill height of foundations can vary, the temperature profiles of the soil surrounding the

basement wall will also vary. A temperature of 5 °C (41 °F) represents the northern (cold) climate while the southern mild climate can be simulated by a temperature of 20 °C (68 °F).

2.2 Test setup

2.2.1 Climate chamber test facility

The climate chamber test facility was designed and built in BeTL at Penn State. The climate chamber test facility consists of:

- *The structure.* The dimensions of the insulated climate chamber are 4.9m x 3m x 2.6m (16 x 10 x 9 ft) (length x width x height). The chamber is finished with PVC on both the interior and exterior. This encapsulated form system is filled with foam insulation to ensure high R-value. Nine 1.1m x 0.7m (3.6 x 2.3 ft) test specimens can be simultaneously tested in the chamber.
- *A cooling system for the climate side.* The cooling system consists of two sub-systems: a freezer and a cooler. Each sub-system has a hot-air-bypass valve controlled by the computer to adjust the air temperature in the climate chamber. In case of computer failure, the system is equipped with its own thermostat for each sub-system.
- *A humidifier for the climate side.* The humidifier is a two-way (on/off) system controlled by the computer to produce small water droplets and thus provide moisture to the climate chamber.
- *A lighting system for solar radiation (used to dry the soil).* Ten lamps for each test panel are mounted on a steel rack system to provide evenly distributed radiation energy. The output power of the lights can be adjusted by the computer. A short dry-up cycle program (warm/evaporate-cool/dehumidify) was written to remove the residual water.
- *Two portable humidifiers.* One for the room side and one for the climate side to support the permanent humidifier to attain relative humidity levels close to saturation.
- *A baseboard heater for the room side.*
- *A portable radiant heater* for the climate side to balance temperature swings.

The climate chamber test facility is able to take the input climate-condition profile and control the temperature, relative humidity, and solar radiation when needed. Examples of the climate-condition control profile and the control actually achieved can be found in Section 3.1. Figure 2-2 shows an overall view of the climate chamber test facility.



Figure Error! Style not defined.-2: Climate chamber test facility

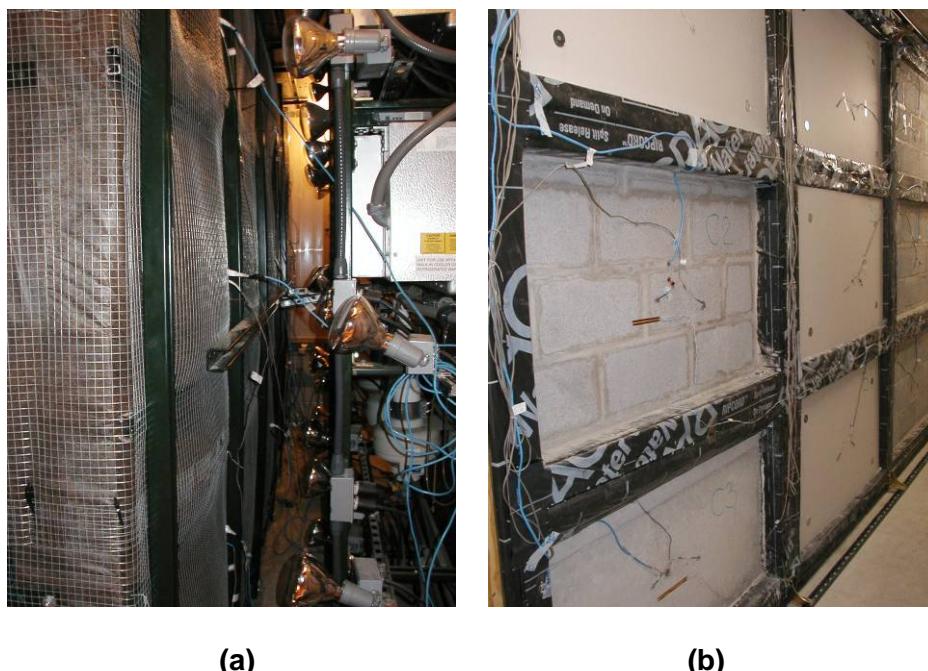


Figure 2-3: Inside view of the climate chamber test facility; (a) climate side, (b) room side

2.2.2 Wall test specimens and instrumentation

Nine different below-grade wall specimens were constructed, instrumented and installed in the climate chamber. The wall support of eight specimens was built from 8" thick CMU's with two cores while one segment was made from concrete. The wall specimens' construction followed the building code requirements [1]. Seven specimens were insulated: three had exterior insulation and the other four had interior insulation. The two remaining specimens were plain CMU and concrete walls. All segments were parged. The walls with exterior insulation were not finished from the interior to simulate unfinished basement and the walls with interior insulation had 3/8" (9.5 mm) drywall applied. The drywall was unfinished.

To compare various wall systems' hygro-thermal behavior, different insulation materials were introduced: (1) *extruded polystyrene*, (2) *polyisocyanurate*, and (3) *glass fiber semi-rigid board*. These insulations were applied on six specimens. The seventh specimen had expanded polystyrene insulation applied from the interior. Each of the insulation was at least 2" (50.8 mm) thick to satisfy the building code energy conservation requirement. Because of very similar physical properties of sprayed polyurethane and polyisocyanurate insulations, the polyisocyanurate boards without foil-facing were used.

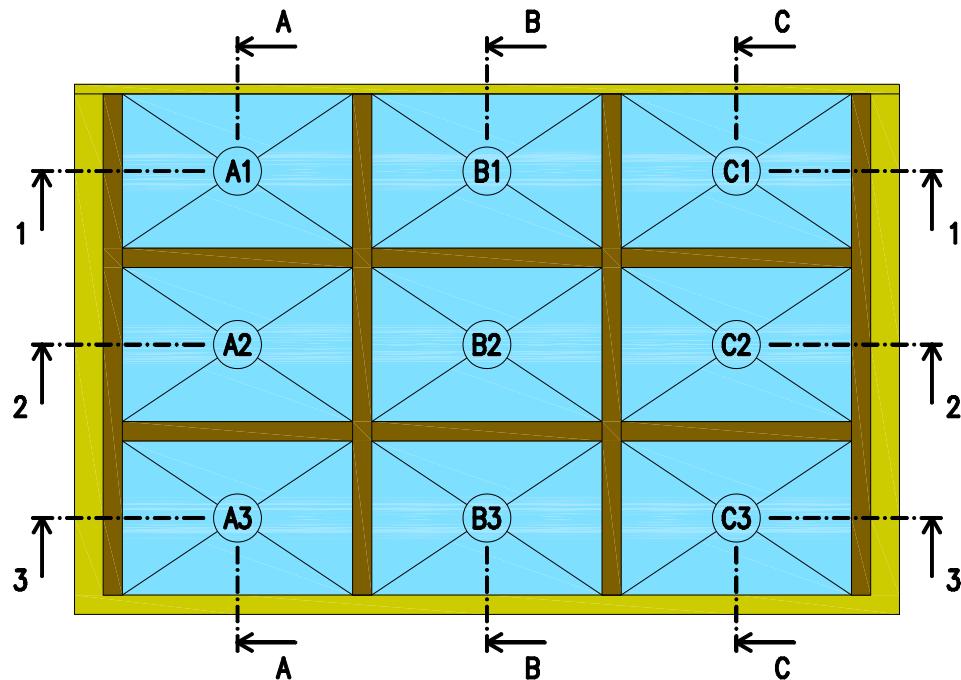


Figure 2-4: Schematic of specimens in the climate chamber

Figure 2-4 shows the configuration of specimens in the climate chamber. Specimens in section A are insulated from the exterior, specimens in section B and C1 have interior insulation applied. The remaining specimens C2 and C3 have no insulation. Table 2-4 summarizes the layer configuration of the test specimens in detail.

Table 2-4: Configuration of the tests specimens

| Specimen | Layer | Thickness (inch) (mm) | | Comments | Cross section |
|----------|------------------------------|--------------------------|-------|---------------------|---------------|
| A1 | Soil | 10 | 254.0 | | |
| | Extruded Polystyrene (XPS) | 2 | 50.8 | | |
| | * Damp-proofing (paint coat) | - | - | Exterior insulation | |
| | Parging (Stucco) | 3/8 | 9.5 | | |
| | Concrete Masonry Unit (CMU) | 8 | 203.2 | | |
| | Gypsum Board (Drywall) | 3/8 | 9.5 | | |
| A2 | Soil | 10 | 254.0 | | |
| | Polyisocyanurate | 2 | 50.8 | | |
| | * Damp-proofing (paint coat) | - | - | Exterior insulation | |
| | Parging (Stucco) | 3/8 | 9.5 | | |
| | Concrete Masonry Unit (CMU) | 8 | 203.2 | | |
| | Gypsum Board (Drywall) | 3/8 | 9.5 | | |
| A3 | Soil | 10 | 254.0 | | |
| | Glass Fiber | 2 1/4 | 57.2 | | |
| | * Damp-proofing (paint coat) | - | - | Exterior insulation | |
| | Parging (Stucco) | 3/8 | 9.5 | | |
| | Concrete Masonry Unit (CMU) | 8 | 203.2 | | |
| | Gypsum Board (Drywall) | 3/8 | 9.5 | | |

* Damp-proofing is applied only in the third and fourth test cycles

Table 2-4: Configuration of the tests specimens (continued)

| Specimen | Layer | Thickness (inch) (mm) | | Comments | Wall specimen's fragment |
|-----------|------------------------------|--------------------------|-------|---------------------|--------------------------|
| B1 | Soil | 10 | 254.0 | | |
| | * Damp-proofing (paint coat) | - | - | | |
| | Parging (Stucco) | 3/8 | 9.5 | Interior insulation | |
| | Concrete Masonry Unit (CMU) | 8 | 203.2 | | |
| | Extruded Polystyrene (XPS) | 2 | 50.8 | | |
| B2 | Gypsum Board (Drywall) | 3/8 | 9.5 | | |
| | Soil | 10 | 254.0 | | |
| | * Damp-proofing (paint coat) | - | - | | |
| | Parging (Stucco) | 3/8 | 9.5 | Interior insulation | |
| | Concrete Masonry Unit (CMU) | 8 | 203.2 | | |
| B3 | Polyisocyanurate | 2 | 50.8 | | |
| | Gypsum Board (Drywall) | 3/8 | 9.5 | | |
| | Soil | 10 | 254.0 | | |
| | * Damp-proofing (paint coat) | - | - | | |
| | Parging (Stucco) | 3/8 | 9.5 | Interior insulation | |
| | Concrete Masonry Unit (CMU) | 8 | 203.2 | | |
| | Glass Fiber | 2 1/4 | 57.2 | | |
| | Gypsum Board (Drywall) | 3/8 | 9.5 | | |

* Damp-proofing is applied only in the third and fourth test cycles

Table 2-4: Configuration of the tests specimens (continued)

| Specimen | Layer | Thickness (inch) (mm) | | Comments | Wall specimen's fragment |
|----------|------------------------------|--------------------------|-------|-----------------------|--------------------------|
| C1 | Soil | 10 | 254.0 | | |
| | * Damp-proofing (paint coat) | - | - | | |
| | Parging (Stucco) | 3/8 | 9.5 | Interior insulation | |
| | Concrete Masonry Unit (CMU) | 8 | 203.2 | | |
| | Expanded Polystyrene (EPS) | 2 | 50.8 | | |
| C2 | Gypsum Board (Drywall) | 3/8 | 9.5 | | |
| | Soil | 10 | 254.0 | | |
| | * Damp-proofing (paint coat) | - | - | | |
| | Parging (Stucco) | 3/8 | 9.5 | Not insulated (plain) | |
| | Concrete Masonry Unit (CMU) | 8 | 203.2 | | |
| C3 | | | | | |
| | Soil | 10 | 254.0 | | |
| | * Damp-proofing (paint coat) | - | - | | |
| | Parging (Stucco) | 3/8 | 9.5 | Not insulated (plain) | |
| | Concrete | 8 | 203.2 | | |

* Damp-proofing is applied only in the third and fourth test cycles

The figures shown below document the test wall construction. Frame construction and the use of thermal insulation at specimen boundaries are shown in Figure 2-5. Figure 2-6 shows the hygro protection used to eliminate the lateral moisture movement between specimens.



Figure 2-5: Frame and insulation



Figure 2-6: Moisture barrier



Figure 2-7: Specimens construction



Figure 2-8: Finished test wall

Figure 2-7 shows the CMU placed in the insulated frame. The final test wall construction with all finishes ready for testing is shown in Figure 2-8.

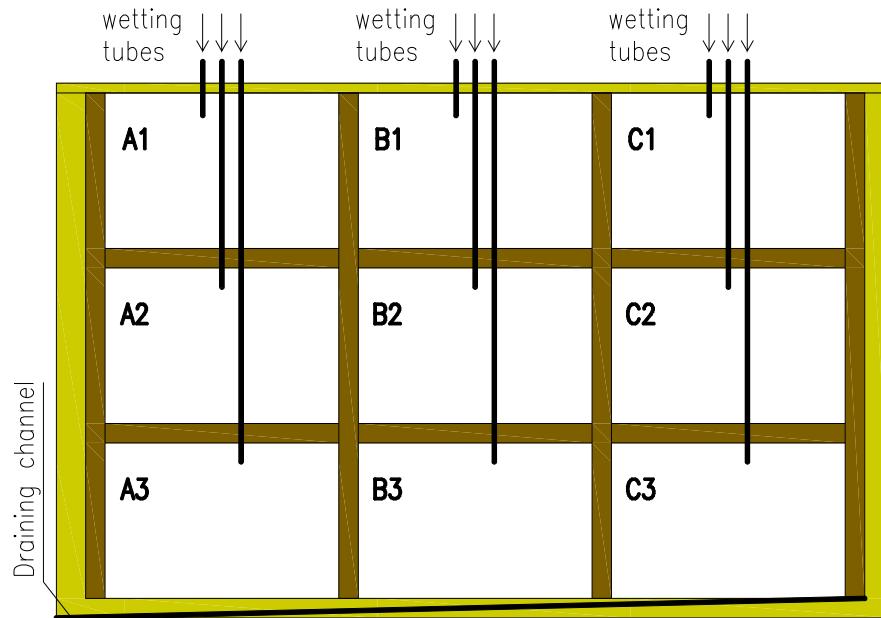
2.2.3 The soil

To simulate the influence of adjacent soil on the hygro-thermal behavior of the basement walls, it was necessary to create a structure that can be easily instrumented with sensors and allow quick soil change. After finishing the wall segments from the exterior (parging and applying thermal insulations to section A), a metal holding frame was constructed. Wire mesh and permeable garden fabric were used to hold the soil in place. The soil was placed into the cage through the opening at the top of the climate chamber. The soil layer was insulated on the boundary from adjacent segments in exactly the same way as the CMU wall.

Draining channel was installed under the soil, to remove the excess water from wetting the soil during the third and fourth test cycle. Known amounts of water were introduced into the soil only at the third and fourth test cycle, and relative humidity of the air was used to control the soil's moisture content during remaining cycles. A tubular wetting system was inserted into the soil, to ensure even water distribution. The moisture contents of soil were measured via taking and evaluating gravimetric soil samples from the top of the soil cage.

Figure 2-9 shows the wetting system installed for the third and fourth test cycles. Known amounts of water were introduced through each tube into the soil to attain saturated conditions.

Figure 2-9: Soil wetting system



The figures below show the soil holding cage construction. Finishing of the exterior side, especially section A, with different types of insulation materials (XPS – at the top, polyisocyanurate and glass fiber – at the bottom) is shown in Figure 2-10.



Figure 2-10: Finishing of the exterior



Figure 2-11: Holding cage construction

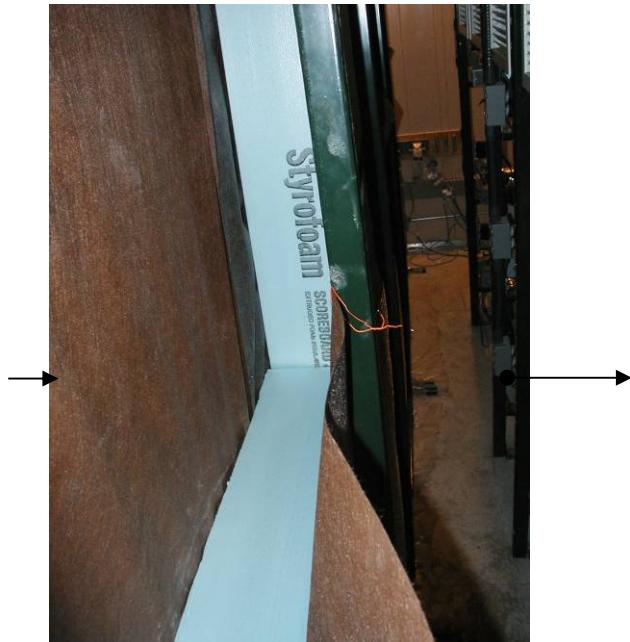


Figure 2-12: Soil insulation / separation

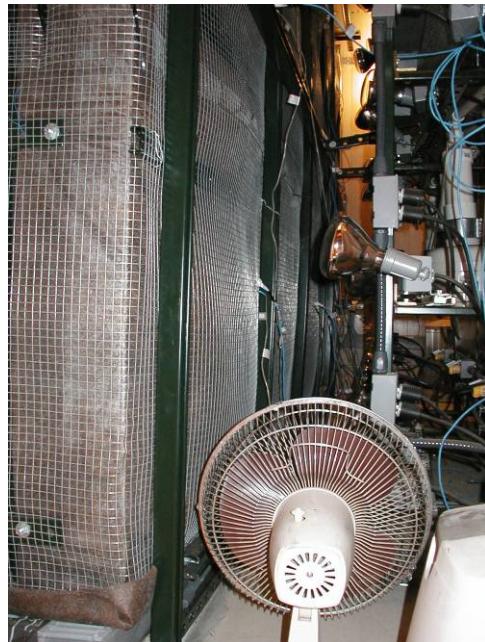


Figure 2-13: Finished soil cage

Figure 2-11 shows the soil holding frame and wire mesh installation. The insulation and separation of soil with XPS boards is shown in Figure 2-12. Figure 2-12 shows the finished soil holding cage.

2.2.4 Construction of the specimens

The construction of the experimental wall specimens consisted of:

1. Construction of the wood frames.
2. Installation of the XPS thermal insulation boards on the frame to separate the boundaries.
3. Wrapping the insulated frame with waterproof self-adhered underlayment.
4. Building the CMU wall segments. Type S mortar was used and the CMU's were not grouted.
5. Construction of concrete form; the concrete was poured into the form; plain concrete was used
6. 9.5mm (3/8 in) white base stucco was applied on the CMU's and concrete specimens
7. Insulation materials were applied to the specimens; thickness of at least 50.8mm (2")
8. The specimens with the interior insulation were finished; drywall 9.5mm (3/8") (unfinished) was fastened through four dowel-joints at each specimen.
9. Soil holding cage was constructed using metal U-type profile and bolted joints; drainage channel was installed to drain the excessive water; parged and exterior insulated test specimens (such as section A) were covered with permeable garden fabric to prevent sensor damage.
10. The garden fabric was stapled and attached to the wire mesh to hold the soil in place.
11. During installing the soil into the cage, insulation and separation of soil was achieved by inserting XPS boards between the test specimens.
12. The wetting system was installed before the third test cycle to achieve saturated soil conditions.

2.2.5 Instrumentation and data acquisition system

Four parameters were measured and recorded during the test: (1) temperature, (2) relative humidity, (3) condensation, and (4) pressure difference. Table 2-5 summarizes the instrumentation used in the experiments.

Of the properties monitored, only temperature, relative humidity, and pressure difference were measured directly. The moisture content of the CMU's was determined indirectly through the equilibrium relative humidity measurements. A relative humidity vs. moisture content curve was developed and the moisture content was calculated. Condensation was detected through a custom built sensor that functioned as a switch. Condensation was not quantified, only the presence or absence of condensation was determined.

Table 2-5: Instrumentation

| Parameter | Location | Sensor Type | Manufacturer & model number | Comments |
|-------------------------------|------------------------------|---|-----------------------------|--|
| Temperature | Soil | Thermistor | Fenwall 192-103LEW-A01 | 10k Ohms at 25 degC see Figure 68 pc. |
| | Exterior side of the wall | | | |
| | ¹ Wall | | | |
| | Drywall | | | |
| | Interior side of the wall | | | |
| | Environment | Relative humidity a temperature transmitter | Vaisala HMW40Y | see Figure 1 pc. |
| Relative Humidity | Room | Relative humidity a temperature transmitter | Vaisala HMP233 | see Figure 1 pc. |
| | Soil | R.H. sensor | Honeywell HIH-3610 | see Figure 32 pc. |
| | ¹ Wall | | | |
| | Environment | Relative humidity a temperature transmitter | Vaisala HMW40Y | 1 pc. |
| Equilibrium Relative Humidity | Room | Relative humidity a temperature transmitter | Vaisala HMP233 | 1 pc. |
| | Inside wall cavity | R.H. sensor | Honeywell HIH-3610 | 18 pc. |
| Condensation | ¹ Wall | Condensation Gages | BeTL | 9 pc. |
| Pressure difference | Environmental / Climate Side | Differential Pressure Transmitter | Omega PX274-30DI | 1 pc. |

¹ location on the wall – beneath the insulation

Figure 2-14 shows the configuration of specimens and the instrumentation setup. A better view of the instrumentation is shown in Figure 2-15.

Figure 2-14: Configuration of the specimens

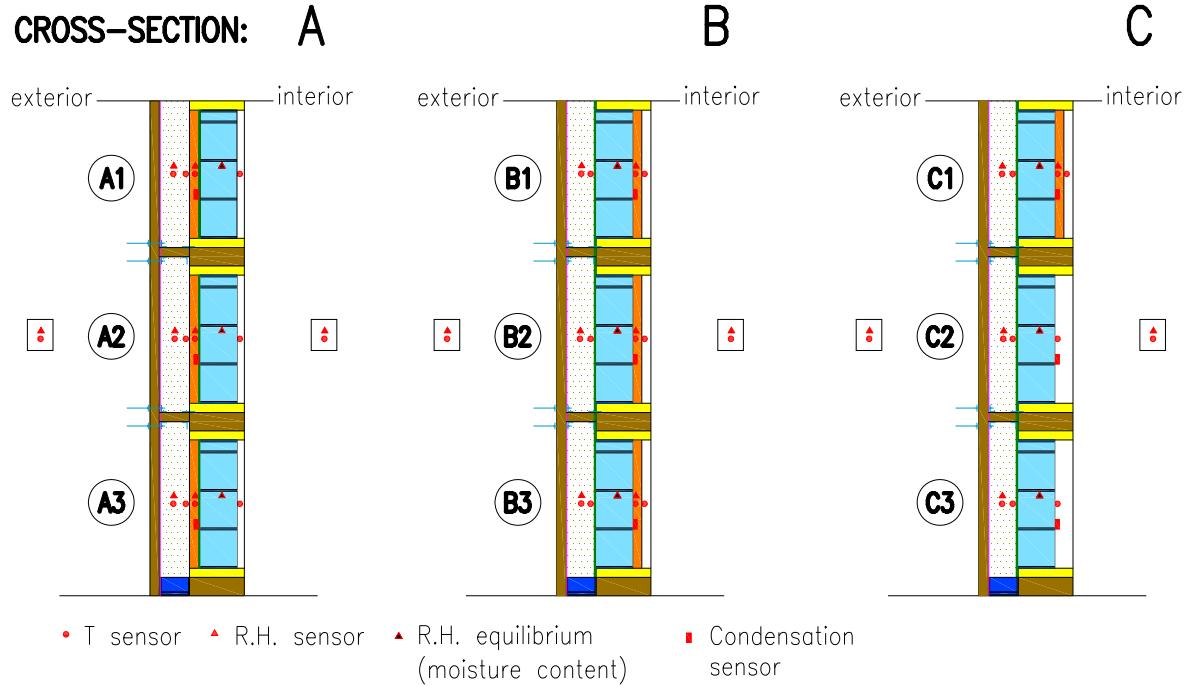
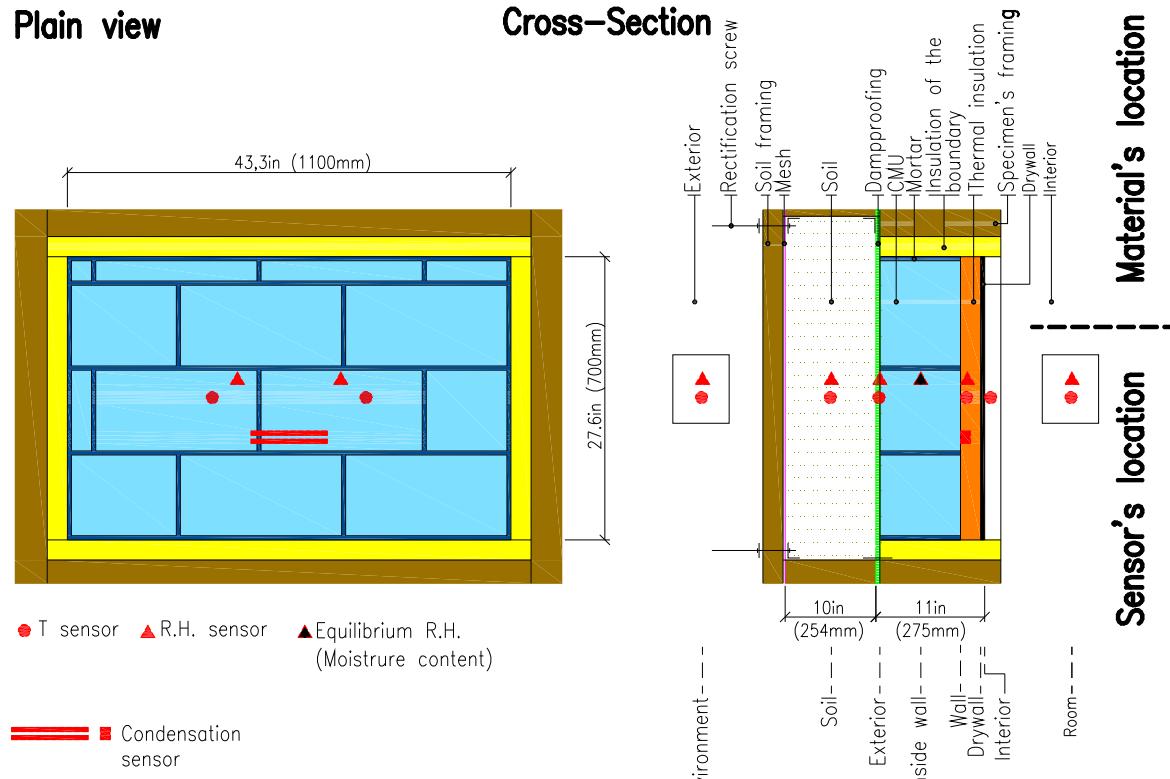


Figure 2-15: Schematic of the test segment and instrumentation



Temperature measurement

Surface and air temperatures were measured with Uni-Curve series interchangeable thermistors. The thermistors did not require individual resistance temperature calibration. The Resistance – Temperature measurement calibration curve is expressed by the following formula:

$$T_i = -0.101(\ln(R_i))^3 + 4.346(\ln(R_i))^2 - 77.18(\ln(R_i)) + 446.05 \quad (\text{°C}) \quad (1)$$

Temperature measurements were conducted on the NI Field Points (A110, A111 – mentioned below) where the first channel was used to measure the current across the fixed resistance ($R_0 = 10\text{k}\Omega$) with a precision of 1%. The applied voltage is:

$$V_s = I_0 / R_0 \quad (\text{V}) \quad (2)$$

The temperature of the remaining channels was calculated via the measured fixed resistance R_0 and the resistance induced by temperature difference R_T .

$$R_i = R_0 + R_T \quad (\Omega) \quad (3)$$

Relative Humidity (or Water Vapor Pressure) measurement

The relative humidity was measured using commercial multi-layer construction capacitance relative humidity sensor. The used RH sensor is a laser trimmed thermoset polymer capacitive sensing element with on-chip integrated signal conditioning. Direct input to a controller (A110 – mentioned below) is done via linear voltage output of the sensor. RH is calculated via linear expression of the voltage output in the form of:

$$\text{RH} = (V_{\text{out}} - \text{zero offset}) / \text{slope} \quad (\%) \quad (4)$$

To prevent sensor damage and erroneous readings caused by water contact, the RH probes were inserted into a perforated plastic tube for measuring RH between the individual layers. Similarly, RH probes inserted into a perforated plastic tube with a larger diameter and wrapped in a permeable garden fabric were used to measure the Equilibrium RH (discussed next) of soil. The tubes were inserted into the soil with a small slope to avoid direct contact of the probe with water.

Equilibrium Relative Humidity (Moisture Content) measurement

As we will discuss in later sections, the moisture storage characteristics of the CMU's and concrete have a significant impact on thermal properties of materials (such as conductivity and heat storage). In order to characterize the disposition of moisture in the CMU and concrete walls, the moisture stored in those layers must be quantified. The most logical way of quantifying the amount of moisture stored in the CMU and concrete layers is the average moisture content. However, no commercially available hardware was found to have this capability. A number of sensors (mostly resistance-based) and moisture meters are available, but lack the necessary sensitivity or are not economical choices for long-term monitoring of moisture content. Therefore, an alternative method is required.

A relative humidity sensor was used to measure the moisture content of the CMU's and concrete. A $\frac{3}{4}$ in (19.05 mm) hole was drilled into the center of CMU and concrete walls and relative humidity sensor was inserted into the cavity to measure the equilibrium relative humidity. The hole around the protruded wiring was sealed with a silicone-based sealant.

To quantify the moisture content of the test wall assemblies it was necessary to develop the RH – Moisture Content curves (sorption and desorption isotherms). Thus, the moisture content was calculated from the established RH-MC isotherms and potential hysteresis was ignored.

Condensation measurement

Two copper conductors, separated by a 1-2 mm gap, were installed on each of the wall surface. A 5V DC excitation was applied across these terminals and the voltage drop was measured. Dry conditions (no condensation) were indicated by a zero reading and condensation was indicated by a positive reading.

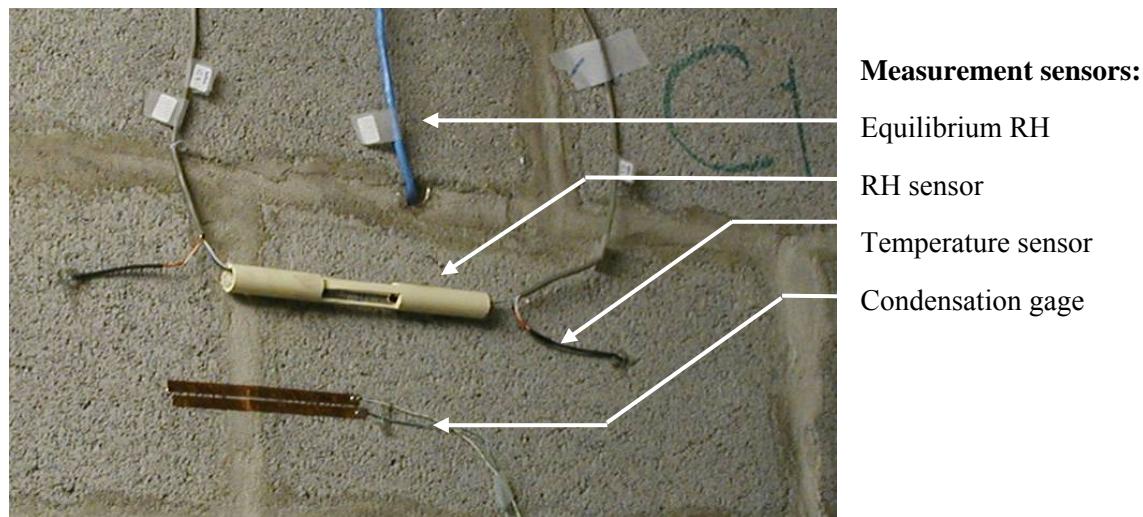


Figure 2-16: Sensors used in the measurement

2.2.6 Instrumentation and data acquisition system

The NI (National Instruments) FieldPoint system and LabVIEW 7.1 were used as the data acquisition hardware and software for the climate chamber tests. The FieldPoint distributed I/O system is a modular data acquisition system for automatic measurement and process control. The modules used in the project were as follows:

FP – 1000/1001

The National Instruments FP-1000/1001 is a network interface module for the FieldPoint I/O system. Each NI FP-1000/1001 connects a node of up to nine FieldPoint I/O modules to an RS-232 or RS-485 network. A FieldPoint network can consist of up to 25 network nodes, for a total

of 225 FieldPoint I/O modules. The NI FP-1000/1001 network module manages communications between the host PC and the I/O modules via a local high-speed bus formed by FieldPoint terminal bases. The network module also provides several diagnostic and auto-configuration features, simplifying installation, use, and maintenance. FieldPoint Explorer and server software are included with RS-232/RS-485 FieldPoint systems. These software tools save the basic configuration information of the system and communicate with the application software.

FP-DO-410

The FP-DO-410 module has eight discrete sourcing output channels individually protected from overload conditions with an electronic resettable fuse. The module is designed to have input-output isolation, HotPnP (plug and play) operation, and onboard diagnostics. The main reason for including FP-DO-410 is to power the input modules.

FP-AO-200/210

The NI FP-AO-200 series consists of versatile analog output modules for the FieldPoint I/O system. The FP-AO-200 is an 8-channel analog output module for 4 to 20 mA and 0 to 20 mA current loops while FP-AO-210 is an 8-channel analog voltage output module (0 to 10 V, up to 10 mA per channel). The modules include open-circuit detection for wiring and sensor troubleshooting and short-circuit protection for wiring errors. Both of them incorporate overranging protection, HotPnP (plug and play) operation, and onboard diagnostics to protect the modules. These modules were used in the test to control the equipment in the climate chamber.

FP-AI-110/111

The NI FP-AI-100 series consists of versatile analog input modules for the FieldPoint I/O system. The FP-AI-110 and FP-AI-111 feature 16-bit, filtered low-noise inputs. The FP-AI-110 is an 8-channel single-ended input module for direct measurement of millivolt, low voltage, or milliamperc signals from a variety of sensors and transmitters while FP-AI-111 is a 16-channel input module for direct measurement of millamp current signals from a variety of sensors and transmitters. Both of them incorporate overranging protection, HotPnP (plug and play) operation, and onboard diagnostics to protect the modules. These modules were used in the test to read the sensor measurements.

Figure 2.17 and Figure 2.18 show the configuration of the FieldPoint system, including the communication with the computer.

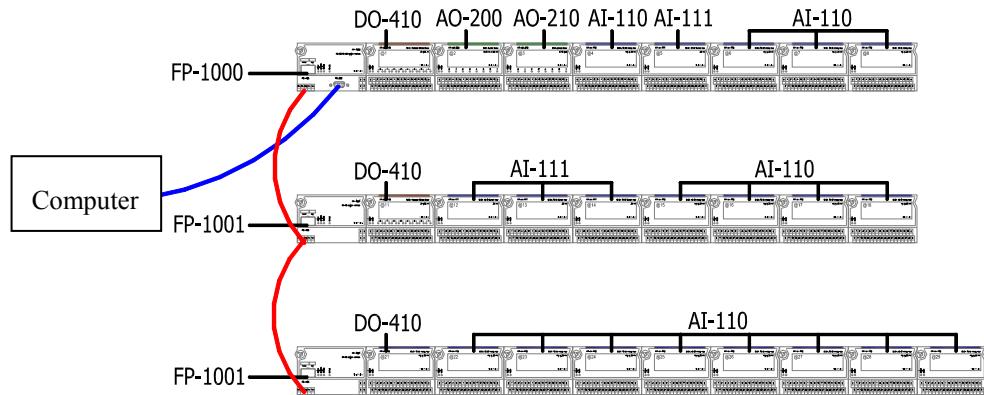


Figure 2-17: Schematic of the data acquisition system

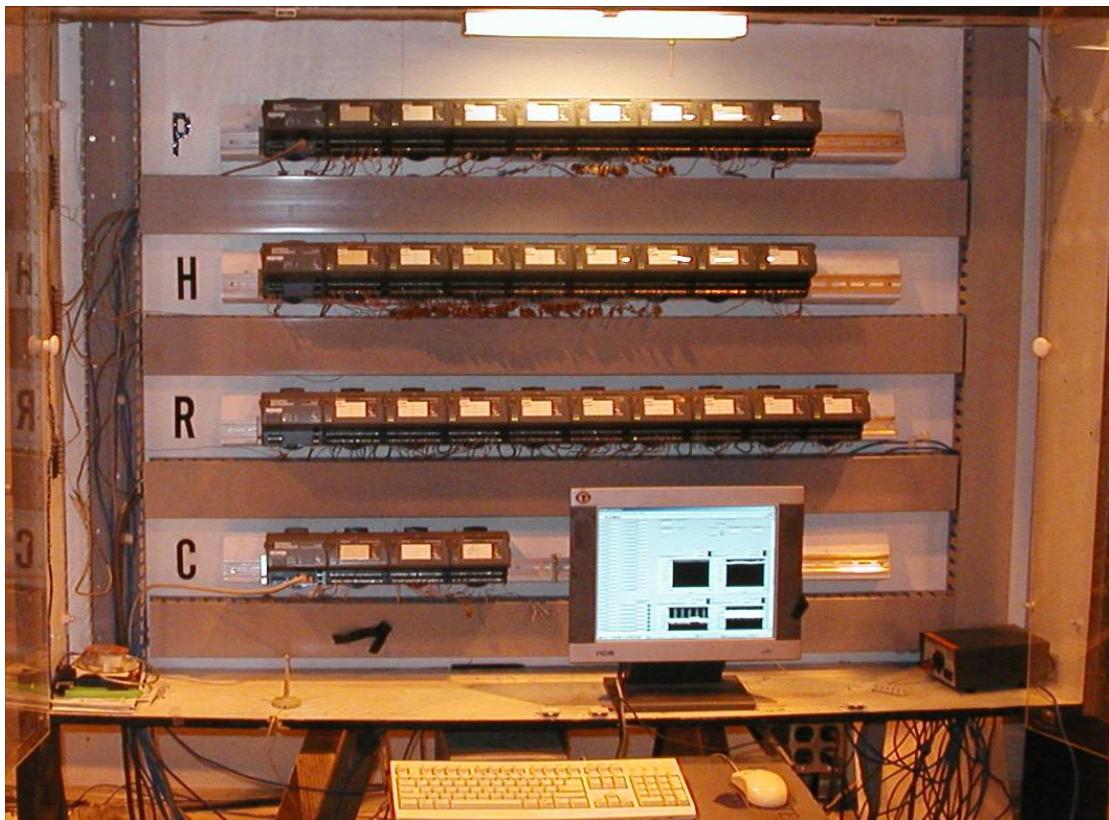


Figure 2-18: Data acquisition system at BeTL

2.3 Testing procedure

The nine wall test specimens were constructed, instrumented, and completely installed prior to the start of testing. The procedure for each test was as follows:

1. Make sure to reach the desired soil condition before the measurement. For the first and second test cycle use the dry-up program to remove water from the soil. For the third and fourth cycle wet the soil to attain saturated soil conditions (add 4 gal. of water to each specimen; check the soil condition by using a gravimetric test)
2. After setting up the specimens turn on the HVAC equipment and set the control parameters according to the proposed settings in Table 2-2 and 2-3. To minimize fluctuations in temperature and RH set the control loop to 1 - 2 min. (60 to 30 time reaction time during an hour)
3. When measuring the cold climate variations hold the ambient air temperature above 3 °C to prevent freezing and to ensure the soil temperature around 5 °C.
4. Allow achieving steady-state conditions and minimize fluctuations, if any.
5. Measure and record the temperature, relative humidity, equilibrium relative humidity, pressure difference, and condensation sensors every 6 minutes until the end of the test (10 measurements during an hour).
6. Evaluate only the latest results, i.e. the last 24 hours of the measurement.

3. Boundary conditions

Steady-state conditions were maintained during the tests. During the experiment the focus was kept on moisture accumulation at the interface of two physically different materials (such as CMU and insulation material).

3.1.1 Boundary conditions on the interior side

The interior temperature was set equally to 20 °C (68 °F) for all tests. The RH was set to either 30 % or 60 %, which represented relatively dry (30%) and humid (60%) conditions. The test setups are shown in Table 2-2 and 2-3 in detail.

3.1.2 Boundary conditions on the exterior side

The exterior boundary conditions were ambient air temperature and relative humidity. The temperature for all four test cycles was either 5 °C (41 °F) representing cold climate or 20 °C (68 °F) representing mild climate. According to the Table 2-2, the RH setup for the first and second cycle included three different values: 50 %, 70 % (for cold climate), and >95 %. Since the first and second test runs did not show any significant influence of the RH difference and the soil in the third and fourth test run was fully saturated, the RH was maintained at a constant level of >95 % (see Table 2-3).

Figure 3-1 shows an example of controlling the interior and exterior boundary conditions.

The boundary conditions were controlled with a precision of ± 1 °C for temperature and ± 5 % for RH. The peak values of exterior temperature were achieved by defrost cycles during the cold climate. Controlling the exterior relative humidity was difficult due to the high RH values (>95 %). The fluctuations of RH depend on the temperature profile and RH sensor delay. In the third and fourth test runs, the relative humidity was reaching lower values because the soil was wetted through the tubular wetting system. The ambient air RH values were slightly lower to avoid excessive moisture absorption through the exterior side of the chiller and freezer.

When the difference between exterior and interior relative humidities was high, additional dehumidification equipment was required to maintain low RH on the interior.

Insulated Concrete Masonry Below-grade Walls

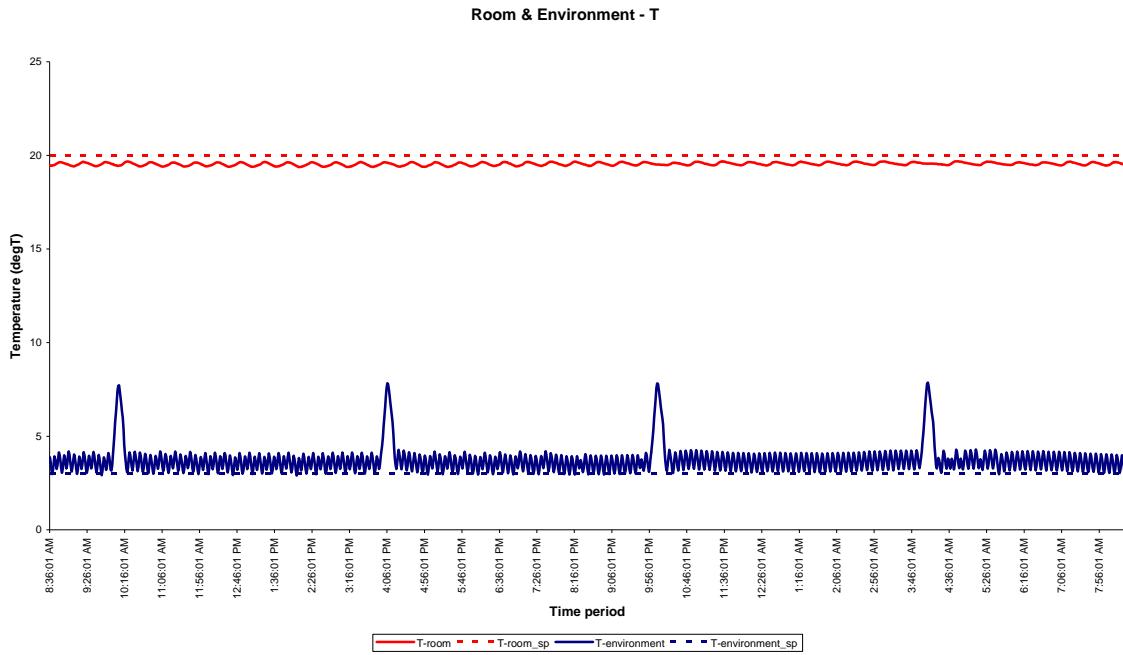


Figure 3-1: Example of temperature control



Figure 3-2: Example of RH control

3.1.3 Material properties

The hygro-thermal properties of materials used in test wall specimens are shown below (Table 3-1). The data from available literature was used to minimize the experimental costs. Ideally, one would like to measure all relevant physical properties in the laboratory to minimize the errors due to inherent material variability.

Table 3-1: Thermal properties of used materials

| Specimen | Layer | Thickness | | Conductivity "k" | Conductance "C" | Thermal Resistance "R" | |
|-----------|-----------------------|-----------|-------|---------------------|-------------------------|---------------------------|---------------------------|
| | | (inch) | (mm) | (W/(m.K)) | (W/(m ² .K)) | (m ² K/W) | (ft ² h°F/Btu) |
| A1 | Extruded Polystyrene | 2 | 50.8 | 0.0289 | 0.57 | 1.758 | 9.987 |
| | * Damp-proofing | 0 | 1.6 | - | - | - | - |
| | Parging | 3/8 | 9.5 | 0.7200 | 75.59 | 0.013 | 0.075 |
| | Concrete Masonry Unit | 8 | 203.2 | - | 2.58 | 0.388 | 2.202 |
| | Gypsum Board | 3/8 | 9.5 | 0.1680 | 17.64 | 0.057 | 0.322 |
| | Total | | | | 2.335 | 13.269 | |
| A2 | Polyisocyanurate | 2 | 50.8 | 0.0222 | 0.44 | 2.288 | 13.002 |
| | * Damp-proofing | 0 | 1.6 | - | - | - | - |
| | Parging | 3/8 | 9.5 | 0.7200 | 75.59 | 0.013 | 0.075 |
| | Concrete Masonry Unit | 8 | 203.2 | - | 2.58 | 0.388 | 2.202 |
| | Gypsum Board | 3/8 | 9.5 | 0.1680 | 17.64 | 0.057 | 0.322 |
| | Total | | | | 2.866 | 16.283 | |
| A3 | Glass Fibre | 2 1/4 | 57.2 | 0.0338 | 0.59 | 1.691 | 9.607 |
| | * Damp-proofing | 0 | 1.6 | - | - | - | - |
| | Parging | 3/8 | 9.5 | 0.7200 | 75.59 | 0.013 | 0.075 |
| | Concrete Masonry Unit | 8 | 203.2 | - | 2.58 | 0.388 | 2.202 |
| | Gypsum Board | 3/8 | 9.5 | 0.1680 | 17.64 | 0.057 | 0.322 |
| | Total | | | | 2.268 | 12.888 | |
| B1 | * Damp-proofing | 0 | 1.6 | - | - | - | - |
| | Parging | 3/8 | 9.5 | 0.7200 | 75.59 | 0.013 | 0.075 |
| | Concrete Masonry Unit | 8 | 203.2 | - | 2.58 | 0.388 | 2.202 |
| | Extruded Polystyrene | 2 | 50.8 | 0.0289 | 0.57 | 1.758 | 9.987 |
| | Gypsum Board | 3/8 | 9.5 | 0.1680 | 17.64 | 0.057 | 0.322 |
| | Total | | | | 2.335 | 13.269 | |

* Damp-proofing is applied only in the third and fourth test cycle

Table 3-1: Thermal properties of used materials (continued)

| Specimen | Layer | Thickness | | Conductivity "k" | Conductance "C" | Thermal Resistance "R" | |
|-----------|-----------------------|-----------|-------|---------------------|-------------------------|---------------------------|---------------------------|
| | | (inch) | (mm) | (W/(m.K)) | (W/(m ² .K)) | (m ² K/W) | (ft ² h°F/Btu) |
| B2 | * Damp-proofing | 0 | 1.6 | - | - | - | - |
| | Parging | 3/8 | 9.5 | 0.7200 | 75.59 | 0.013 | 0.075 |
| | Concrete Masonry Unit | 8 | 203.2 | - | 2.58 | 0.388 | 2.202 |
| | Polyisocyanurate | 2 | 50.8 | 0.0222 | 0.44 | 2.288 | 13.002 |
| | Gypsum Board | 3/8 | 9.5 | 0.1680 | 17.64 | 0.057 | 0.322 |
| | Total | | | | | 2.866 | 16.283 |
| B3 | * Damp-proofing | 0 | 1.6 | - | - | - | - |
| | Parging | 3/8 | 9.5 | 0.7200 | 75.59 | 0.013 | 0.075 |
| | Concrete Masonry Unit | 8 | 203.2 | - | 2.58 | 0.388 | 2.202 |
| | Glass Fibre | 2 1/4 | 57.2 | 0.0338 | 0.59 | 1.691 | 9.607 |
| | Gypsum Board | 3/8 | 9.5 | 0.1680 | 17.64 | 0.057 | 0.322 |
| | Total | | | | | 2.268 | 12.888 |
| C1 | * Damp-proofing | 0 | 1.6 | - | - | - | - |
| | Parging | 3/8 | 9.5 | 0.7200 | 75.59 | 0.013 | 0.075 |
| | Concrete Masonry Unit | 8 | 203.2 | - | 2.58 | 0.388 | 2.202 |
| | Expanded Polystyrene | 2 | 50.8 | 0.0350 | 0.69 | 1.451 | 8.247 |
| | Gypsum Board | 3/8 | 9.5 | 0.1680 | 17.64 | 0.057 | 0.322 |
| | Total | | | | | 2.029 | 11.528 |
| C2 | * Damp-proofing | 0 | 1.6 | - | - | - | - |
| | Parging | 3/8 | 9.5 | 0.7200 | 75.59 | 0.013 | 0.075 |
| | Concrete Masonry Unit | 8 | 203.2 | - | 2.58 | 0.388 | 2.202 |
| | Total | | | | | 0.521 | 2.959 |
| C3 | * Damp-proofing | 0 | 1.6 | - | - | - | - |
| | Parging | 3/8 | 9.5 | 0.7200 | 75.59 | 0.013 | 0.075 |
| | Concrete | 8 | 203.2 | 2.0000 | 9.84 | 0.102 | 0.577 |
| | Total | | | | | 0.235 | 1.334 |

* Damp-proofing is applied only in the third and fourth test cycle

The R-value of each specimen is shown in Figure 3-3 in SI units and in Figure 3-4 in IP units. Thermal insulation corresponding to Pennsylvania requirements (10 ft²h°F/Btu) was applied to seven specimens (test segments) (A1 to C1). The last two specimens were plain CMU and concrete structures without thermal insulation (C2 and C3) and served as controls.

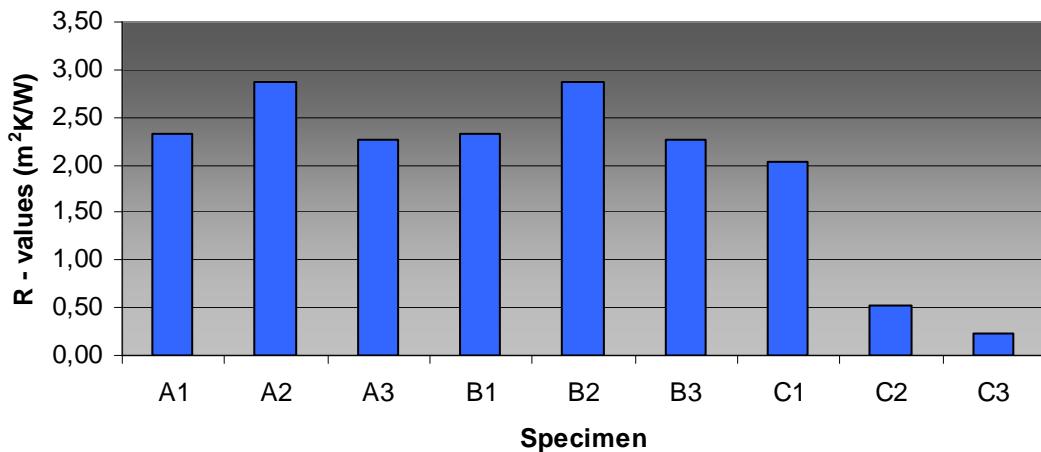


Figure 3-3: R – values used in specimens – SI units

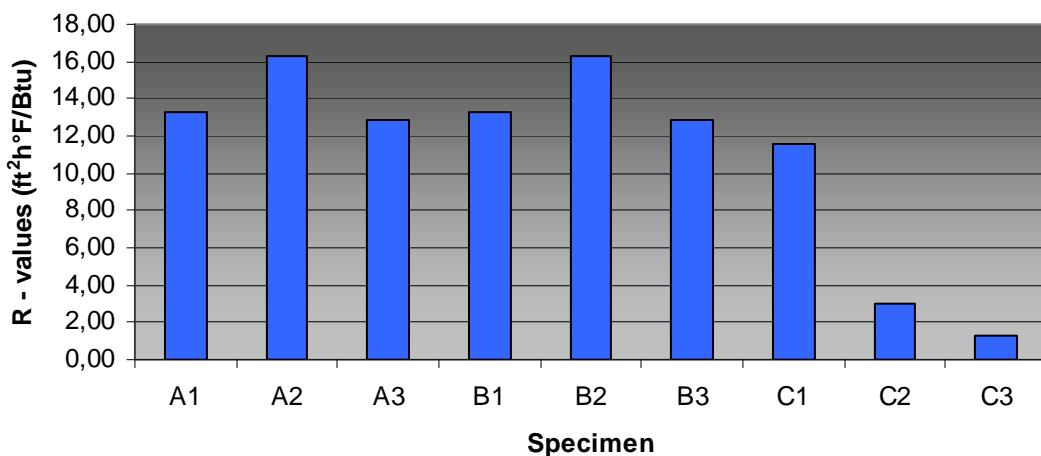


Figure -4: R – values used in specimens – IP units

For calculation of the water vapor diffusion through walls, moisture related physical properties were needed. The properties are listed in Table 3-2.

Table 3-2 Water vapor transmission data

| Specimen | Layer | Permeability | | Permeance "M" | | Diffusion resistance (without coating) "Z" | Diffusion resist. (with coating) "Z" |
|-----------|-----------------------|--------------|-------------|---------------------------|--------|--|--------------------------------------|
| | | (ng/s.m.Pa) | (perm.inch) | (ng/s.m ² .Pa) | (perm) | (Pa.m ² .s/ng) | (Pa.m ² .s/ng) |
| A1 | Extruded Polystyrene | 1.605 | 1.100 | 31.598 | 0.550 | 0.0316 | 0.0316 |
| | * Damp-proofing | 0.013 | 0.009 | 8.043 | 0.140 | - | 0.1243 |
| | Parging | - | - | 333.210 | 5.800 | 0.0030 | 0.0030 |
| | Concrete Masonry Unit | - | - | 137.880 | 2.400 | 0.0073 | 0.0073 |
| | Gypsum Board | - | - | 2872.500 | 50.000 | 0.0003 | 0.0003 |
| Total | | | | | | 0.0424 | 0.1667 |
| A2 | Polyisocyanurate | 5.107 | 3.500 | 100.538 | 1.750 | 0.0099 | 0.0099 |
| | * Damp-proofing | 0.013 | 0.009 | 8.043 | 0.140 | - | 0.1243 |
| | Parging | - | - | 333.210 | 5.800 | 0.0030 | 0.0030 |
| | Concrete Masonry Unit | - | - | 137.880 | 2.400 | 0.0073 | 0.0073 |
| | Gypsum Board | - | - | 2872.500 | 50.000 | 0.0003 | 0.0003 |
| Total | | | | | | 0.0207 | 0.1450 |
| A3 | Glass Fibre | 175.108 | 120.000 | 3064.000 | 53.333 | 0.0003 | 0.0003 |
| | * Damp-proofing | 0.013 | 0.009 | 8.043 | 0.140 | - | 0.1243 |
| | Parging | - | - | 333.210 | 5.800 | 0.0030 | 0.0030 |
| | Concrete Masonry Unit | - | - | 137.880 | 2.400 | 0.0073 | 0.0073 |
| | Gypsum Board | - | - | 2872.500 | 50.000 | 0.0003 | 0.0003 |
| Total | | | | | | 0.0110 | 0.1354 |
| B1 | * Damp-proofing | 0.013 | 0.009 | 8.043 | 0.140 | - | 0.1243 |
| | Parging | - | - | 333.210 | 5.800 | 0.0030 | 0.0030 |
| | Concrete Masonry Unit | - | - | 137.880 | 2.400 | 0.0073 | 0.0073 |
| | Extruded Polystyrene | 1.605 | 1.100 | 31.598 | 0.550 | 0.0316 | 0.0316 |
| | Gypsum Board | - | - | 2872.500 | 50.000 | 0.0003 | 0.0003 |
| Total | | | | | | 0.0424 | 0.1667 |

* Damp-proofing is applied only in the third and fourth test cycle

Table 3-2: Water vapor transmission data (continued)

| Specimen | Layer | Permeability | | Permeance "M" | | Diffusion resistance (without coating) "Z" | Diffusion resist. (with coating) "Z" |
|-----------|-----------------------|--------------|-------------|---------------------------|--------|--|--------------------------------------|
| | | (ng/s.m.Pa) | (perm.inch) | (ng/s.m ² .Pa) | (perm) | (Pa.m ² .s/ng) | (Pa.m ² .s/ng) |
| B2 | * Damp-proofing | 0.013 | 0.009 | 8.043 | 0.140 | - | 0.1243 |
| | Parging | - | - | 333.210 | 5.800 | 0.0030 | 0.0030 |
| | Concrete Masonry Unit | - | - | 137.880 | 2.400 | 0.0073 | 0.0073 |
| | Polyisocyanurate | 5.107 | 3.500 | 100.538 | 1.750 | 0.0099 | 0.0099 |
| | Gypsum Board | - | - | 2872.500 | 50.000 | 0.0003 | 0.0003 |
| Total | | | | | | 0.0207 | 0.1450 |
| B3 | * Damp-proofing | 0.013 | 0.009 | 8.043 | 0.140 | - | 0.1243 |
| | Parging | - | - | 333.210 | 5.800 | 0.0030 | 0.0030 |
| | Concrete Masonry Unit | - | - | 137.880 | 2.400 | 0.0073 | 0.0073 |
| | Glass Fibre | 175.108 | 120.000 | 3064.000 | 53.333 | 0.0003 | 0.0003 |
| | Gypsum Board | - | - | 2872.500 | 50.000 | 0.0003 | 0.0003 |
| Total | | | | | | 0.0110 | 0.1354 |
| C1 | * Damp-proofing | 0.013 | 0.009 | 8.043 | 0.140 | - | 0.1243 |
| | Parging | - | - | 333.210 | 5.800 | 0.0030 | 0.0030 |
| | Concrete Masonry Unit | - | - | 137.880 | 2.400 | 0.0073 | 0.0073 |
| | Expanded Polystyrene | 7.296 | 5.000 | 143.625 | 2.500 | 0.0070 | 0.0070 |
| | Gypsum Board | - | - | 2872.500 | 50.000 | 0.0003 | 0.0003 |
| Total | | | | | | 0.0177 | 0.1420 |
| C2 | * Damp-proofing | 0.013 | 0.009 | 8.043 | 0.140 | - | 0.1243 |
| | Parging | - | - | 333.210 | 5.800 | 0.0030 | 0.0030 |
| | Concrete Masonry Unit | - | - | 137.880 | 2.400 | 0.0073 | 0.0073 |
| | Total | | | | | 0.0104 | 0.1347 |
| C3 | * Damp-proofing | 0.013 | 0.009 | 8.043 | 0.140 | - | 0.1243 |
| | Parging | - | - | 333.210 | 5.800 | 0.0030 | 0.0030 |
| | Concrete | 4.670 | 3.200 | 22.980 | 0.400 | 0.0435 | 0.0435 |
| | Total | | | | | 0.0466 | 0.1710 |

* Damp-proofing is applied only in the third and fourth test cycle

The interior air film resistance was taken for a vertical surface position with horizontal direction of heat flow, according to the ASHRAE Handbook. This represented an R-value of 0.12 m²K/W. Similarly, the permeance of air film of 9200 ng/(s.m²Pa) was used. Permeance of the air film is very large compared of other materials used in the system and therefore does not affect the results significantly.

4. Determination of moisture content

The moisture content of materials was determined using equilibrium RH measurements.

4.1 Soil characteristics

Soil contains solid particles such as sand, silt, and clay and voids or pores. The pores contain air and water. Void or pore volume, which contains air and water, ranges from about 30 % in sand to about 50 % in clay of the total volume of soil. Clay has more pore volume than sand but the pores are smaller because of the smaller particle sizes of clay. Sand has larger pore sizes because of larger particle sizes. Both pore volume and pore size play major roles in water movement and the water retention or water-holding capacity of soil.

Saturated soil has pores completely filled with water but in reality, complete saturation does not occur because some entrapped air exists in saturated soil. No air can flow through the soil. Unsaturated soil has pores partially filled with water so that air can flow through the soil.

4.2 Characteristics of wall assemblies

Regular 8 in thick concrete-masonry units were used and bonded by S-type regular mortar and parged with base white stucco. The moisture content of such wall assembly varies according to water vapor transmission properties of individual material. Therefore, sorption isotherms were determined for each of the wall components.

4.3 Measurement of sorption isotherms

The relative humidity of soils and wall components at equilibrium steady-state were measured in the small environmental chamber. The properties of soil were measured directly and the wall assembly RH was measured in the CMU cavity. As mentioned above the wall assembly contained three different materials. Therefore, the sorption isotherms were measured for each material and the sorption isotherm for the wall assembly was calculated based on its component properties.

The sorption isotherms were developed for the test conditions representing 10°C and 20°C (approximate temperatures in the middle of the wall).

Separate sorption isotherm data were obtained for materials initially dry and for materials initially saturated (desorption isotherm). The moisture content of all materials was measured gravimetrically. ThermoForma 3911 shown in the figure 4-1 and Watflow series 988 controller were used in the test. Each temperature and water vapor setting was held constant for 5 days prior taking the measurements.



Figure 4-1: ThermoForma 3911 environmental chamber

Prior to the test each sample was dried at 100 °C to obtain the dry weight. The following formulas were used to calculate the moisture content and the bulk density of each material:

1. Gravimetric moisture content:

$$GMC = ((W_w - W_d) / W_d) \cdot 100 \quad (\%) \quad (5)$$

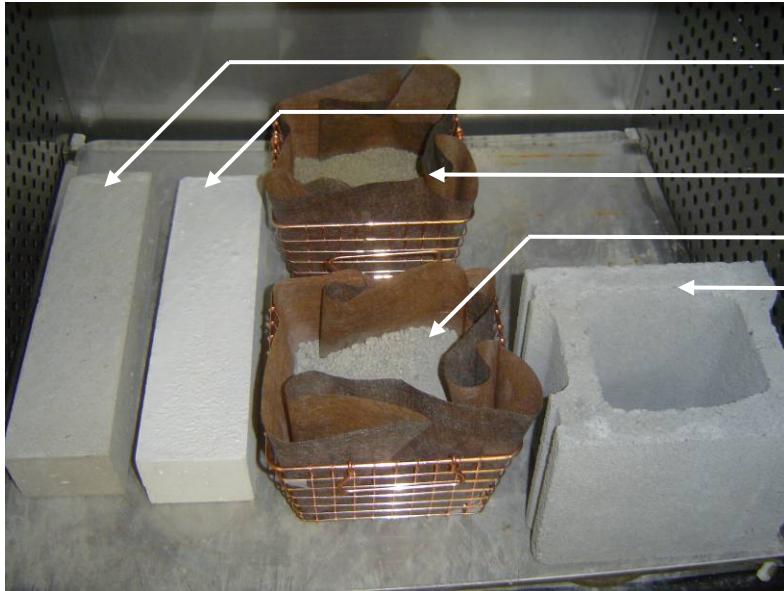
W_w = weight of the wet material

W_w = weight of the dry material (g, kg)

2. Bulk density:

$$BD = W_d / V_s \quad (\text{kg/m}^3) \quad (6)$$

V_s = volume of the soil sample (m^3)



Measurement sensors:

Mortar – S type
Plaster
Sand
Clay
CMU

Figure 4-2: Specimens used in sorption isotherm tests

Figure 4-2 shows the sorption isotherm test specimens. The sand and clay was put into a basket. To hold the soil in basket was lined with permeable fabric. $\frac{1}{2}$ of the CMU unit was used to minimize the test time.

Figure 4-3 shows the sorption and desorption isotherms at 10°C (50°F) for each tested material. Dry samples were subjected to increased 50% RH and the RH was increased in 10% steps until the upper RH limit (about 99%) was reached. Then the RH in the chamber was stepwise reduced (again in decrements of 10%) until 50% RH was reached. At each step (5 days/step) specimens were weighed.

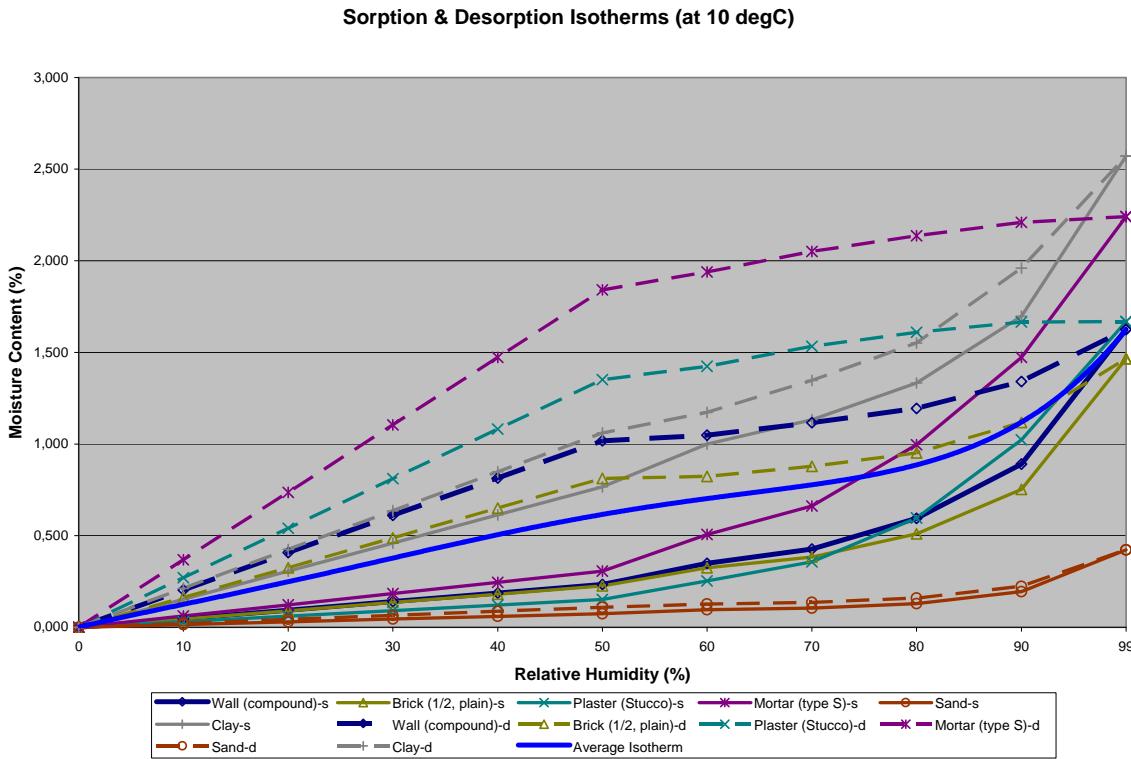


Figure 4-3: Sorption and desorption isotherms at 10 °C (50 °F)

Figure 4-4 shows sorption and desorption isotherms at 20 °C (68 °F) for individual materials. Calculated properties of the wall assembly are also shown. The bold red (10 °C; figure 4-2) and blue (20 °C; figure 4-2) isotherms show moisture content of parged wall without hysteresis. Regression equations can be used to estimate the overall moisture contents of the wall (note that the formula applies to this test assembly only):

1. MC-RH curve for 10 °C (50 °F) is expressed by a following polynomial function:

$$MC_{10} = 10.614x^5 - 18.242x^4 + 9.8522x^3 - 1.9674x^2 + 1.369x + 9E-05$$

x is the measured level of RH (-)

2. MC-RH curve for 20 °C (68 °F) is expressed by a following polynomial function:

$$MC_{20} = 29.634x^5 - 53.202x^4 + 29.963x^3 - 6.3596x^2 + 2.6556x - 0.0007$$

For example, at 100 % of RH and 10 °C the MC of the parged wall is 1.63 % of its dry weight. At about 100 % of RH and 20 °C the MC of the parged wall is 2.69 %.

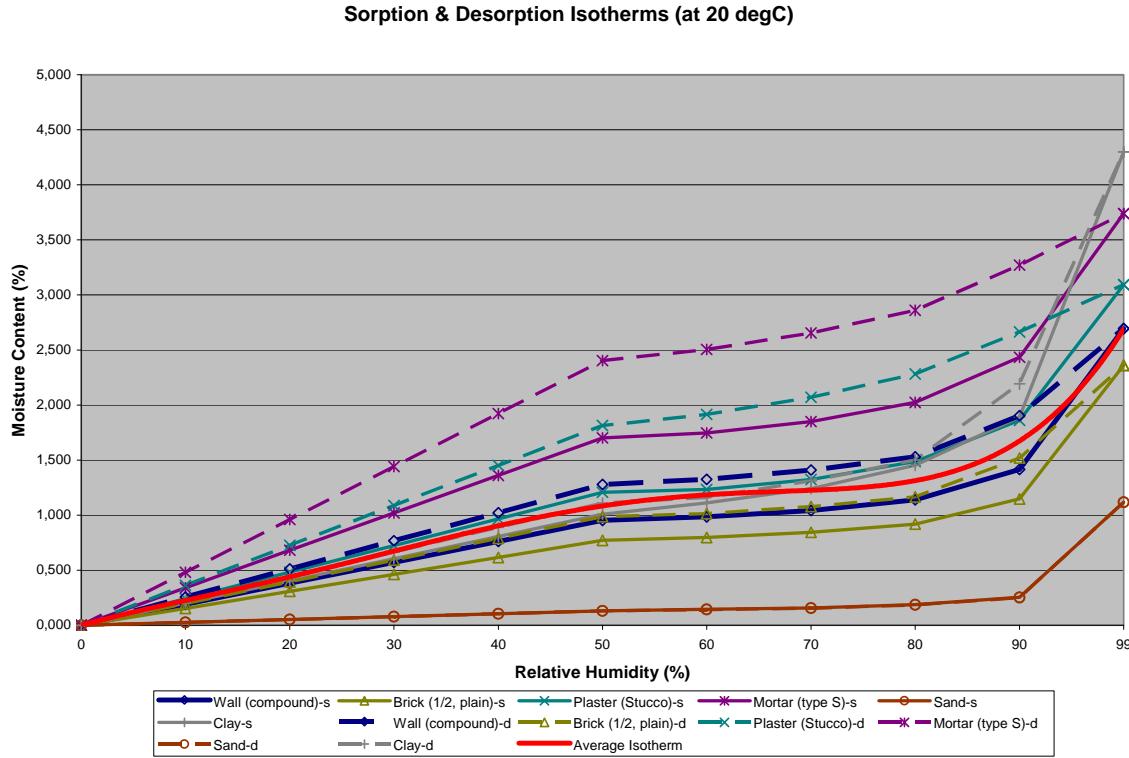


Figure 4-4: Sorption isotherms at 20 °C (68 °F)

From Figures 4-3 and 4-4 it is evident that the lower moisture content is attained by sand compared to clay.

5. Experimental results

The experiments yielded large volume of data and individual results are in the Appendix. The impact of soil, environmental parameters, position of the insulation layer, damp-proofing, sorption and desorption of wall assemblies on wall performance are discussed below. The test cycles and setup are discussed in Chapter 2.

The accuracy of the results was influenced by the following factors:

1. Material properties from manufacturer technical data sheets were used.
2. Finite time was used to declare steady state conditions (steady-state conditions are approached asymptotically and relatively long times are required to achieve them).
3. Significant time to dry the wall assembly is required. In the experiments, this time was kept to a minimum (again, steady-state is reached asymptotically).
4. HVAC equipment was producing suction or overpressure during interior/exterior side conditioning.

5.1 Soil

Soil thermal properties are difficult to measure in the field because soil temperatures are in a constant state of flux from diurnal and seasonal variations. Temperature variations are most extreme at the surface of the soil and these variations are transferred to sub-surface layers at reduced rates as depth increases. Additionally there is a time delay when maximum and minimum temperatures are achieved at increasing soil depth (referred to as thermal lag). To better understand the impact of soil on below-grade walls, our measurements were focusing only on thermal and moisture effects during steady state conditions.

Thermal properties of soils are influenced by soil volumetric water content, volume fraction of solids, and volume fraction of air. Air is a poor thermal conductor and reduces the effectiveness of solid and liquid phases to conduct heat. While the solid phase has the highest conductivity it is the variability of soil moisture that largely determines land temperatures. Soil moisture and thermal properties are closely linked and are often measured and reported together.

Our results indicate that at lower moisture contents the thermal properties of sand and clay are similar. At higher moisture and up to the saturation point, the thermal conductivity of sand is twice higher than the thermal conductivity of clay. This means that clay is a better thermal insulation material compared to sand at higher MC – see figures 5-1 and 5-2 and Appendix C. The measurements show a slight increase in temperature along the vertical axis.

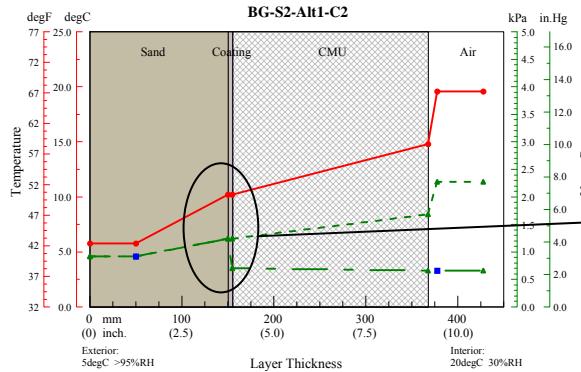


Figure 5-1: Wall diagram of S2-Alt1-C2 (sand – 3rd cycle, damp-proofing, $T_i = 20^\circ\text{C}$ (68°F), $T_e = 5^\circ\text{C}$ (41°F), $\text{RH}_i = 30\%$, $\text{RH}_e = 70\%$, uninsulated (plain) CMU structure)

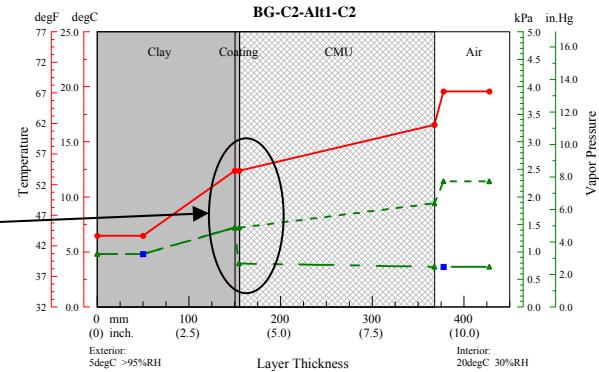


Figure 5-2: Wall diagram of C2-Alt1-C2 (clay – 3rd cycle, damp-proofing, $T_i = 20^\circ\text{C}$ (68°F), $T_e = 5^\circ\text{C}$ (41°F), $\text{RH}_i = 30\%$, $\text{RH}_e = 70\%$, uninsulated (plain) CMU structure)

Water can enter basement walls by capillary suction while in contact with wet soil. Clay soils can transfer large volumes of moisture through a basement wall by capillary suction. Installation of a capillary break between the soil and the basement wall will prevent capillary wetting of the structure. Free draining backfill, drainage boards, rigid insulation and especially water-proofing and damp-proofing (shown in figures 5-1 and 5-2) are effective capillary breaks. Soil moisture content was always at the full saturation value.

5.2 Wall components

Each wall component was evaluated using procedures presented in Chapter 2. Individual results are shown in the Appendix. Some of the major findings are summarized in Tables 5-1 to 5-4. According to research studies (ASHRAE Handbook, etc.[3]), surface relative humidity above 70 % is considered to represent a threshold for potential risk of mold growth (marked with green rectangles). The value of $\pm 2\%$ of $>97\%$ RH defines condensation beneath the insulation layer (marked with red rectangles).

5.2.1 S1 and C1-Alt1 (sand – 1st and clay – 2nd cycle, no damp-proofing, $T_i = 20^\circ\text{C}$ (68°F), $T_e = 5^\circ\text{C}$ (41°F), $\text{RH}_i = 30\%$, $\text{RH}_e = 70\%$)

Appendix C shows that the wall assemblies with an exterior insulation (A1, A2, A3) performed significantly better compared to walls with interior insulation (B1, B2, B3, C1). Exterior insulation absorbs the temperature drop and allows higher interior surface temperature of the wall. The water vapor saturation pressure allows higher indoor RH. Moisture content of specimens was affected by placement of thermal insulation. For example, XPS could be used as a water-proofing layer against bulk water intrusion due to its low permeability. Drying to exterior that is present in cold climates and saturated soil in contact with the wall influences the interface

beneath a thermal insulation. Because of the higher permeance of glass fiber, the specimen A3 has slightly higher moisture content compared to specimens insulated from the exterior. Permeable interior insulation allows interior moisture to migrate into the wall. This can only happen, however, if the relative water vapor pressure in the wall is lower than the relative water vapor pressure in the interior (this is the case in 5.2.2). Such a condition is rarely achieved under these circumstances (30 % of RH is maintained in interior) and unless a wall is protected in the exterior by a low-permeance material, moisture will migrate from exterior to interior. Plain walls (uninsulated) perform relatively well because they allow drying. The problem with plain walls involves high energy demand.

Thermal behavior of a wall is reflected by the overall R – values shown in Figures 3-3 and 3-4. The plain concrete wall has highest thermal conductivity followed by the plain CMU wall.

5.2.2 S1 and C1-Alt2 (sand – 1st and clay – 2nd cycle, no damp-proofing, T_i = 20°C (68°F), T_e = 5°C (41°F), RH_i = 60%, RH_e = 70%)

Performance of the walls is slightly different due to higher interior RH. Additional moisture introduced to the wall resulted in higher RH in the wall cavity (CMU). A higher value of RH is reached behind the exterior insulation while stopping the moisture transfer. XPS insulation inhibits the moisture entering the wall from interior and has reached lower RH values compared to other test setups (see Table 5-1 and 5-2). This is a consequence of otherwise prevailing influence of indoor R.H. (in this case blocked by low permeance XPS insulation) compared to low gravimetric and/or capillary forces in the soil (dry cycle of the soil preceded). Plain (uninsulated) walls have low condensation potential but will increase the moisture load in the interior dramatically if not equipped with reliable exterior water retarder (and water vapor barrier). If high permeance insulation (glass fiber) is applied from interior condensation can occur when humid air reaches a cold wall surface.

Table 5-1: Measurement results of S1

| S1 | | A1 | | A2 | | A3 | | B1 | | B2 | | B3 | | C1 | | C2 | | C3 | |
|----------|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | T | RH |
| | | (°C) | (%) |
| S1-Alt-1 | Soil | 5,58 | 100,0 | 6,29 | 100,0 | 6,26 | 100,0 | 4,61 | 98,1 | 5,70 | 100,0 | 5,93 | 100,0 | 4,99 | 100,0 | 6,56 | 100,0 | 6,66 | 100,0 |
| | *Wall | 15,86 | 55,8 | 16,47 | 58,0 | 16,47 | 62,3 | 7,07 | 77,8 | 8,42 | 84,6 | 8,61 | 80,3 | 7,90 | 76,3 | | | | |
| | Room air | 19,07 | 35,9 | 2,21 | 35,9 | 19,07 | 35,9 | 19,07 | 35,9 | 19,07 | 35,9 | 19,07 | 35,9 | 19,07 | 35,9 | 19,07 | 35,9 | 19,07 | 35,9 |
| | Cavity | | 47,1 | | 52,6 | | 52,5 | | 82,7 | | 84,1 | | 82,2 | | 80,6 | | 73,5 | | 100,0 |
| S1-Alt-2 | Soil | 5,39 | 100,0 | 6,08 | 100,0 | 6,09 | 100,0 | 4,36 | 91,8 | 5,49 | 100,0 | 5,76 | 100,0 | 4,78 | 99,9 | 6,50 | 100,0 | 6,78 | 100,0 |
| | *Wall | 15,66 | 55,9 | 16,30 | 58,9 | 16,32 | 62,3 | 6,96 | 82,9 | 8,12 | 96,6 | 8,67 | 99,8 | 7,74 | 90,3 | | | | |
| | Room air | 19,02 | 60,8 | 2,20 | 60,8 | 19,02 | 60,8 | 19,02 | 60,8 | 19,02 | 60,8 | 19,02 | 60,8 | 19,02 | 60,8 | 19,02 | 60,8 | 19,02 | 60,8 |
| | Cavity | | 50,4 | | 59,1 | | 58,6 | | 85,6 | | 86,6 | | 84,7 | | 83,1 | | 77,6 | | 100,0 |
| S1-Alt-3 | Soil | 5,83 | 100,0 | 6,33 | 100,0 | 6,31 | 100,0 | 4,71 | 100,0 | 5,72 | 100,0 | 6,11 | 100,0 | 4,91 | 95,2 | 6,68 | 100,0 | 7,17 | 100,0 |
| | *Wall | 16,27 | 56,8 | 17,04 | 60,2 | 17,02 | 61,0 | 7,36 | 83,5 | 8,51 | 98,2 | 9,16 | 100,0 | 8,18 | 94,0 | | | | |
| | Room air | 19,52 | 61,0 | 2,27 | 61,0 | 19,52 | 61,0 | 19,52 | 61,0 | 19,52 | 61,0 | 19,52 | 61,0 | 19,52 | 61,0 | 19,52 | 61,0 | 19,52 | 61,0 |
| | Cavity | | 52,1 | | 62,7 | | 61,9 | | 85,8 | | 89,0 | | 87,5 | | 85,6 | | 80,5 | | 100,0 |
| S1-Alt-4 | Soil | 5,69 | 100,0 | 6,43 | 100,0 | 6,59 | 100,0 | 4,40 | 99,4 | 5,55 | 100,0 | 5,88 | 100,0 | 4,35 | 100,0 | 6,29 | 100,0 | 6,75 | 100,0 |
| | *Wall | 15,74 | 56,7 | 16,77 | 60,4 | 16,78 | 62,4 | 6,85 | 78,8 | 8,13 | 96,7 | 8,33 | 94,3 | 7,10 | 86,9 | | | | |
| | Room air | 19,49 | 33,7 | 2,27 | 33,7 | 19,49 | 33,7 | 19,49 | 33,7 | 19,49 | 33,7 | 19,49 | 33,7 | 19,49 | 33,7 | 19,49 | 33,7 | 19,49 | 33,7 |
| | Cavity | | 46,5 | | 59,5 | | 58,8 | | 84,6 | | 90,1 | | 89,5 | | 86,6 | | 79,3 | | 100,0 |



Risk of condensation and potential mold growth



Condensing

Table -1: Measurement results of S1 (continued)

| S1 | | A1 | | A2 | | A3 | | B1 | | B2 | | B3 | | C1 | | C2 | | C3 | |
|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | | T (°C) | RH (%) |
| | | 19,35 | 100,0 | 19,14 | 100,0 | 19,23 | 100,0 | 18,88 | 94,6 | 17,87 | 100,0 | 18,36 | 100,0 | 19,51 | 100,0 | 19,96 | 100,0 | 21,80 | 100,0 |
| S1-Alt-5 | Soil | 19,87 | 66,4 | 19,46 | 73,0 | 19,56 | 88,5 | 18,22 | 73,6 | 17,09 | 94,3 | 17,50 | 66,2 | 19,54 | 79,2 | | | | |
| | *Wall | 20,86 | 37,0 | 2,47 | 37,0 | 20,86 | 37,0 | 20,86 | 37,0 | 20,86 | 37,0 | 20,86 | 37,0 | 20,86 | 37,0 | 20,86 | 37,0 | 20,86 | 37,0 |
| | Room air | | | | | | | | | | | | | | | | | | |
| | Cavity | | | | | | | | | | | | | | | | | | |
| S1-Alt-6 | Soil | 19,58 | 98,5 | 19,43 | 100,0 | 19,43 | 100,0 | 19,83 | 94,7 | 19,18 | 100,0 | 19,49 | 100,0 | 20,40 | 100,0 | 20,22 | 100,0 | 21,65 | 100,0 |
| | *Wall | 20,17 | 71,4 | 19,79 | 77,5 | 19,93 | 86,4 | 19,80 | 79,8 | 19,33 | 90,8 | 19,42 | 70,2 | 20,60 | 76,4 | | | | |
| | Room air | 20,53 | 56,8 | 2,42 | 56,8 | 20,53 | 56,8 | 20,53 | 56,8 | 20,53 | 56,8 | 20,53 | 56,8 | 20,53 | 56,8 | 20,53 | 56,8 | 20,53 | 56,8 |
| | Cavity | | | | | | | | | | | | | | | | | | |
| S1-Alt-7 | Soil | 20,57 | 100,0 | 21,27 | 100,0 | 20,45 | 100,0 | 20,87 | 100,0 | 20,47 | 100,0 | 21,17 | 100,0 | 21,41 | 100,0 | 21,31 | 100,0 | 22,16 | 100,0 |
| | *Wall | 18,68 | 72,5 | 18,34 | 81,7 | 18,63 | 100,0 | 20,07 | 72,2 | 19,85 | 80,7 | 19,72 | 69,1 | 21,10 | 77,8 | | | | |
| | Room air | 19,53 | 59,7 | 2,27 | 59,7 | 19,53 | 59,7 | 19,53 | 59,7 | 19,53 | 59,7 | 19,53 | 59,7 | 19,53 | 59,7 | 19,53 | 59,7 | 19,53 | 59,7 |
| | Cavity | | | | | | | | | | | | | | | | | | |
| S1-Alt-8 | Soil | 20,32 | 100,0 | 20,09 | 100,0 | 20,06 | 100,0 | 19,68 | 100,0 | 20,17 | 100,0 | 20,49 | 100,0 | 20,50 | 100,0 | 20,43 | 100,0 | 22,87 | 100,0 |
| | *Wall | 19,51 | 74,4 | 19,00 | 81,5 | 19,23 | 100,0 | 20,29 | 57,6 | 20,03 | 73,1 | 20,13 | 43,2 | 20,81 | 69,0 | | | | |
| | Room air | 19,47 | 32,4 | 2,26 | 32,4 | 19,47 | 32,4 | 19,47 | 32,4 | 19,47 | 32,4 | 19,47 | 32,4 | 19,47 | 32,4 | 19,47 | 32,4 | 19,47 | 32,4 |
| | Cavity | | | | | | | | | | | | | | | | | | |



Risk of condensation and potential mold growth



Condensing

Table -2: Measurement results of C1

| C1 | | A1 | | A2 | | A3 | | B1 | | B2 | | B3 | | C1 | | C2 | | C3 | |
|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | | T (°C) | RH (%) |
| | | 5,27 | 100,0 | 6,11 | 100,0 | 6,71 | 100,0 | 4,85 | 100,0 | 6,07 | 100,0 | 7,11 | 100,0 | 5,89 | 100,0 | 7,27 | 100,0 | 7,07 | 100,0 |
| C1-Alt-1 | Soil | 16,70 | 55,1 | 17,72 | 57,4 | 17,71 | 67,5 | 7,88 | 70,1 | 11,41 | 74,1 | 12,29 | 57,3 | 9,15 | 69,3 | | | | |
| | *Wall | 19,54 | 30,2 | 2,27 | 30,2 | 19,54 | 30,2 | 19,54 | 30,2 | 19,54 | 30,2 | 19,54 | 30,2 | 19,54 | 30,2 | 19,54 | 30,2 | 19,54 | 30,2 |
| | Room air | | | | | | | | | | | | | | | | | | |
| | Cavity | | | | | | | | | | | | | | | | | | |
| C1-Alt-2 | Soil | 5,45 | 100,0 | 6,06 | 100,0 | 6,55 | 100,0 | 4,96 | 100,0 | 5,82 | 100,0 | 6,84 | 100,0 | 5,86 | 100,0 | 7,23 | 100,0 | 7,04 | 100,0 |
| | *Wall | 16,56 | 54,6 | 17,44 | 55,7 | 17,48 | 65,5 | 7,79 | 76,4 | 10,51 | 91,6 | 11,82 | 92,6 | 9,08 | 84,7 | | | | |
| | Room air | 19,50 | 57,9 | 2,27 | 57,9 | 19,50 | 57,9 | 19,50 | 57,9 | 19,50 | 57,9 | 19,50 | 57,9 | 19,50 | 57,9 | 19,50 | 57,9 | 19,50 | 57,9 |
| | Cavity | | | | | | | | | | | | | | | | | | |
| C1-Alt-3 | Soil | 6,10 | 100,0 | 6,54 | 100,0 | 6,84 | 100,0 | 5,89 | 100,0 | 6,09 | 100,0 | 7,04 | 100,0 | 5,91 | 100,0 | 7,19 | 100,0 | 6,88 | 100,0 |
| | *Wall | 16,66 | 56,7 | 17,47 | 57,2 | 17,49 | 65,2 | 8,09 | 79,1 | 10,43 | 97,1 | 11,59 | 97,6 | 9,07 | 89,5 | | | | |
| | Room air | 19,50 | 58,2 | 2,27 | 58,2 | 19,50 | 58,2 | 19,50 | 58,2 | 19,50 | 58,2 | 19,50 | 58,2 | 19,50 | 58,2 | 19,50 | 58,2 | 19,50 | 58,2 |
| | Cavity | | | | | | | | | | | | | | | | | | |
| C1-Alt-4 | Soil | 6,07 | 100,0 | 6,45 | 100,0 | 6,70 | 100,0 | 5,76 | 100,0 | 6,03 | 100,0 | 6,82 | 100,0 | 5,88 | 100,0 | 7,07 | 100,0 | 6,73 | 100,0 |
| | *Wall | 16,65 | 56,6 | 17,58 | 57,2 | 17,56 | 64,7 | 8,05 | 74,7 | 10,30 | 93,4 | 11,07 | 72,9 | 8,91 | 82,1 | | | | |
| | Room air | 19,50 | 32,8 | 2,27 | 32,8 | 19,50 | 32,8 | 19,50 | 32,8 | 19,50 | 32,8 | 19,50 | 32,8 | 19,50 | 32,8 | 19,50 | 32,8 | 19,50 | 32,8 |
| | Cavity | | | | | | | | | | | | | | | | | | |



Risk of condensation and potential mold growth



Condensing

Table -2: Measurement results of C1 (continued)

| C1 | | A1 | | A2 | | A3 | | B1 | | B2 | | B3 | | C1 | | C2 | | C3 | |
|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | | T (°C) | RH (%) |
| | | 18,34 | 100,0 | 18,60 | 100,0 | 18,75 | 100,0 | 18,14 | 100,0 | 17,93 | 100,0 | 18,51 | 99,8 | 18,04 | 100,0 | 18,69 | 100,0 | 21,69 | 100,0 |
| C1-Alt-5 | Soil | 18,73 | 66,8 | 18,58 | 75,2 | 18,69 | 98,4 | 18,15 | 66,7 | 17,41 | 87,3 | 17,77 | 44,6 | 18,36 | 66,3 | | | | |
| | *Wall | 19,51 | 27,8 | 2,27 | 27,8 | 19,51 | 27,8 | 19,51 | 27,8 | 19,51 | 27,8 | 19,51 | 27,8 | 19,51 | 27,8 | 19,51 | 27,8 | 19,51 | 27,8 |
| | Room air | | | | | | | | | | | | | | | | | | |
| | Cavity | | | | | | | | | | | | | | | | | | |
| C1-Alt-6 | Soil | 18,54 | 100,0 | 18,91 | 100,0 | 19,10 | 100,0 | 18,41 | 100,0 | 18,31 | 100,0 | 19,00 | 100,0 | 18,32 | 100,0 | 18,86 | 100,0 | 21,22 | 100,0 |
| | *Wall | 18,64 | 67,7 | 18,51 | 76,9 | 18,67 | 99,9 | 18,50 | 74,6 | 18,16 | 85,8 | 18,59 | 71,8 | 18,61 | 76,8 | | | | |
| | Room air | 19,56 | 60,9 | 2,28 | 60,9 | 19,56 | 60,9 | 19,56 | 60,9 | 19,56 | 60,9 | 19,56 | 60,9 | 19,56 | 60,9 | 19,56 | 60,9 | 19,56 | 60,9 |
| | Cavity | | | | | | | | | | | | | | | | | | |
| C1-Alt-7 | Soil | 19,31 | 100,0 | 19,44 | 100,0 | 19,58 | 100,0 | 19,76 | 100,0 | 19,45 | 100,0 | 19,69 | 100,0 | 19,95 | 100,0 | 20,70 | 100,0 | 23,45 | 100,0 |
| | *Wall | 18,46 | 73,0 | 18,05 | 79,3 | 18,17 | 100,0 | 18,97 | 79,3 | 18,60 | 89,4 | 18,95 | 75,3 | 19,64 | 79,9 | | | | |
| | Room air | 18,36 | 70,4 | 2,11 | 70,4 | 18,36 | 70,4 | 18,36 | 70,4 | 18,36 | 70,4 | 18,36 | 70,4 | 18,36 | 70,4 | 18,36 | 70,4 | 18,36 | 70,4 |
| | Cavity | | | | | | | | | | | | | | | | | | |
| C1-Alt-8 | Soil | 19,15 | 100,0 | 19,25 | 100,0 | 19,41 | 100,0 | 19,57 | 100,0 | 19,54 | 100,0 | 19,72 | 100,0 | 20,98 | 100,0 | 21,08 | 100,0 | 23,71 | 100,0 |
| | *Wall | 18,72 | 76,2 | 18,46 | 80,7 | 18,58 | 100,0 | 19,29 | 75,3 | 19,21 | 86,9 | 19,07 | 45,0 | 20,69 | 68,1 | | | | |
| | Room air | 19,43 | 32,8 | 2,26 | 32,8 | 19,43 | 32,8 | 19,43 | 32,8 | 19,43 | 32,8 | 19,43 | 32,8 | 19,43 | 32,8 | 19,43 | 32,8 | 19,43 | 32,8 |
| | Cavity | | | | | | | | | | | | | | | | | | |



Risk of condensation and potential mold growth



Condensing

Table -3: Measurement results of S2

| S2 | | A1 | | A2 | | A3 | | B1 | | B2 | | B3 | | C1 | | C2 | | C3 | |
|----------|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | T | RH |
| | | (°C) | (%) |
| S2-Alt-1 | Soil | 4,62 | 100,0 | 5,22 | 100,0 | 5,43 | 100,0 | 3,69 | 100,0 | 5,14 | 100,0 | 5,27 | 100,0 | 4,11 | 100,0 | 5,75 | 100,0 | 6,31 | 100,0 |
| | *Wall | 14,70 | 48,7 | 16,01 | 58,6 | 15,81 | 66,4 | 5,92 | 72,6 | 7,51 | 85,2 | 8,15 | 68,4 | 6,58 | 71,8 | | | | |
| | Room air | 19,57 | 28,9 | 2,28 | 28,9 | 19,57 | 28,9 | 19,57 | 28,9 | 19,57 | 28,9 | 19,57 | 28,9 | 19,57 | 28,9 | 19,57 | 28,9 | 19,57 | 28,9 |
| | Cavity | | 49,6 | | 51,1 | | 53,1 | | 79,9 | | 90,2 | | 81,3 | | 81,1 | | 66,8 | | 98,2 |
| S2-Alt-2 | Soil | 4,76 | 100,0 | 5,28 | 100,0 | 5,50 | 100,0 | 3,83 | 100,0 | 5,09 | 100,0 | 5,09 | 100,0 | 4,27 | 100,0 | 5,73 | 100,0 | 6,09 | 100,0 |
| | *Wall | 14,74 | 50,2 | 16,20 | 61,3 | 16,15 | 74,2 | 6,20 | 79,1 | 7,48 | 91,5 | 8,11 | 100,0 | 6,82 | 91,0 | | | | |
| | Room air | 19,51 | 59,2 | 2,27 | 59,2 | 19,51 | 59,2 | 19,51 | 59,2 | 19,51 | 59,2 | 19,51 | 59,2 | 19,51 | 59,2 | 19,51 | 59,2 | 19,51 | 59,2 |
| | Cavity | | 66,6 | | 61,2 | | 63,5 | | 83,0 | | 92,1 | | 93,3 | | 86,3 | | 77,9 | | 98,2 |
| S2-Alt-3 | Soil | 18,70 | 100,0 | 18,58 | 100,0 | 18,59 | 100,0 | 19,49 | 100,0 | 19,01 | 100,0 | 19,14 | 100,0 | 20,64 | 100,0 | 20,31 | 100,0 | 20,00 | 100,0 |
| | *Wall | 18,30 | 70,9 | 17,74 | 65,4 | 17,76 | 70,8 | 18,97 | 79,5 | 18,52 | 90,8 | 18,51 | 75,4 | 20,39 | 77,8 | | | | |
| | Room air | 18,62 | 63,4 | 2,15 | 63,4 | 18,62 | 63,4 | 18,62 | 63,4 | 18,62 | 63,4 | 18,62 | 63,4 | 18,62 | 63,4 | 18,62 | 63,4 | 18,62 | 63,4 |
| | Cavity | | 71,5 | | 64,1 | | 66,2 | | 87,4 | | 92,9 | | 99,8 | | 88,9 | | 83,1 | | 100,0 |
| S2-Alt-4 | Soil | 19,03 | 100,0 | 18,95 | 100,0 | 18,90 | 100,0 | 19,59 | 100,0 | 19,20 | 100,0 | 19,29 | 100,0 | 20,71 | 100,0 | 20,30 | 100,0 | 19,82 | 100,0 |
| | *Wall | 18,66 | 72,4 | 17,95 | 66,9 | 17,66 | 70,4 | 19,28 | 77,1 | 18,85 | 83,0 | 18,63 | 56,7 | 20,51 | 69,4 | | | | |
| | Room air | 19,29 | 45,2 | 2,24 | 45,2 | 19,29 | 45,2 | 19,29 | 45,2 | 19,29 | 45,2 | 19,29 | 45,2 | 19,29 | 45,2 | 19,29 | 45,2 | 19,29 | 45,2 |
| | Cavity | | 62,6 | | 61,1 | | 61,7 | | 91,4 | | 93,2 | | 100,0 | | 89,3 | | 83,7 | | 100,0 |



Risk of condensation and potential mold growth



Condensing

Table -4: Measurement results of C2

| C2 | | A1 | | A2 | | A3 | | B1 | | B2 | | B3 | | C1 | | C2 | | C3 | |
|----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | | T (°C) | RH (%) |
| | | 5,21 | 100,0 | 5,78 | 100,0 | 6,34 | 100,0 | 4,32 | 100,0 | 4,73 | 100,0 | 5,58 | 100,0 | 5,09 | 100,0 | 6,45 | 100,0 | 5,99 | 100,0 |
| C2-Alt-1 | Soil | 14,96 | 60,7 | 16,76 | 58,4 | 16,74 | 63,6 | 6,74 | 85,5 | 8,50 | 83,8 | 8,63 | 77,0 | 7,56 | 81,1 | | | | |
| | *Wall | 19,59 | 32,1 | 2,28 | 32,1 | 19,59 | 32,1 | 19,59 | 32,1 | 19,59 | 32,1 | 19,59 | 32,1 | 19,59 | 32,1 | 19,59 | 32,1 | 19,59 | 32,1 |
| | Room air | | | | | | | | | | | | | | | | | | |
| | Cavity | | | | | | | | | | | | | | | | | | |
| C2-Alt-2 | Soil | 4,29 | 100,0 | 4,73 | 100,0 | 5,47 | 100,0 | 3,67 | 100,0 | 4,38 | 100,0 | 5,19 | 100,0 | 4,57 | 100,0 | 6,13 | 100,0 | 5,55 | 100,0 |
| | *Wall | 14,86 | 61,2 | 16,76 | 60,7 | 16,99 | 66,3 | 6,13 | 91,8 | 8,05 | 95,9 | 9,10 | 100,0 | 6,98 | 95,9 | | | | |
| | Room air | 19,48 | 61,7 | 2,26 | 61,7 | 19,48 | 61,7 | 19,48 | 61,7 | 19,48 | 61,7 | 19,48 | 61,7 | 19,48 | 61,7 | 19,48 | 61,7 | 19,48 | 61,7 |
| | Cavity | | | | | | | | | | | | | | | | | | |
| C2-Alt-3 | Soil | 18,86 | 100,0 | 18,70 | 100,0 | 18,70 | 100,0 | 19,25 | 100,0 | 18,63 | 100,0 | 19,68 | 100,0 | 20,45 | 100,0 | 20,27 | 100,0 | 19,95 | 100,0 |
| | *Wall | 18,47 | 84,1 | 17,92 | 68,6 | 17,97 | 72,4 | 18,93 | 93,8 | 18,27 | 96,7 | 18,36 | 81,4 | 20,24 | 88,1 | | | | |
| | Room air | 18,90 | 63,6 | 2,18 | 63,6 | 18,90 | 63,6 | 18,90 | 63,6 | 18,90 | 63,6 | 18,90 | 63,6 | 18,90 | 63,6 | 18,90 | 63,6 | 18,90 | 63,6 |
| | Cavity | | | | | | | | | | | | | | | | | | |
| C2-Alt-4 | Soil | 18,86 | 100,0 | 18,74 | 100,0 | 18,75 | 100,0 | 19,36 | 100,0 | 18,81 | 100,0 | 19,37 | 100,0 | 20,60 | 100,0 | 20,46 | 100,0 | 20,10 | 100,0 |
| | *Wall | 18,61 | 84,4 | 17,98 | 68,3 | 17,83 | 71,6 | 19,22 | 88,9 | 18,73 | 86,1 | 18,63 | 55,8 | 20,32 | 81,9 | | | | |
| | Room air | 19,22 | 42,7 | 2,23 | 42,7 | 19,22 | 42,7 | 19,22 | 42,7 | 19,22 | 42,7 | 19,22 | 42,7 | 19,22 | 42,7 | 19,22 | 42,7 | 19,22 | 42,7 |
| | Cavity | | | | | | | | | | | | | | | | | | |



Risk of condensation and potential mold growth



Condensing

5.2.3 S1 and C1-Alt3 (sand – 1st and clay – 2nd cycle, no damp-proofing, T_i = 20°C (68°F), T_e = 5°C (41°F), RH_i = 60%, RH_e = >95%)

This test introduces >95 % RH from the exterior (environmental side) and 60 % from the interior (room side). Exterior insulation that protects the wall structure and keeps it warm performs better under high interior RH. Interior insulation with low-permeance fiber or porous materials increases a risk of condensation.

The results here are very similar to results in Alt1 (see S1 or C1-Alt1). Because of this small differences between Alt3 and Alt1 and Alt4 and Alt2 the remaining test runs (3rd and 4th) used >95 % of RH from exterior. This reduced number of test alternatives.

5.2.4 S1 and C1-Alt4 (sand – 1st and clay – 2nd cycle, no damp-proofing, T_i = 20°C (68°F), T_e = 5°C (41°F), RH_i = 30%, RH_e = >95%)

This test represents desorption cycle. The results indicate that with correct air conditioning system no condensation will occur. An alternate drying mechanism through an above-grade portion of a basement wall can alleviate the energy consumption issues. In cold climates, the drying will be toward the exterior; in warm climates the drying will occur toward the interior making the energy demand high. Interior glass fiber insulation showed the fastest drying because of its high permeance. This makes this material suitable more for mild climate when a drying to the interior is possible.

5.2.5 S1 and C1-Alt5 (sand – 1st and clay – 2nd cycle, no damp-proofing, T_i = 20°C (68°F), T_e = 20°C (68°F), RH_i = 30%, RH_e = 50%)

Mild climate is simulated in alternatives 5, 6, 7 and 8. The mild climate condition facilitates inward drying (or no mass transfer when equal conditions are achieved on both sides). This means that moisture, (gravimetric, capillary, and water vapor diffusion) transfer toward the interior. Again a water vapor retarder such as damp-proofing must be on the outside of the insulation. By using a low permeance thermal insulation, its position can be changed and this will not significantly affect the overall moisture transfer. This is shown in Figures 5-2 and 5-4 where the RH of specimen A1 reached the lowest values. High permeance fiber insulation on the exterior allows moisture migration into a basement wall and a habitable space. Therefore high permeance fiber insulations are more suitable for interior applications. On the other hand low permeance interior insulation does not prevent inward drying and this may result in condensation on the interface of the wall and insulation.

5.2.6 S1 and C1-Alt6 (sand – 1st and clay – 2nd cycle, no damp-proofing, T_i = 20°C (68°F), T_e = 20°C (68°F), RH_i = 60%, RH_e = 50%)

Increased interior RH is mostly influencing the drying process. This case is very similar to the previous one except that the high permeance fiber insulation has attained more moisture due to higher interior RH, which is slowing down the drying process.

5.2.7 S1 and C1-Alt7 (sand – 1st and clay – 2nd cycle, no damp-proofing, T_i = 20°C (68°F), T_e = 20°C (68°F), RH_i = 60%, RH_e = >95%)

High exterior RH resulted in higher RH beneath the insulation. Low permeance insulation boards (XPS, EPS) applied on the exterior performed well. Because of a draining function of glass fiber in specimen A3, the measured RH beneath it showed condensation. Again using high permeance fiber insulation permits drying and condensation should be preventable by dehumidification. The interior insulation resulted in about a 28% moisture increase in the CMU compared to the placement of the insulation on the exterior. For Alt5 test the difference in the CM|U RH was about 40 %.

5.2.8 S1 and C1-Alt8 (sand – 1st and clay – 2nd cycle, no damp-proofing, T_i = 20°C (68°F), T_e = 20°C (68°F), RH_i = 30%, RH_e = >95%)

High permeance fiber insulation on interior side requires dehumidification to permit inward drying of the structure. Exterior insulation constitutes a barrier to forces participating in moisture transfer. In general, low permeance insulation should be used on the exterior surface while high permeance insulation is more suitable for the interior surface. The behavior of each insulation is influenced through their water vapor transmission data and thermal characteristics.

5.2.9 S2 and C2-Alt1 (sand – 3rd and clay – 4th cycle, damp-proofing, T_i = 20°C (68°F), T_e = 5°C (41°F), RH_i = 30%, RH_e = >95%)

The third and fourth test runs included additional wetting of soil. Damp-proofing was applied on the exterior surface. The measurements using sand and clay showed very similar results. Damp-proofing applied on the wall surface is most of the time used as a barrier to block the moisture transfer induced by hydrostatic pressure. This provides a barrier against bulk water that can enter from the exterior. When clay is used as backfill, insulation capable of draining water should be used.

5.2.10 S2 and C2-Alt2 (sand – 3rd and clay – 4th cycle, damp-proofing, T_i = 20°C (68°F), T_e = 5°C (41°F), RH_i = 60%, RH_e = >95%)

When interior RH increases and drying toward the exterior is possible, low permeance insulation is acceptable. Damproofing and low permeance interior insulation require drying through the above-grade section of the wall to eliminate excessive moisture. Using high permeance fiber insulations increases the risk of condensation since moisture will come in contact with a cold wall beneath the insulation. The best results in the interior insulation strategy were achieved using XPS interior insulation.

5.2.11 S2 and C2-Alt3 (sand – 3rd and clay – 4th cycle, damp-proofing, T_i = 20°C (68°F), T_e = 20°C (68°F), RH_i = 60%, RH_e = >95%)

Insulation technique in a mild climate is different than in a cold climate. When a water vapor retarder is used (such as damp-proofing) it should be located on the outside surface of the insulation. In mild climate all combinations performed well except for B2 and B3, which reached higher RH during the test run. Low permeance insulation on the interior surface can cause accumulation of water in the structure due to inward moisture drive. This leads to condensation on the wall surface and can cause visible water outflow.

5.2.12 S2 and C2-Alt4 (sand – 3rd and clay – 4th cycle, damp-proofing, $T_i = 20^\circ\text{C}$ (68°F), $T_e = 20^\circ\text{C}$ (68°F), $\text{RH}_i = 30\%$, $\text{RH}_e = >95\%$)

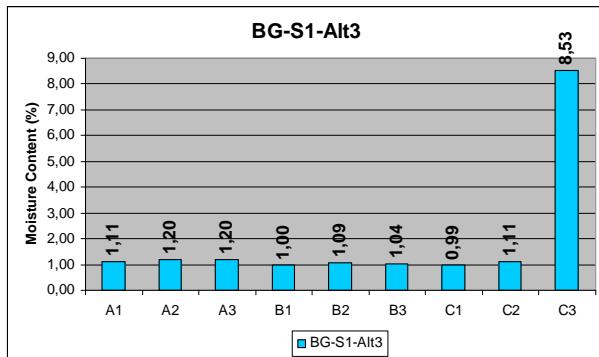
Dehumidification always reduces the risk of condensation but cannot be used as a tool to control steady influx of moisture from the soil. Again, low permeance insulation installed on interior surface constitutes a barrier for the moisture flow. During the test with no temperature difference the moisture flow resulted in evaporation of water vapor in the cavity of the CMU's. Therefore, the wall cavity can be used as a moisture controlling device if an evaporation path is provided.

5.3 Moisture contents of specimens

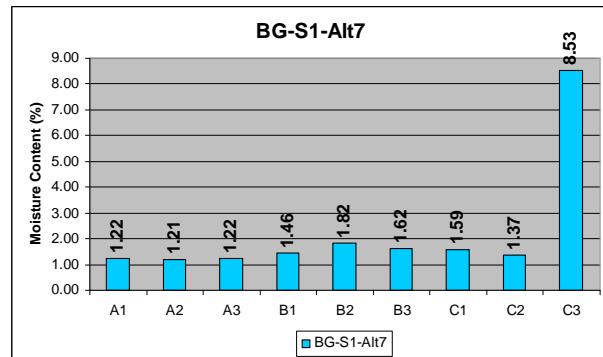
The moisture contents of specimens in cold and mild climates differed due to differences in water vapor pressures. From the thermodynamic point of view, naturally higher moisture contents are present in mild climates. The sorption isotherm at 10 °C was used to calculate the moisture contents in cold climates except when exterior insulation was used (i.e. higher wall temperatures were achieved). In that case the sorption isotherm at 20 °C was used. The sorption isotherm at 20°C was used for mild climates. An average value was determined for the plain CMU wall (specimen C2) when the resulting wall temperature was around 15 °C. The water content attained during the preparation of concrete (100%) was used as a moisture content of the plain concrete wall (specimen C3).

Figure 5-3 shows the moisture content of specimens in cold climate. The difference in the MC is caused by the temperature of the wall itself, Figure 5-4 shows the MC in a mild climate. When insulations are applied from the exterior the moisture contents are less as compared to interior insulation strategies

An interesting finding is that the CMU wall attained less moisture when exterior insulation was applied. This is shown in Figures 5-5 and 5-6. The differences became larger in the third and fourth test runs. This was mainly due to the installation of damp-proofing from the exterior and low permeance insulation from the interior. The moisture in walls could not evaporate since no above grade portion of wall was simulated to enable drying.



**Figure -3: Moisture content of S1-Alt3
(sand – 1st cycle, no damp-proofing, $T_i = 20^\circ\text{C}$ (68°F), $T_e = 5^\circ\text{C}$ (41°F), $\text{RH}_i = 60\%$, $\text{RH}_e = >95\%$)**



**Figure -4: Moisture content of S1-Alt7
(sand – 1st cycle, no damp-proofing, $T_i = 20^\circ\text{C}$ (68°F), $T_e = 20^\circ\text{C}$ (68°F), $\text{RH}_i = 60\%$, $\text{RH}_e = >95\%$)**

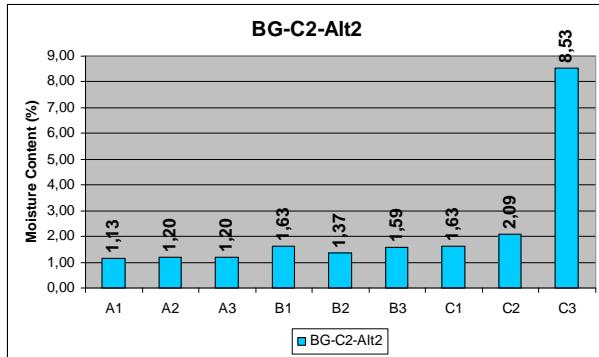


Figure -5: Moisture content of C2-Alt2 (clay – 4th cycle, damp-proofing, $T_i = 20^\circ\text{C}$ (68°F), $T_e = 5^\circ\text{C}$ (41°F), $\text{RH}_i = 60\%$, $\text{RH}_e = >95\%$)

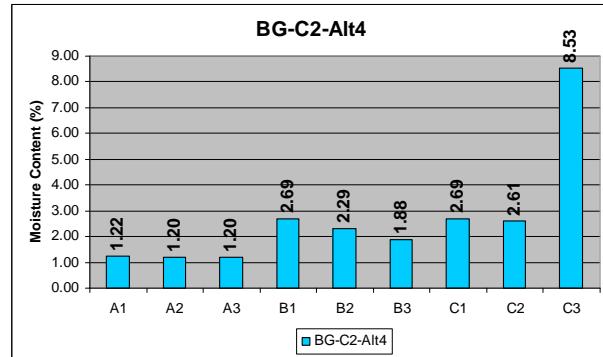


Figure -6: Moisture content of C2-Alt4 (clay – 4th cycle, damp-proofing, $T_i = 20^\circ\text{C}$ (68°F), $T_e = 20^\circ\text{C}$ (68°F), $\text{RH}_i = 30\%$, $\text{RH}_e = >95\%$)

6. Conclusions and recommendations

The final conclusions of the test measurements and wall specimens' performances are summarized in this chapter.

6.1 Conclusions

The tests conducted at BeTL showed interesting results and improved our understanding of the hygro-thermal behavior of below-grade basement walls. While the tests did not contain additional devices (such as flux meters) necessary for more conclusive statements, the following conclusions can be drawn:

1. the type of soil had some influence on the overall hygro-thermal behavior of the wall system. From the moisture transfer point of view plain (uninsulated) walls should be used as a basis for objective result comparison. When clay was used the moisture content in the CMU's cavity reached lower values as compared to sand. The difference was about 7 %. Sand had twice higher thermal conductivity as compared to clay. This resulted in a better thermal performance of the structure with clay soil.
2. Less dehumidification and/or drying is needed when low permeance exterior insulation is used. The drying rate depends on the initial stage of material built into the structure. Such an exterior insulation is working as a water-proofing layer as well.
3. High permeance insulation such as semi rigid glass fiber can be used on the exterior in cold climate to drain water away. From the thermal point of view, the conductivity of the wet insulation is higher compared to the dry one. Therefore, in cold climate and exterior insulation, the thermal performance of a wall decreases as the soil approaches saturation . High permeance insulation should be used on the interior if inward moisture drive is present. When drying to the exterior, high permeance insulation should be avoided due to the condensation on a cold wall beneath the insulation.
4. The advantage of exterior insulation is in its better thermal behavior (i.e. higher temperature of wall enabling higher saturation), water retardation (i.e. water ingress barrier), and thermal inertia (i.e. accumulation of heat in the wall structure during winter).
5. Plain structures without damp-proofing result in significant moisture flow and dehumidification is necessary. Plain structures with damp-proofing can attain higher MC when outward moisture flow is present.
6. Moisture content of CMU's is significantly lower than the initial water content of concrete.

6.2 Recommendations

Absence of heat flux meters during the experiments reduced the precision of measurements and data from manufacturers had to be used.

In order to finish the tests in a reasonable time, the time needed for steady-state conditions was shortened to a minimum. Ideally, one will need more time between the runs to assure close-to-steady-state conditions. The authors recognize, however, that reaching steady state is nearly impossible.

For future research, a comparison between laboratory and in-situ experiments is recommended. This will require a concurrent test where outdoor conditions are carefully monitored and reproduced in the laboratory.

1. Future work will focus on the influence of imperfections in the water retarding layer on durability and effects of material aging on system performance.
2. 2006 International Residential Code for one- and two-family dwellings. ICC Country Club Hills. IL. 672. p.
3. 2005 ASHRAE Handbook. Fundamentals. SI Edition. ASHRAE. Atlanta. GA. ISBN 1-931862-71-0.

Appendix A - Terminology and acronyms

The appendix A summarizes the terminology and acronyms used in the report.

- RH: relative humidity or relative water vapor pressure
- MC: moisture content
- BeTL: Building Enclosure Testing Laboratory
- PHRC: Pennsylvania Housing Research Center

Appendix B – Measurement results

Because of the large amount of data the measurement results are summarized in appendix B.

The measurement results and boundary conditions of the climate chamber are shown below in the following order:

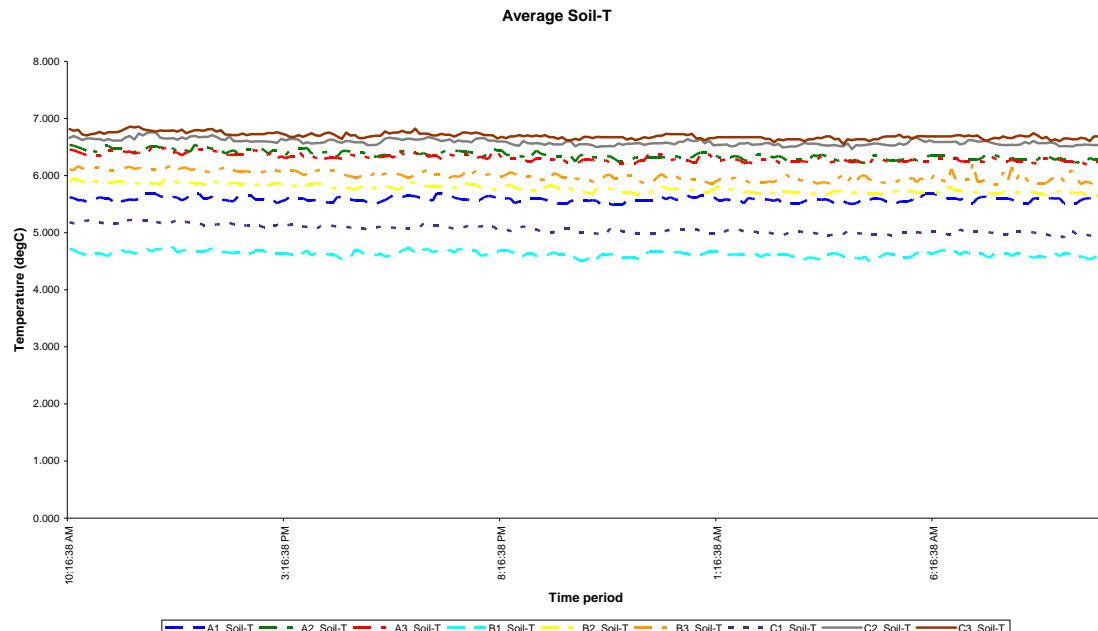
1. Measurement series: S1 (Sand; no dampproofing)
 - 1.1. Test cycle: S1-Alt1
 - 1.2. Test cycle: S1-Alt2
 - 1.3. Test cycle: S1-Alt3
 - 1.4. Test cycle: S1-Alt4
 - 1.5. Test cycle: S1-Alt5
 - 1.6. Test cycle: S1-Alt6
 - 1.7. Test cycle: S1-Alt7
 - 1.8. Test cycle: S1-Alt8
2. Measurement series: C1 (Clay; no dampproofing)
 - 2.1. Test cycle: C1-Alt1
 - 2.2. Test cycle: C1-Alt2
 - 2.3. Test cycle: C1-Alt3
 - 2.4. Test cycle: C1-Alt4
 - 2.5. Test cycle: C1-Alt5
 - 2.6. Test cycle: C1-Alt6
 - 2.7. Test cycle: C1-Alt7
 - 2.8. Test cycle: C1-Alt8
3. Measurement series: S2 (Sand; with dampproofing)
 - 3.1. Test cycle: S2-Alt1
 - 3.2. Test cycle: S1-Alt2
 - 3.3. Test cycle: S1-Alt3
 - 3.4. Test cycle: S1-Alt4
4. Measurement series: C2 (Clay; with dampproofing)
 - 4.1. Test cycle: C2-Alt1
 - 4.2. Test cycle: C1-Alt2
 - 4.3. Test cycle: C1-Alt3
 - 4.4. Test cycle: C1-Alt4

Measurement series: **S1 (Sand; no dampproofing)**

 Test cycle: **S1 – Alt1**
Table B-1: Average data during the last 24 hours for each specimen of S1-Alt1

| Specimen Measurement Data | | | | Control Loop Data | |
|---------------------------|-----------------------|-----------------------|---------------------------|-------------------|-----------------------------|
| B-G | A | B | C | Sand | |
| 1 | A1_Soil-T 5.578 degC | B1_Soil-T 4.608 degC | C1_Soil-T 4.992 degC | 1 | |
| | A1_Soil-RH 100.000 % | B1_Soil-RH 98.138 % | C1_Soil-RH 100.000 % | | T-room 19.073 degC |
| | A1_Wall-T 15.864 degC | B1_Wall-T 7.073 degC | C1_Wall-T 7.899 degC | | RH-room 35.945 % |
| | A1_Ext-T 6.781 degC | B1_Ext-T 5.887 degC | C1_Ext-T 6.175 degC | | T-room_sp 20.000 degC |
| | A1_Int-T 17.453 degC | B1_Int-T 17.601 degC | C1_Int-T 17.326 degC | | RH-room_sp 35.000 % |
| | A1_Inside-RH 47.124 % | B1_Inside-RH 82.661 % | C1_Inside-RH 80.593 % | | T-environment 4.476 degC |
| | A1_Wall-RH 55.775 % | B1_Wall-RH 77.805 % | C1_Wall-RH 76.348 % | | RH-environment 68.171 % |
| | | | | | T-environment_sp 3.000 degC |
| | | | | | RH-environment_sp 70.000 % |
| | | | | | |
| 2 | A2_Soil-T 6.294 degC | B2_Soil-T 5.703 degC | C2_Soil-T 6.561 degC | 2 | |
| | A2_Soil-RH 100.000 % | B2_Soil-RH 100.000 % | C2_Soil-RH 100.000 % | | |
| | A2_Wall-T 16.471 degC | B2_Wall-T 8.416 degC | C2_Ext-T 11.097 degC | | |
| | A2_Ext-T 7.735 degC | B2_Ext-T 7.107 degC | C2_Int-T 15.950 degC | | |
| | A2_Int-T 17.362 degC | B2_Int-T 17.788 degC | C2_Inside-RH 73.489 degC | | |
| | A2_Inside-RH 52.612 % | B2_Inside-RH 84.115 % | | | |
| | A2_Wall-RH 57.965 % | B2_Wall-RH 84.631 % | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| 3 | A3_Soil-T 6.256 degC | B3_Soil-T 5.931 degC | C3_Soil-T 6.664 degC | 3 | |
| | A3_Soil-RH 100.000 % | B3_Soil-RH 100.000 % | C3_Soil-RH 100.000 % | | |
| | A3_Wall-T 16.466 degC | B3_Wall-T 8.610 degC | C3_Ext-T 12.265 degC | | |
| | A3_Ext-T 7.842 degC | B3_Ext-T 6.931 degC | C3_Int-T 14.972 degC | | |
| | A3_Int-T 17.510 degC | B3_Int-T 17.541 degC | C3_Inside-RH 100.000 degC | | |
| | A3_Inside-RH 52.480 % | B3_Inside-RH 82.233 % | | | |
| | A3_Wall-RH 62.279 % | B3_Wall-RH 80.332 % | | | |
| | | | *Pressure diff. 6.076 Pa | | |
| | | | | | |
| | | | | | |
| No | A | B | C | Alt1 | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-1: Average soil temperature of S1-Alt1

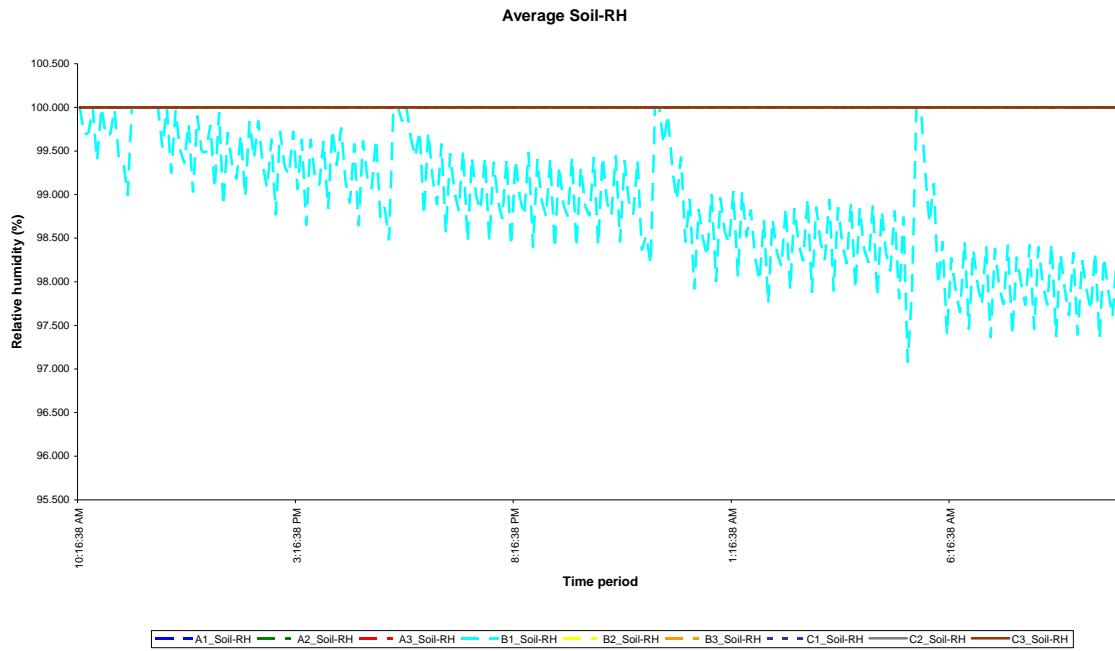


Figure B-2: Average soil relative humidity of S1-Alt1

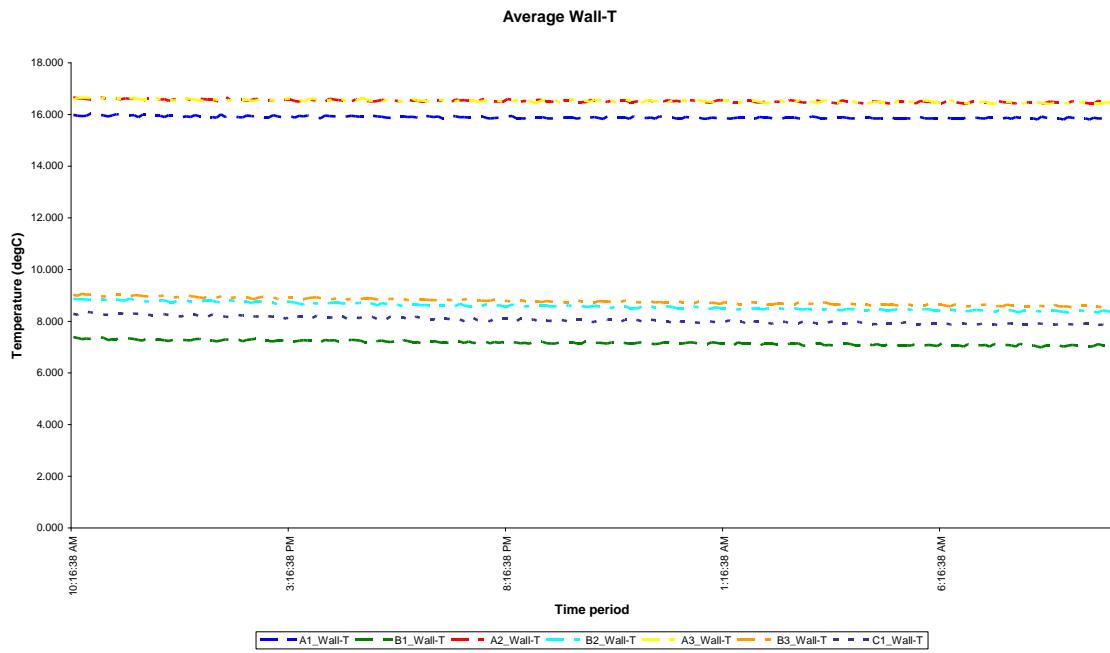


Figure B-3: Average wall temperature of S1-Alt1

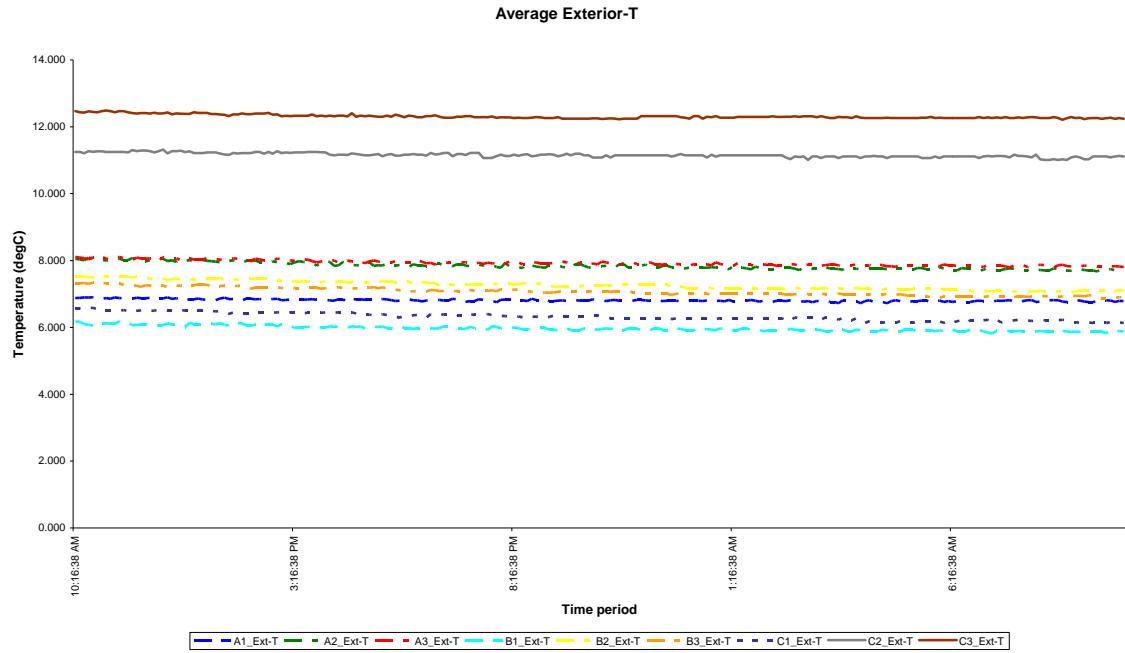


Figure B-4: Average exterior temperature of S1-Alt1

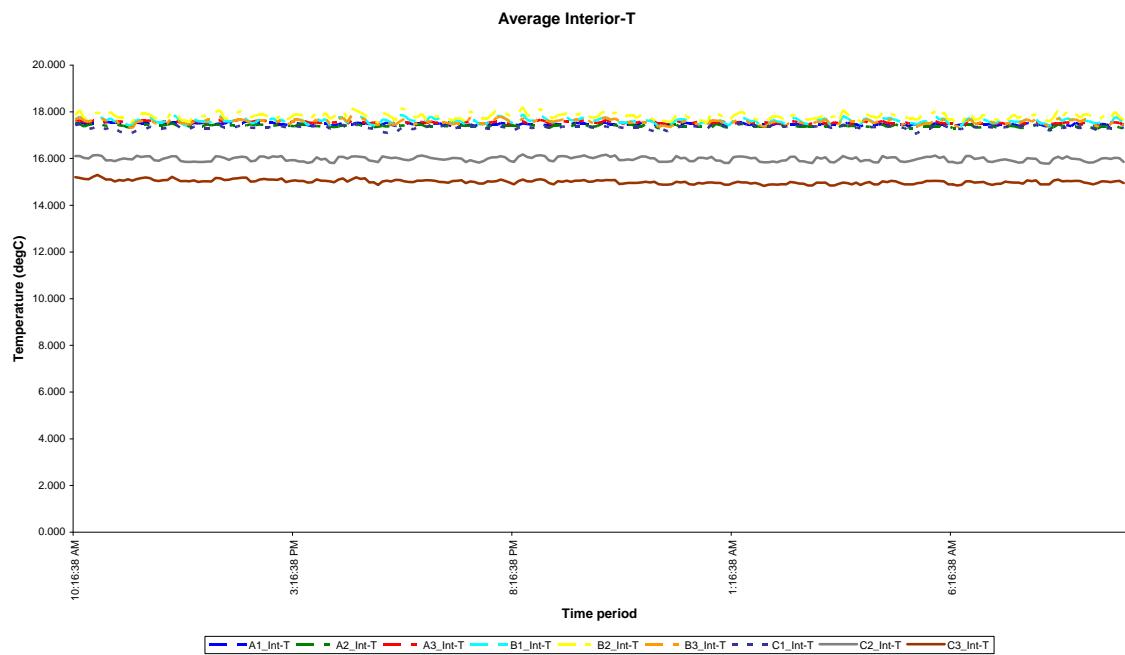


Figure B-5: Average interior temperature of S1-Alt1

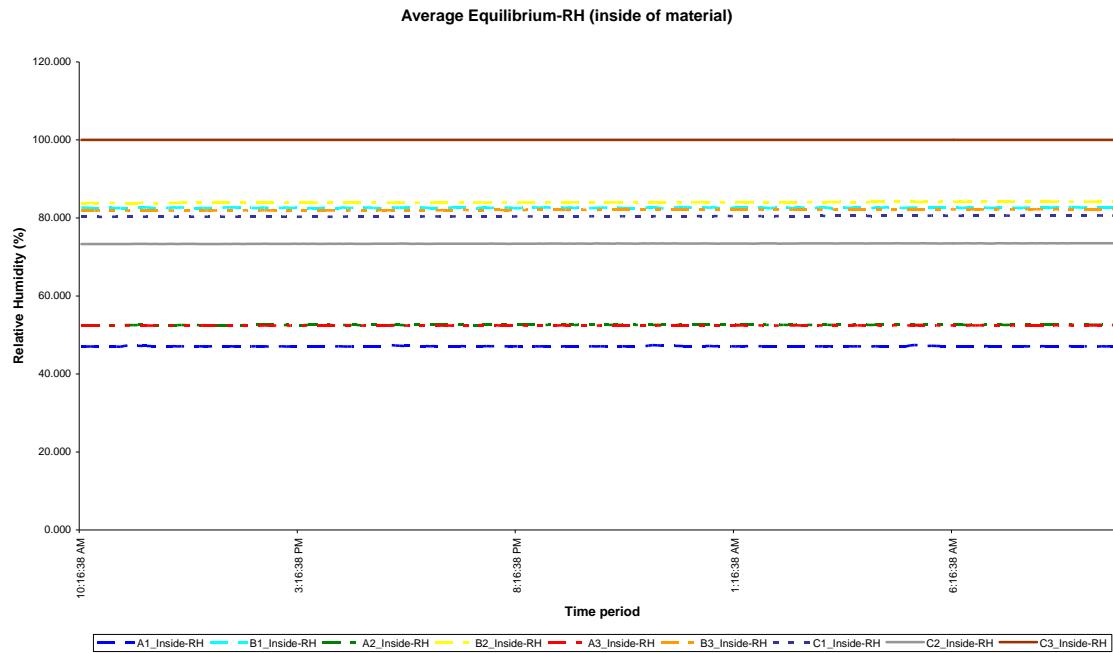


Figure B-6: Average equilibrium of relative humidity in a cavity of S1-Alt1

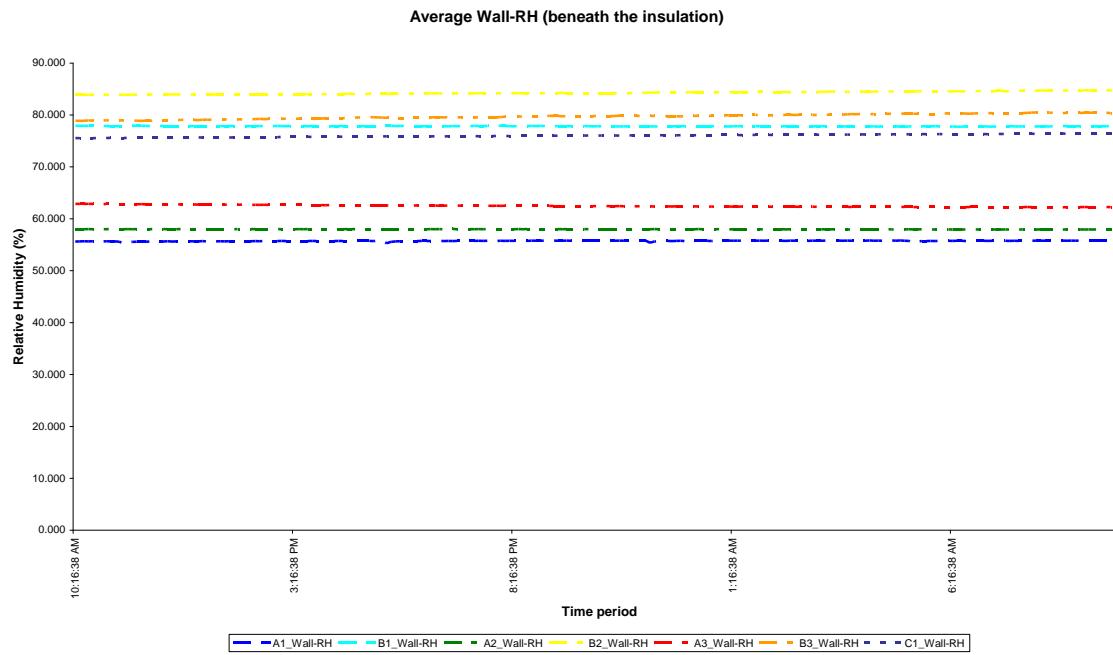


Figure B-7: Average wall relative humidity beneath the insulation of S1-Alt1

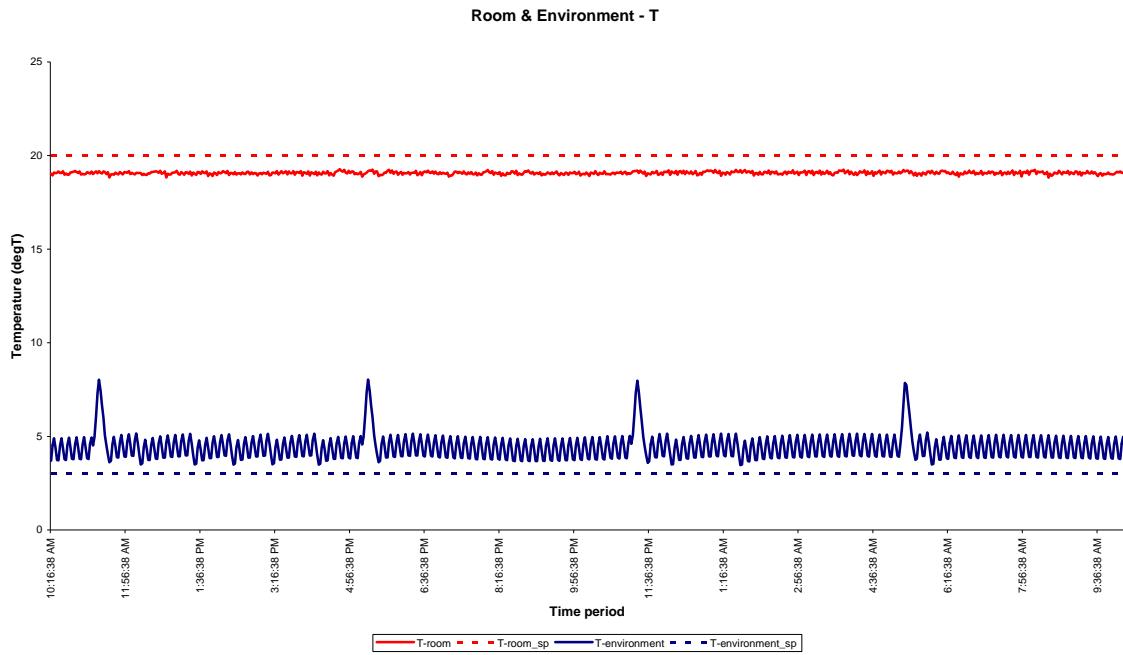


Figure B-8: Temperature of the room and environmental side during S1-Alt1

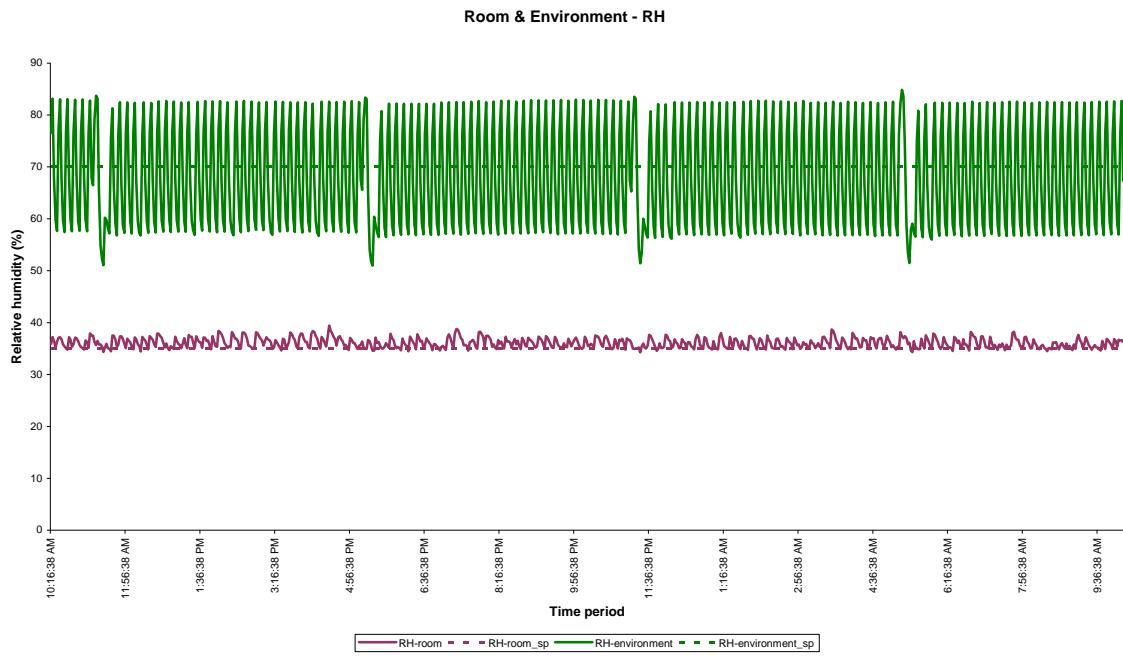


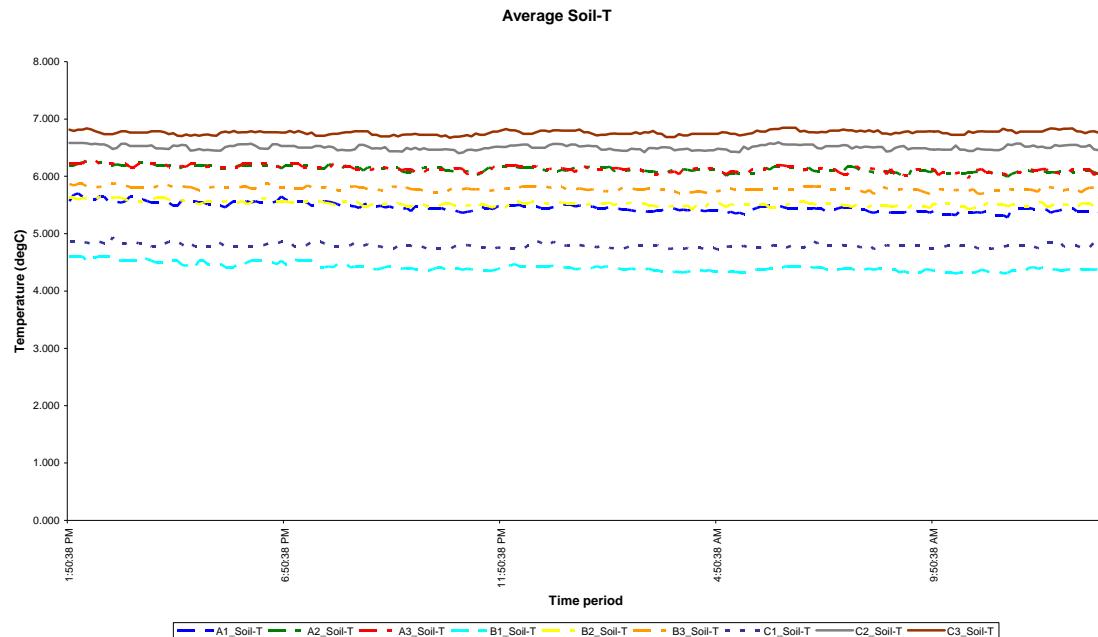
Figure B-9: Relative humidity of the room and environmental side during S1-Alt1

Test cycle: S1 – Alt2

Table B-2: Average data during the last 24 hours for each specimen of S1-Alt2

| Specimen Measurement Data | | | | | Control Loop Data | | | | | | | | | | | | | | | | | |
|---------------------------|--------------|-------------|-----------|--------------|-------------------|-----------------|------------------------|--------------------------------|-------------------|-------------------|-------------------|----------------------------|-------------------|-------------------|--|-------------------|--------------------------------|-------------------|--|--|--|--|
| B-G | A | | B | | C | | Sand | Environmental / Room Side | | | | | | | | | | | | | | |
| 1 | A1_Soil-T | 5.390 degC | B1_Soil-T | 4.357 degC | C1_Soil-T | 4.781 degC | 1 | T-room | 19.019 degC | Remarks | | | | | | | | | | | | |
| | A1_Soil-RH | 100.000 % | | B1_Soil-RH | 91.794 % | C1_Soil-RH | 99.904 % | RH-room | 60.795 % | Type: B-G | Soil type: Sand | | | | | | | | | | | |
| | A1_Wall-T | 15.665 degC | | B1_Wall-T | 6.959 degC | C1_Wall-T | 7.737 degC | T-room_sp | 20.000 degC | Damproofing: No | Alternative: Alt2 | | | | | | | | | | | |
| | A1_Ext-T | 6.693 degC | | B1_Ext-T | 5.742 degC | C1_Ext-T | 6.020 degC | RH-room_sp | 65.000 % | T-environment | | | | | | | | | | | | |
| | A1_Int-T | 17.281 degC | | B1_Int-T | 17.651 degC | C1_Int-T | 17.360 degC | RH-environment | 69.763 % | RH-environment | | | | | | | | | | | | |
| | A1_Inside-RH | 50.434 % | | B1_Inside-RH | 85.592 % | C1_Inside-RH | 83.122 % | T-environment_sp | 3.000 degC | T-environment_sp | | | | | | | | | | | | |
| | A1_Wall-RH | 55.896 % | | B1_Wall-RH | 82.890 % | C1_Wall-RH | 90.259 % | RH-environment_sp | 50.000 % | RH-environment_sp | | | | | | | | | | | | |
| | A2_Soil-T | 6.076 degC | B2_Soil-T | 5.492 degC | C2_Soil-T | 6.501 degC | 2 | Legend | | | | | Remarks | | | | | | | | | |
| | A2_Soil-RH | 100.000 % | | B2_Soil-RH | 100.000 % | C2_Soil-RH | 100.000 % | T - Temperature (degC) | Soil type: Sand | | | | | Damproofing: No | | | | | | | | |
| | A2_Wall-T | 16.298 degC | | B2_Wall-T | 8.119 degC | C2_Ext-T | 11.206 degC | RH - Relative Humidity (%) | Alternative: Alt2 | | | | | T-environment | | | | | | | | |
| | A2_Ext-T | 7.525 degC | | B2_Ext-T | 6.791 degC | C2_Int-T | 16.007 degC | SP - Setpoint (either T or RH) | RH-environment | | | | | RH-environment_sp | | | | | | | | |
| | A2_Int-T | 17.214 degC | | B2_Int-T | 17.940 degC | C2_Inside-RH | 77.572 degC | RH-environment_sp | | | | | RH-environment_sp | | | | | | | | | |
| | A2_Inside-RH | 59.132 % | | B2_Inside-RH | 86.633 % | Remarks | | | | | Remarks | | | | | Remarks | | | | | | |
| | A2_Wall-RH | 58.940 % | | B2_Wall-RH | 96.624 % | Soil type: Sand | | | | | Damproofing: No | | | | | Alternative: Alt2 | | | | | | |
| | A3_Soil-T | 6.086 degC | B3_Soil-T | 5.764 degC | C3_Soil-T | 6.780 degC | 3 | T-environment | | | | | RH-environment | | | | | RH-environment_sp | | | | |
| | A3_Soil-RH | 100.000 % | | B3_Soil-RH | 100.000 % | C3_Soil-RH | 100.000 % | SP - Setpoint (either T or RH) | | | | | RH-environment_sp | | | | | RH-environment_sp | | | | |
| | A3_Wall-T | 16.318 degC | | B3_Wall-T | 8.674 degC | C3_Ext-T | 12.344 degC | RH-environment_sp | | | | | RH-environment_sp | | | | | RH-environment_sp | | | | |
| | A3_Ext-T | 7.694 degC | | B3_Ext-T | 6.900 degC | C3_Int-T | 14.908 degC | RH-environment_sp | | | | | RH-environment_sp | | | | | RH-environment_sp | | | | |
| | A3_Int-T | 17.361 degC | | B3_Int-T | 17.766 degC | C3_Inside-RH | 99.999 degC | RH-environment_sp | | | | | RH-environment_sp | | | | | RH-environment_sp | | | | |
| | A3_Inside-RH | 58.569 % | | B3_Inside-RH | 84.735 % | Remarks | | | | | Remarks | | | | | Remarks | | | | | | |
| | A3_Wall-RH | 62.297 % | | B3_Wall-RH | 99.838 % | Soil type: Sand | | | | | Damproofing: No | | | | | Alternative: Alt2 | | | | | | |
| No | A | | B | | C | | T - Temperature (degC) | | | | | RH - Relative Humidity (%) | | | | | SP - Setpoint (either T or RH) | | | | | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-10: Average soil temperature of S1-Alt2

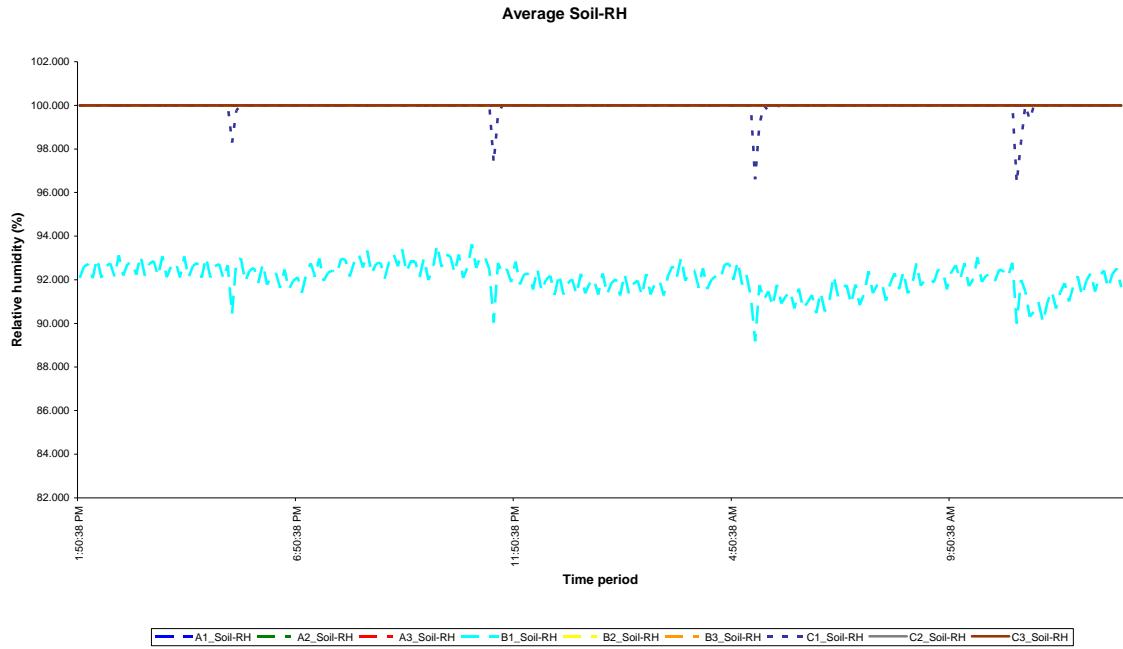


Figure B-11: Average soil relative humidity of S1-Alt2

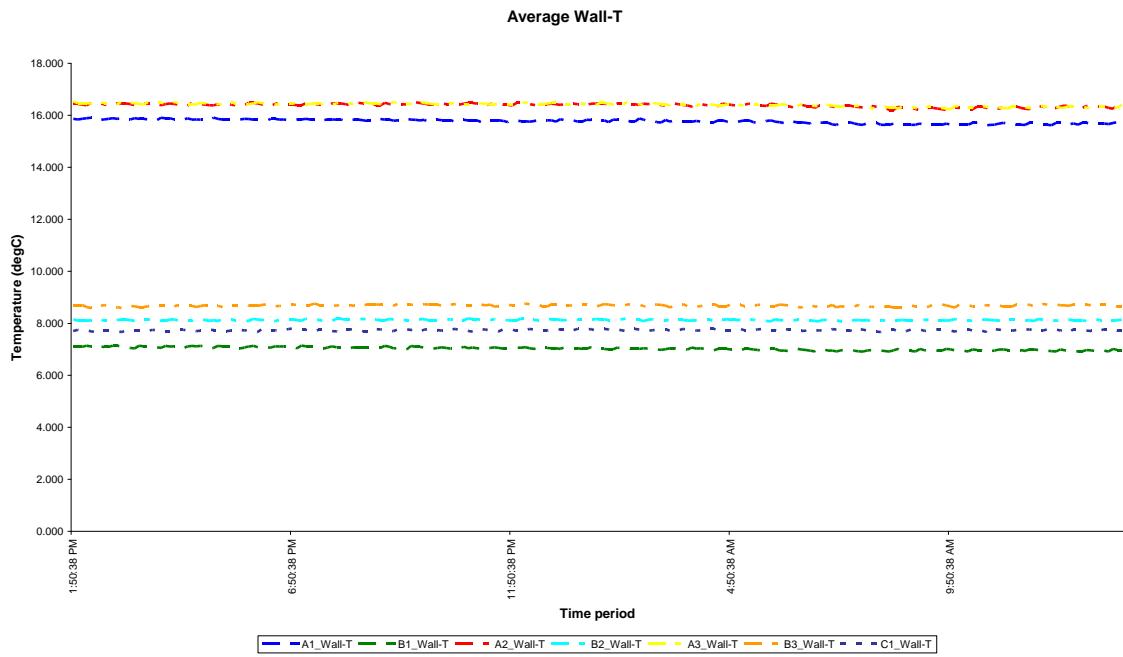


Figure B-12: Average wall temperature of S1-Alt2

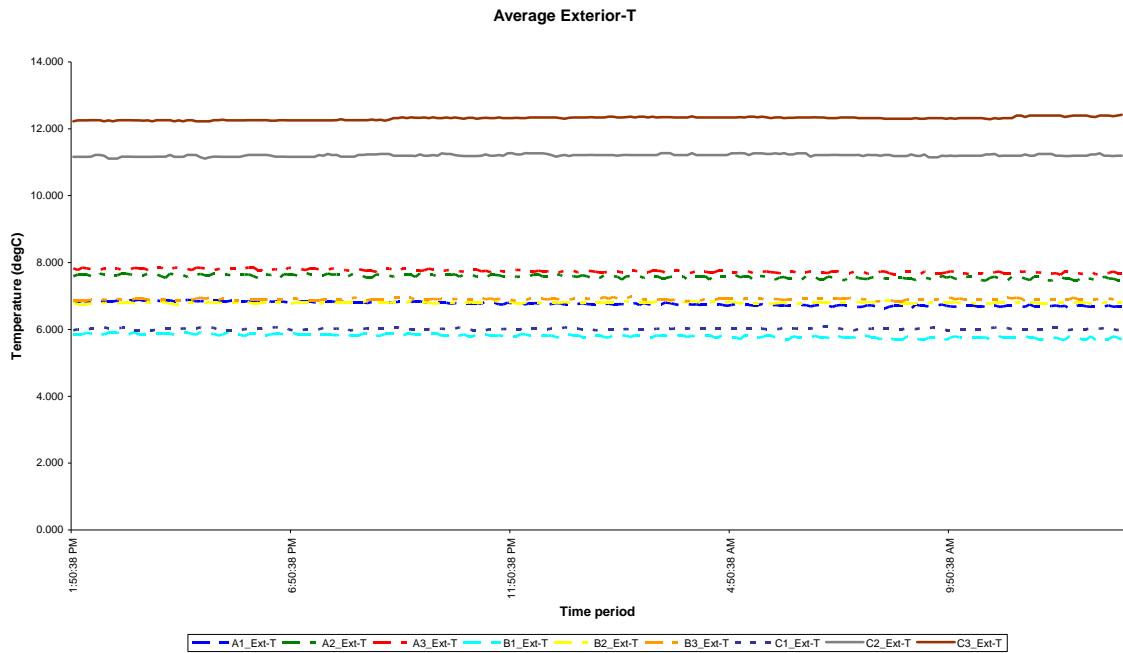


Figure B-13: Average exterior temperature of S1-Alt2

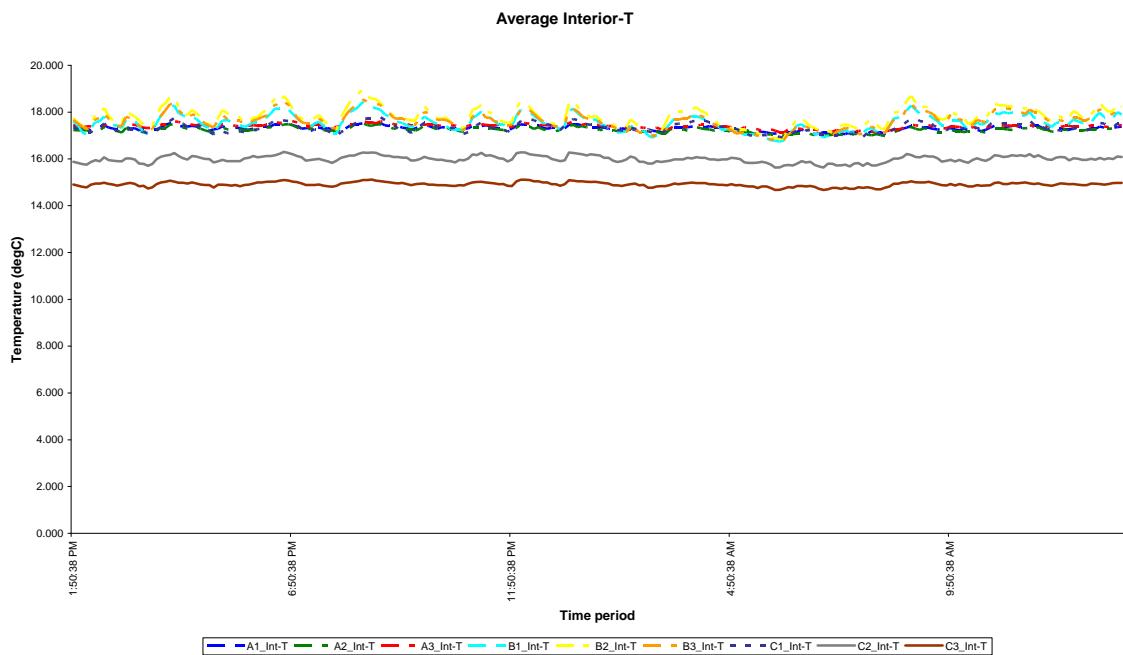


Figure B-14: Average interior temperature of S1-Alt2

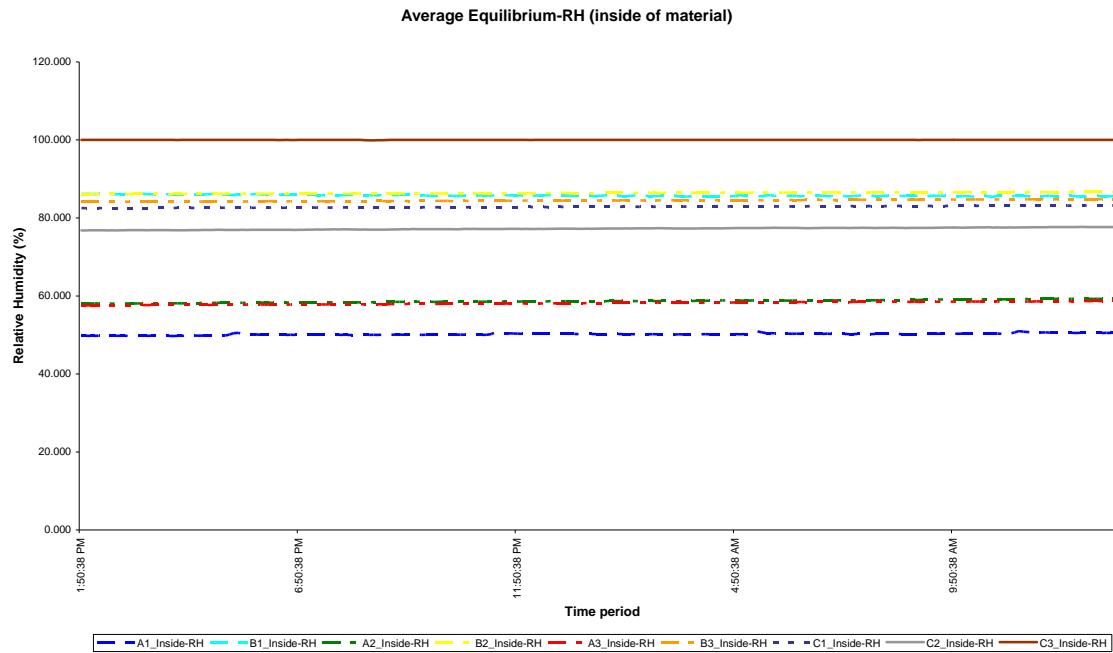


Figure B-15: Average equilibrium of relative humidity in a cavity of S1-Alt2

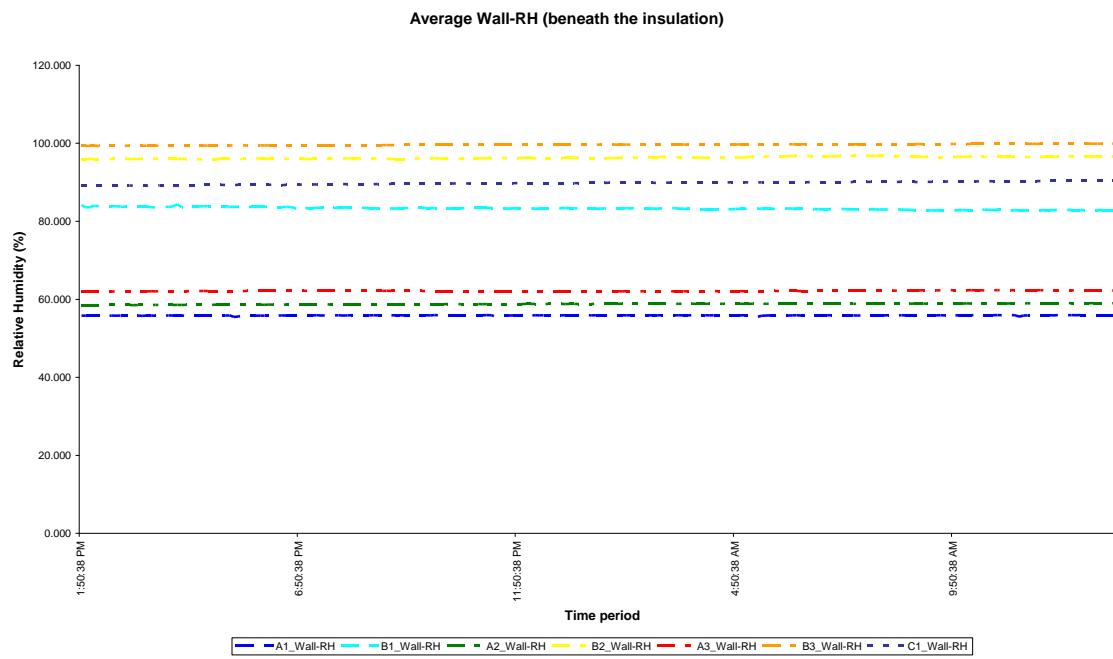


Figure B-16: Average wall relative humidity beneath the insulation of S1-Alt2

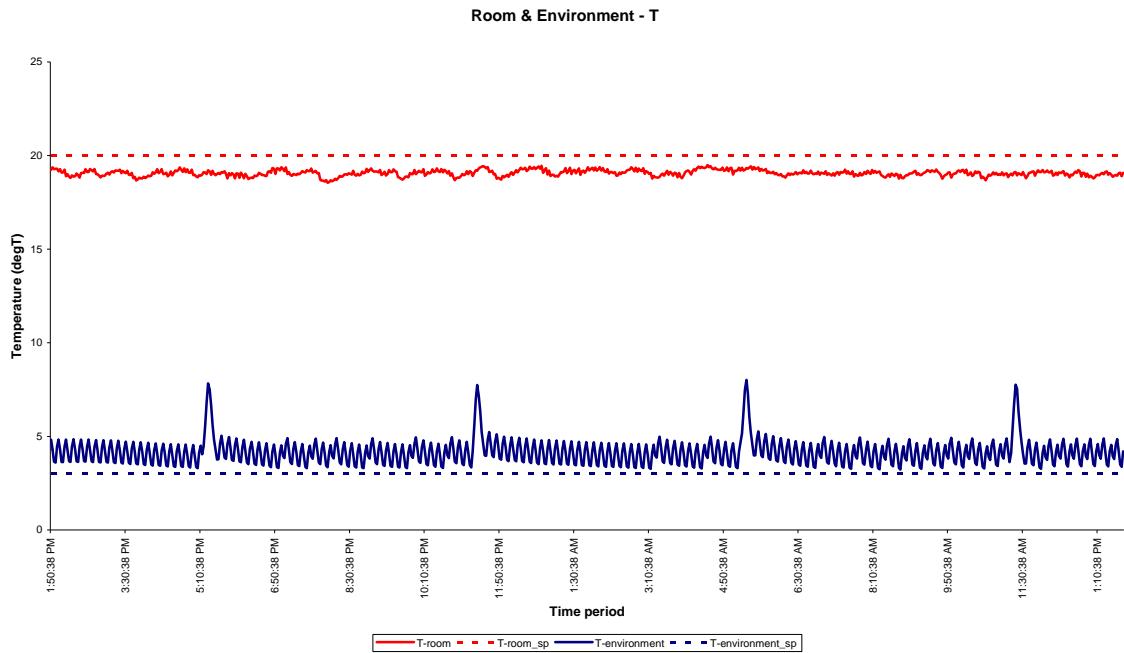


Figure B-17: Temperature of the room and environmental side during S1-Alt2

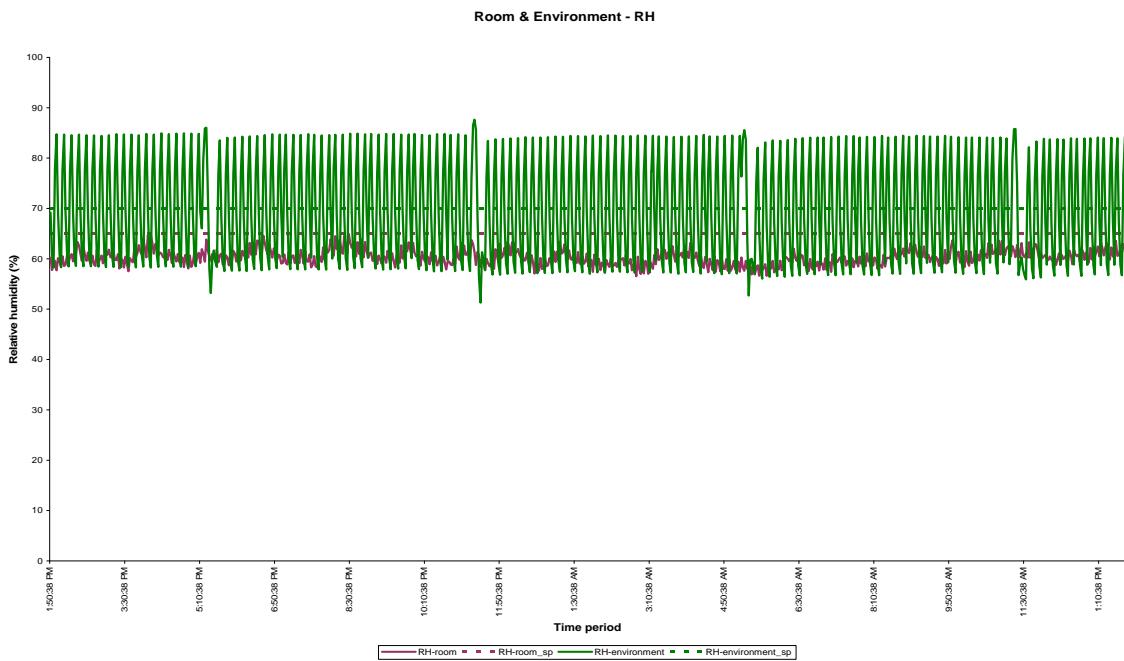
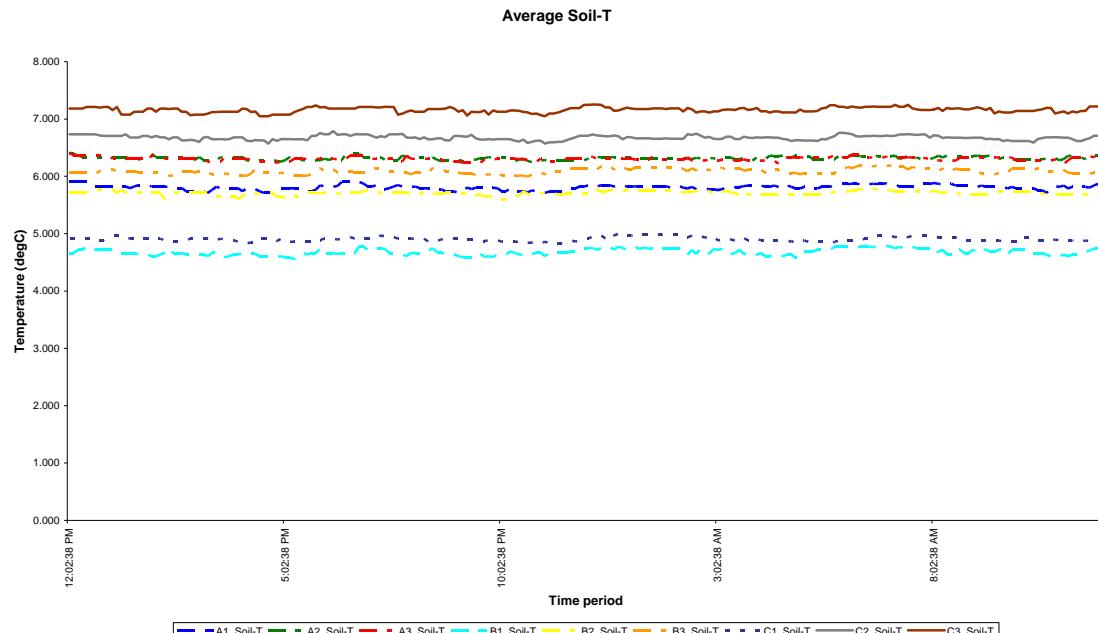


Figure B-18: Relative humidity of the room and environmental side during S1-Alt2

Test cycle: **S1 – Alt3**
Table B-3: Average data during the last 24 hours for each specimen of S1-Alt3

| Specimen Measurement Data | | | | Control Loop Data |
|---------------------------|--|--|--|-------------------|
| B-G | A | B | C | Sand |
| 1 | A1_Soil-T 5.831 degC A1_Soil-RH 100.000 % A1_Wall-T 16.271 degC A1_Ext-T 7.224 degC A1_Int-T 17.864 degC A1_Inside-RH 52.142 % A1_Wall-RH 56.753 % | B1_Soil-T 4.709 degC B1_Soil-RH 100.000 % B1_Wall-T 7.361 degC B1_Ext-T 6.062 degC B1_Int-T 18.380 degC B1_Inside-RH 85.840 % B1_Wall-RH 83.484 % | C1_Soil-T 4.907 degC C1_Soil-RH 95.199 % C1_Wall-T 8.180 degC C1_Ext-T 6.315 degC C1_Int-T 18.175 degC C1_Inside-RH 85.563 % C1_Wall-RH 93.995 % | 1 |
| 2 | A2_Soil-T 6.334 degC A2_Soil-RH 100.000 % A2_Wall-T 17.041 degC A2_Ext-T 7.817 degC A2_Int-T 17.947 degC A2_Inside-RH 62.665 % A2_Wall-RH 60.229 % | B2_Soil-T 5.720 degC B2_Soil-RH 100.000 % B2_Wall-T 8.514 degC B2_Ext-T 7.111 degC B2_Int-T 18.711 degC B2_Inside-RH 88.974 % B2_Wall-RH 98.249 % | C2_Soil-T 6.680 degC C2_Soil-RH 100.000 % C2_Ext-T 11.909 degC C2_Int-T 16.818 degC C2_Inside-RH 80.465 degC | 2 |
| 3 | A3_Soil-T 6.315 degC A3_Soil-RH 100.000 % A3_Wall-T 17.024 degC A3_Ext-T 7.905 degC A3_Int-T 18.067 degC A3_Inside-RH 61.942 % A3_Wall-RH 61.034 % | B3_Soil-T 6.115 degC B3_Soil-RH 100.000 % B3_Wall-T 9.159 degC B3_Ext-T 7.303 degC B3_Int-T 18.538 degC B3_Inside-RH 87.476 % B3_Wall-RH 100.000 % | C3_Soil-T 7.175 degC C3_Soil-RH 100.000 % C3_Ext-T 13.119 degC C3_Int-T 15.923 degC C3_Inside-RH 100.000 degC | 3 |
| No | A | B | C | Alt3 |

* Measured pressure difference between Room Side & Environmental Side


Figure B-19: Average soil temperature of S1-Alt3

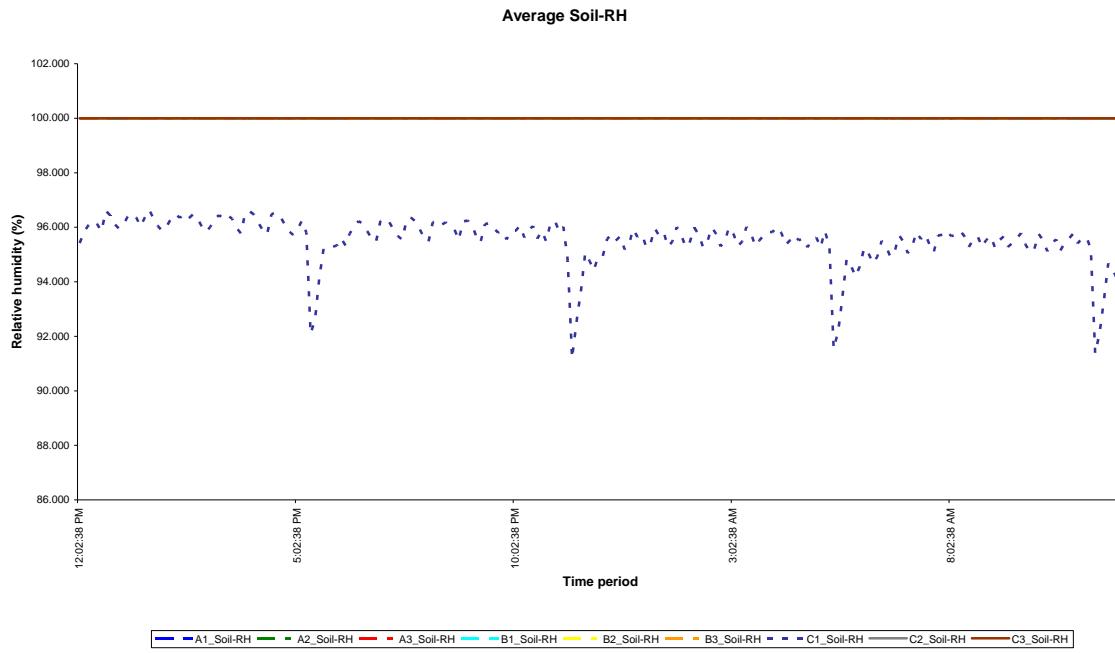


Figure B-20: Average soil relative humidity of S1-Alt3

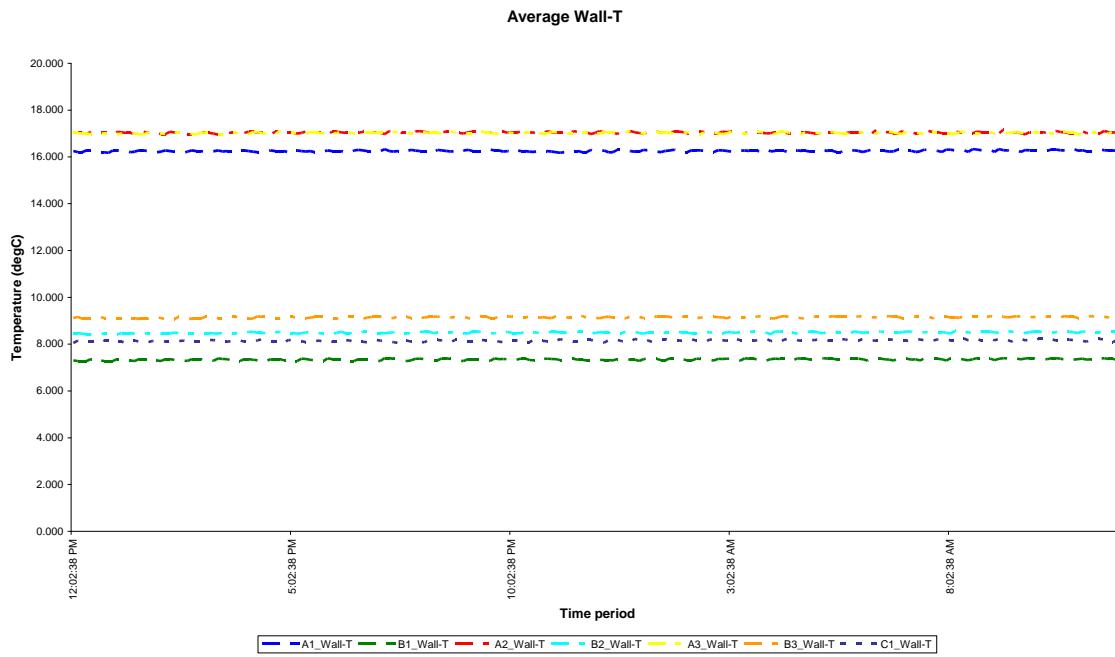


Figure B-21: Average wall temperature of S1-Alt3

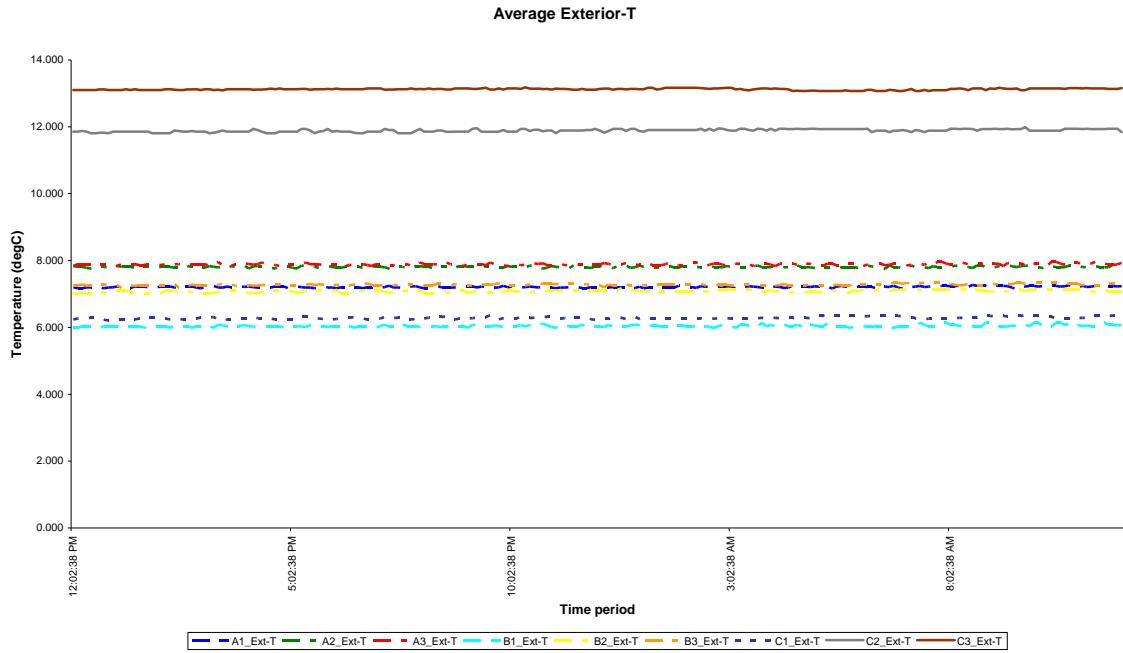


Figure B-22: Average exterior temperature of S1-Alt3

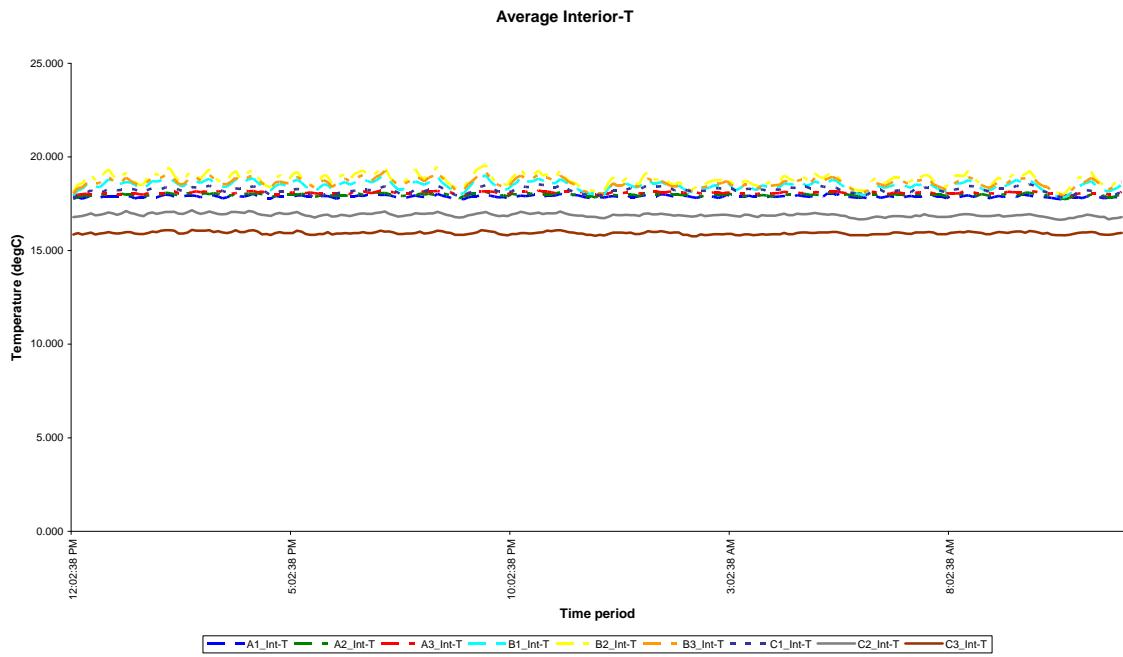


Figure B-23: Average interior temperature of S1-Alt3

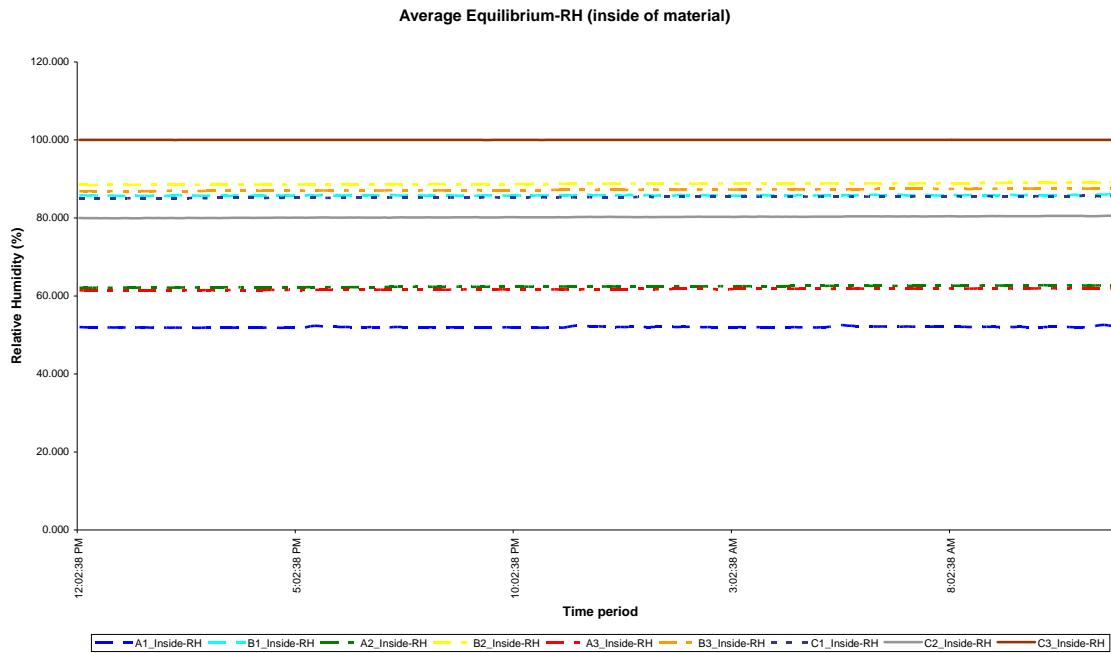


Figure B-24: Average equilibrium of relative humidity in a cavity of S1-Alt3

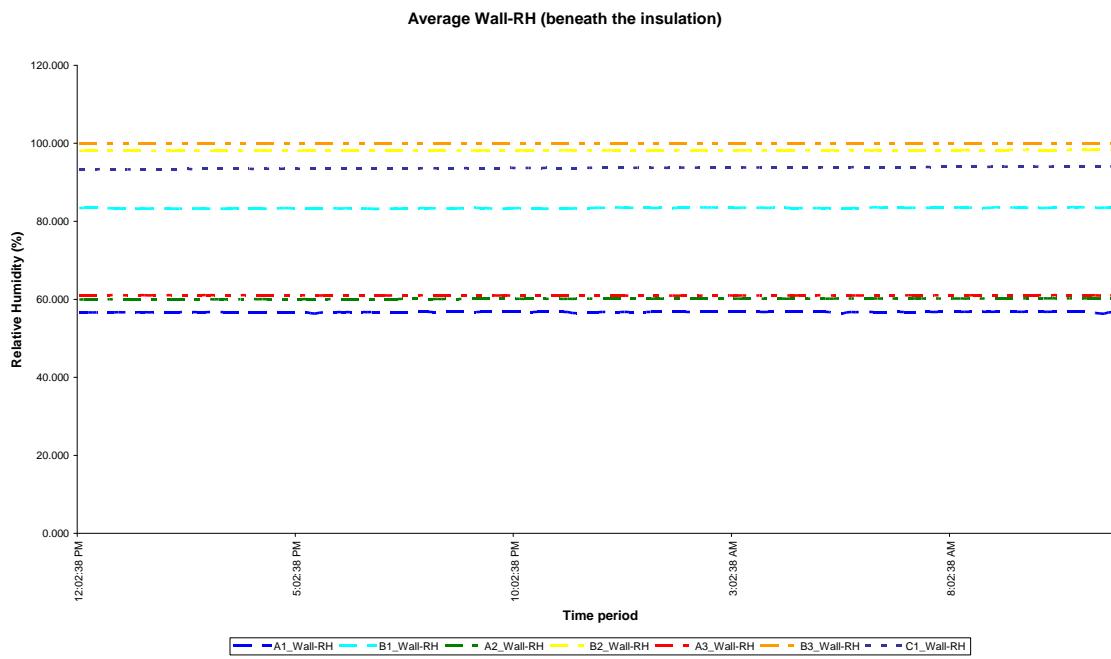


Figure B-25: Average wall relative humidity beneath the insulation of S1-Alt3

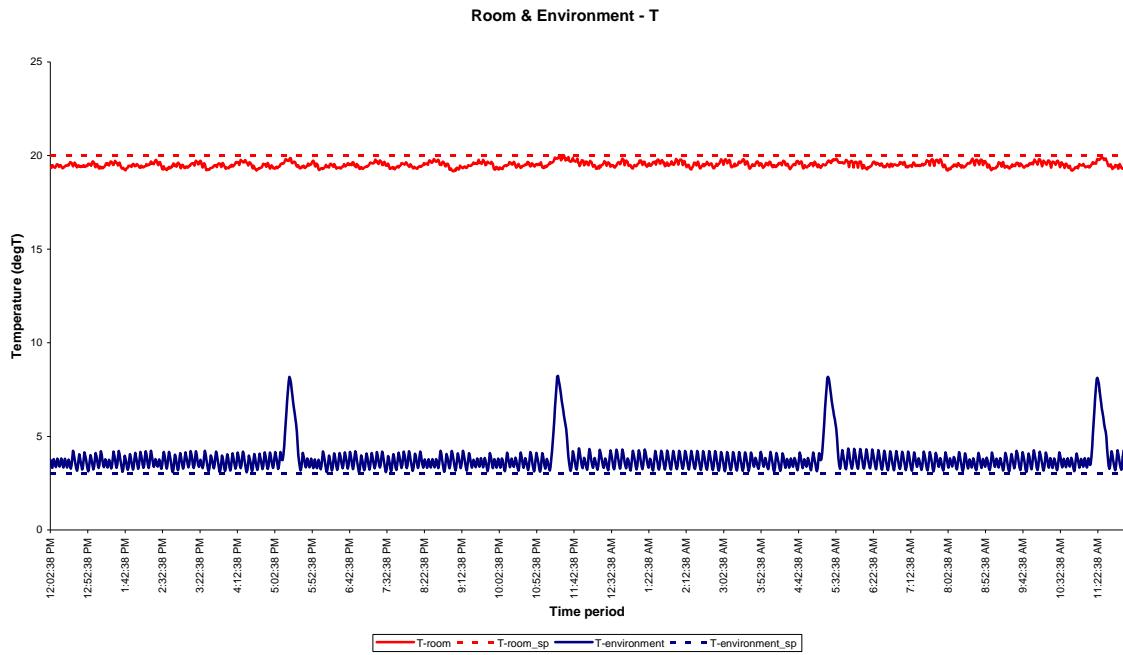


Figure B-26: Temperature of the room and environmental side during S1-Alt3

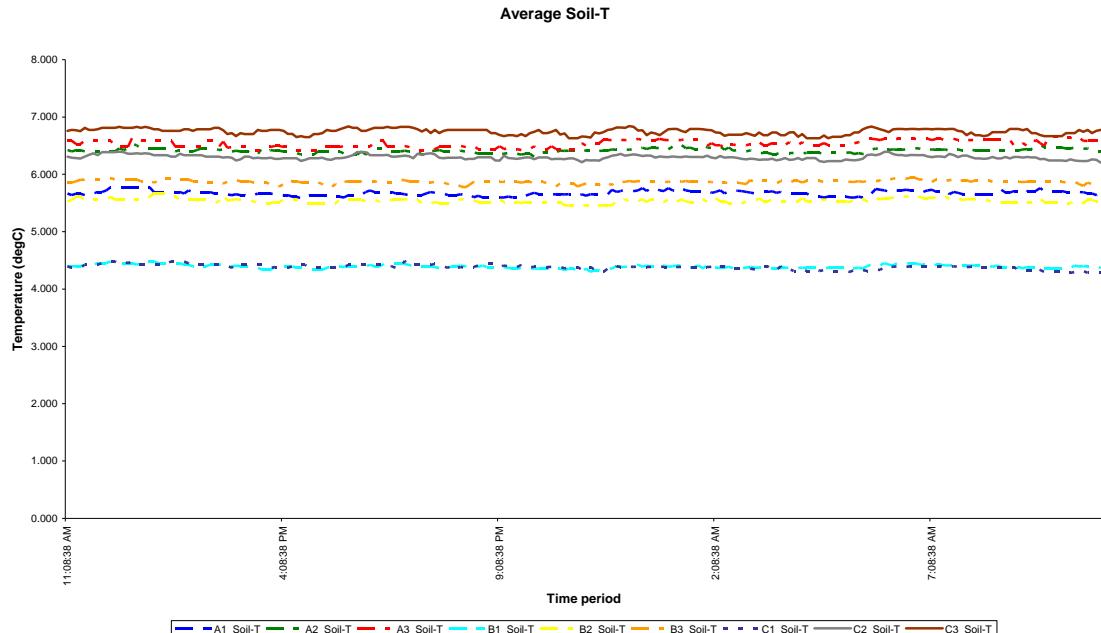


Figure B-27: Relative humidity of the room and environmental side during S1-Alt3

Test cycle: **S1 – Alt4**
Table B-4: Average data during the last 24 hours for each specimen of S1-Alt4

| Specimen Measurement Data | | | | Control Loop Data | |
|---------------------------|--|---|---|-------------------|--|
| B-G | A | B | C | Sand | |
| 1 | A1_Soil-T 5.687 degC A1_Soil-RH 100.000 % A1_Wall-T 15.742 degC A1_Ext-T 7.022 degC A1_Int-T 17.740 degC A1_Inside-RH 46.459 % A1_Wall-RH 56.697 % | B1_Soil-T 4.397 degC B1_Soil-RH 99.381 % B1_Wall-T 6.847 degC B1_Ext-T 5.676 degC B1_Int-T 17.765 degC B1_Inside-RH 84.557 % B1_Wall-RH 78.799 % | C1_Soil-T 4.350 degC C1_Soil-RH 100.000 % C1_Wall-T 7.095 degC C1_Ext-T 5.448 degC C1_Int-T 16.585 degC C1_Inside-RH 86.613 % C1_Wall-RH 86.872 % | 1 | |
| 2 | A2_Soil-T 6.427 degC A2_Soil-RH 100.000 % A2_Wall-T 16.766 degC A2_Ext-T 7.903 degC A2_Int-T 17.684 degC A2_Inside-RH 59.535 % A2_Wall-RH 60.399 % | B2_Soil-T 5.551 degC B2_Soil-RH 100.000 % B2_Wall-T 8.129 degC B2_Ext-T 6.833 degC B2_Int-T 18.090 degC B2_Inside-RH 90.079 % B2_Wall-RH 96.658 % | C2_Soil-T 6.292 degC C2_Soil-RH 100.000 % C2_Ext-T 11.258 degC C2_Int-T 16.031 degC C2_Inside-RH 79.321 degC | 2 | |
| 3 | A3_Soil-T 6.591 degC A3_Soil-RH 100.000 % A3_Wall-T 16.782 degC A3_Ext-T 8.042 degC A3_Int-T 17.822 degC A3_Inside-RH 58.777 % A3_Wall-RH 62.377 % | B3_Soil-T 5.882 degC B3_Soil-RH 100.000 % B3_Wall-T 8.334 degC B3_Ext-T 6.751 degC B3_Int-T 17.778 degC B3_Inside-RH 89.456 % B3_Wall-RH 94.315 % | C3_Soil-T 6.746 degC C3_Soil-RH 100.000 % C3_Ext-T 12.562 degC C3_Int-T 15.181 degC C3_Inside-RH 100.000 degC | 3 | |
| No | A | B | C | Alt4 | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-28: Average soil temperature of S1-Alt4

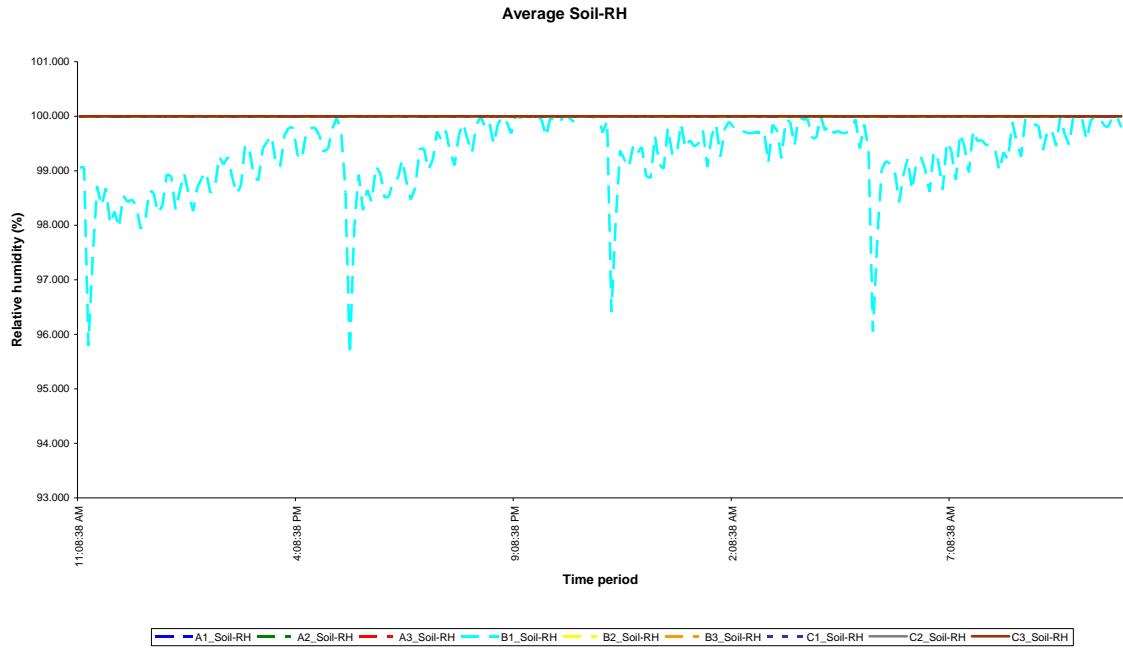


Figure B-29: Average soil relative humidity of S1-Alt4

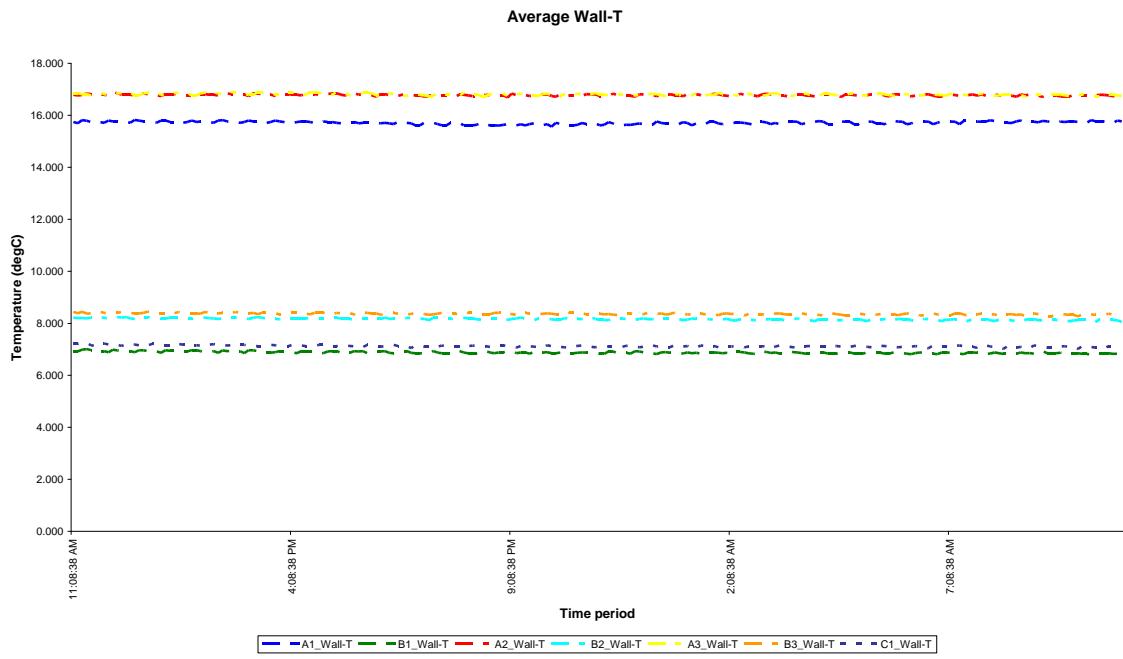


Figure B-30: Average wall temperature of S1-Alt4

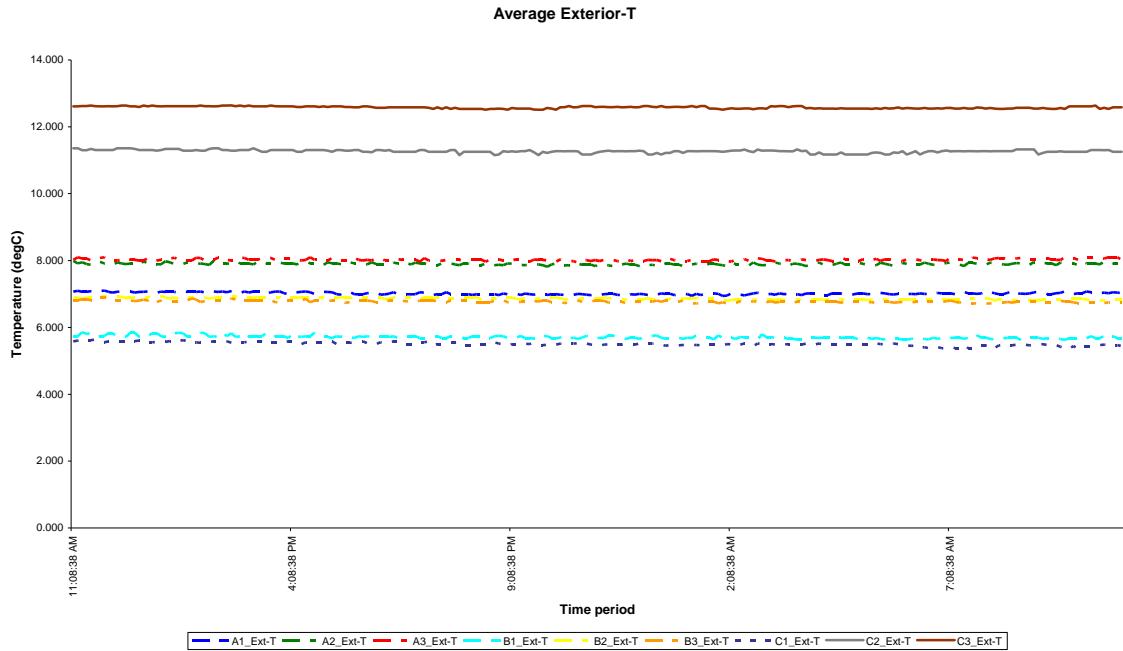


Figure B-31: Average exterior temperature of S1-Alt4

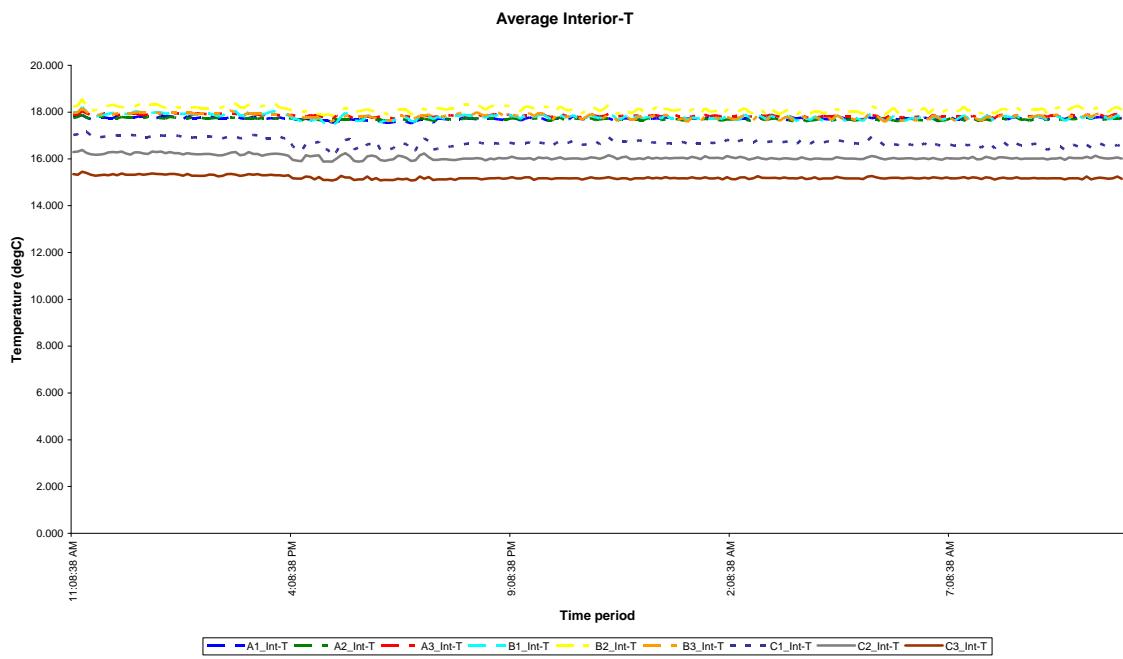


Figure B-32: Average interior temperature of S1-Alt4

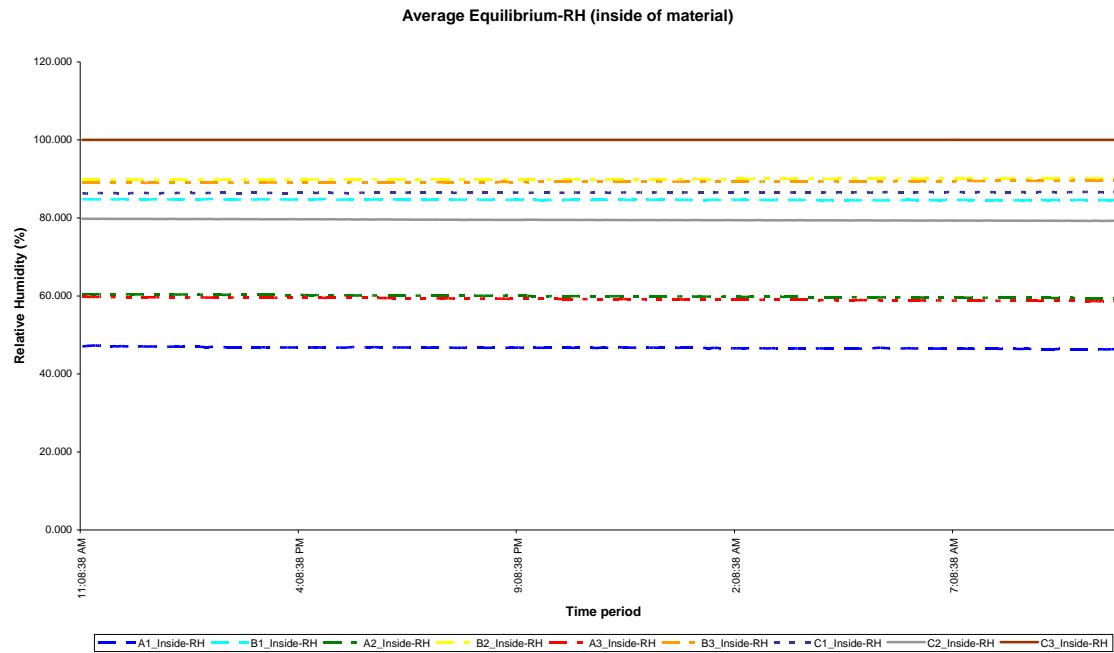


Figure B-33: Average equilibrium of relative humidity in a cavity of S1-Alt4

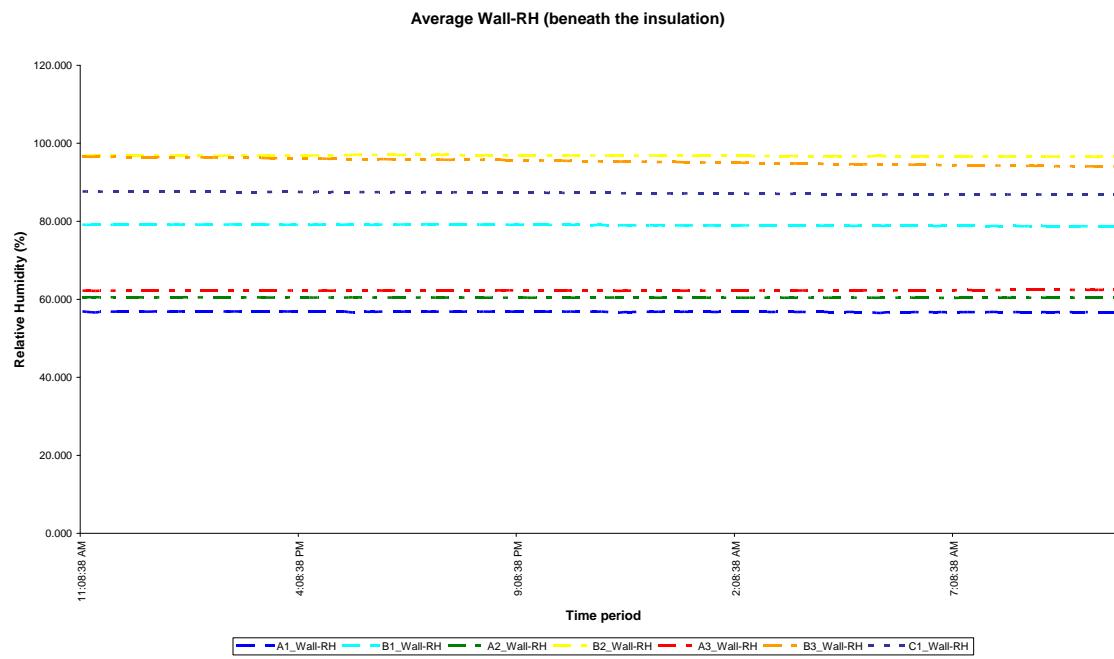


Figure B-34: Average wall relative humidity beneath the insulation of S1-Alt4

Insulated Concrete Masonry Below-grade Walls

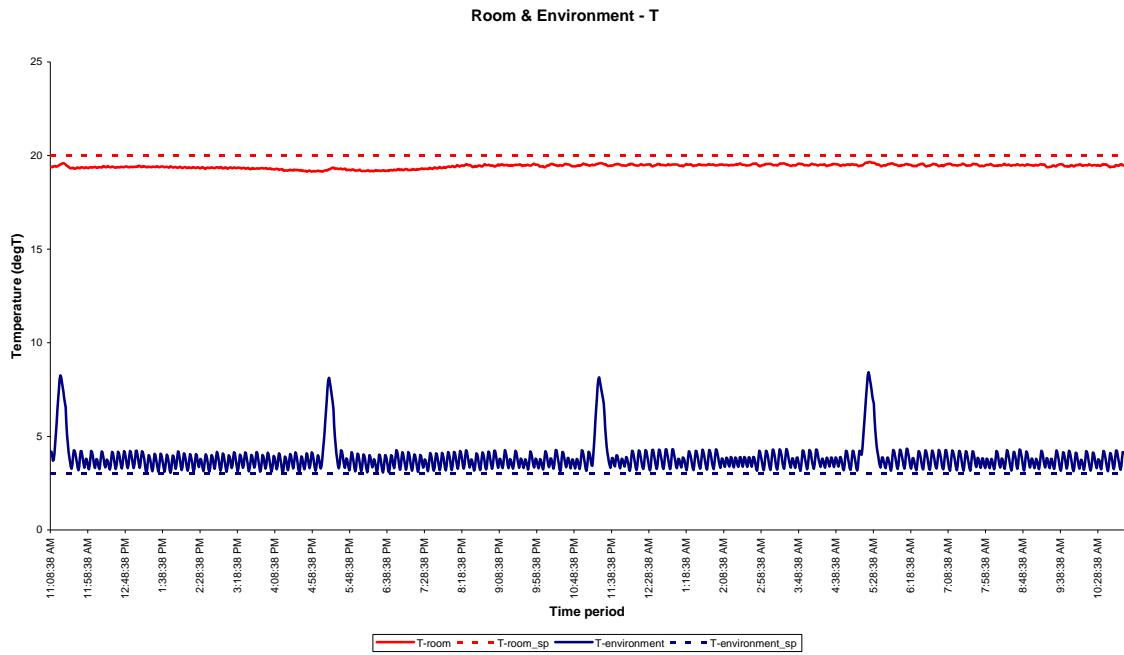


Figure B-35: Temperature of the room and environmental side during S1-Alt4

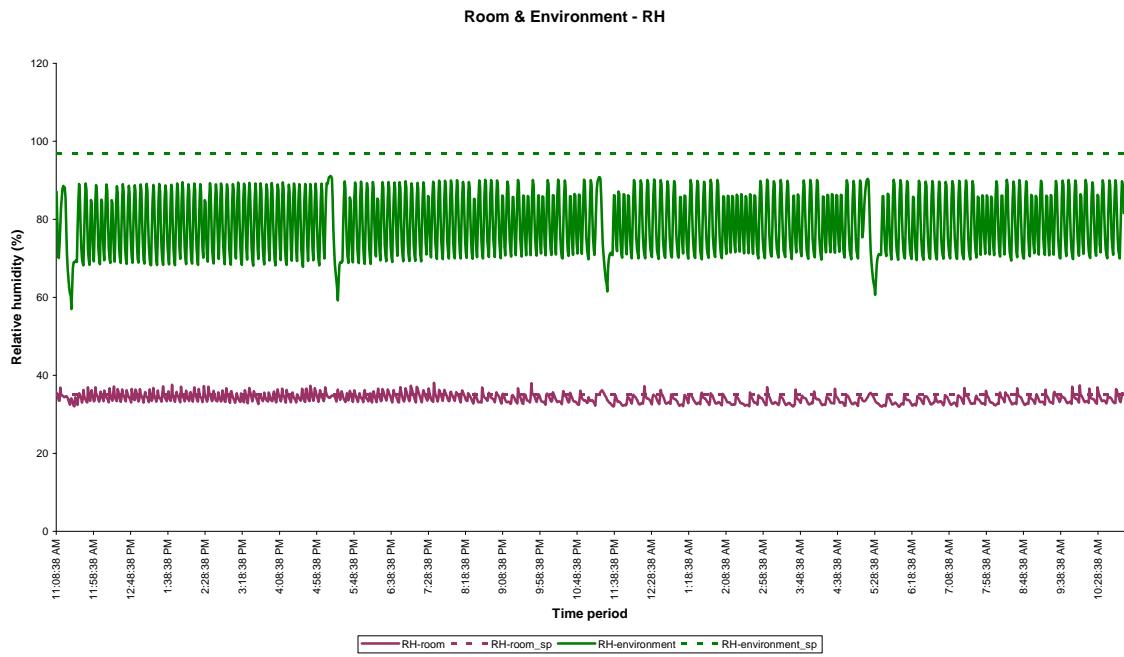
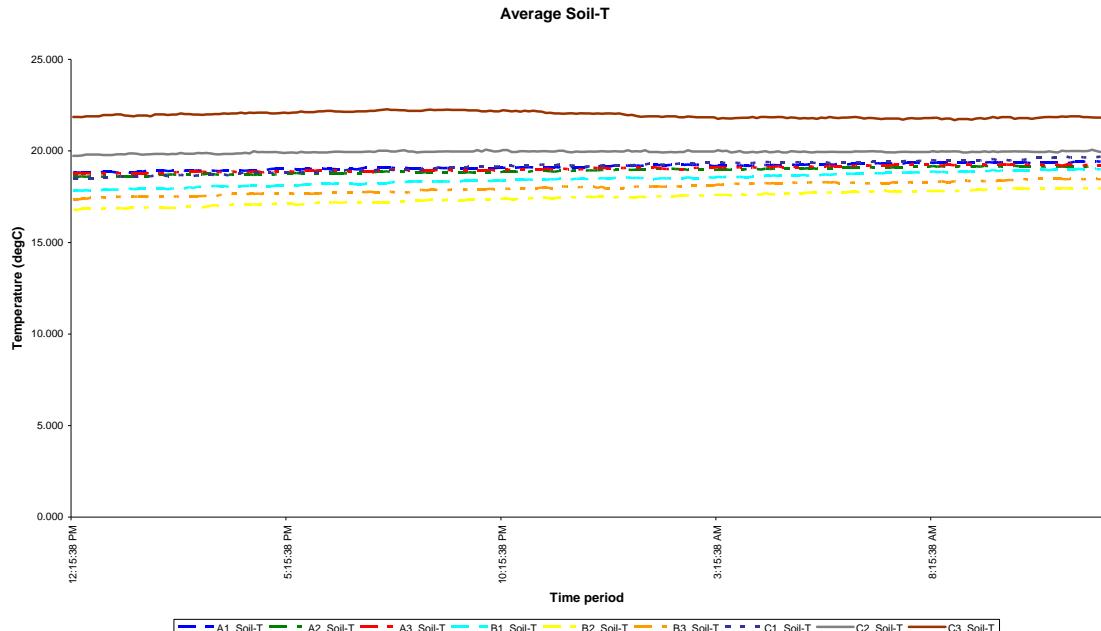


Figure B-36: Relative humidity of the room and environmental side during S1-Alt4

Test cycle: **S1 – Alt5**
Table B-5: Average data during the last 24 hours for each specimen of S1-Alt5

| Specimen Measurement Data | | | | Control Loop Data | |
|---------------------------|--|--|--|-------------------|--|
| B-G | A | B | C | Sand | |
| 1 | A1_Soil-T 19.355 degC A1_Soil-RH 100.000 % A1_Wall-T 19.873 degC A1_Ext-T 19.526 degC A1_Int-T 19.768 degC A1_Inside-RH 56.747 % A1_Wall-RH 66.354 % | B1_Soil-T 18.883 degC B1_Soil-RH 94.595 % B1_Wall-T 18.223 degC B1_Ext-T 18.025 degC B1_Int-T 19.786 degC B1_Inside-RH 86.183 % B1_Wall-RH 73.578 % | C1_Soil-T 19.514 degC C1_Soil-RH 100.000 % C1_Wall-T 19.544 degC C1_Ext-T 19.171 degC C1_Int-T 20.242 degC C1_Inside-RH 87.626 % C1_Wall-RH 79.176 % | 1 | |
| 2 | A2_Soil-T 19.141 degC A2_Soil-RH 100.000 % A2_Wall-T 19.458 degC A2_Ext-T 19.238 degC A2_Int-T 19.320 degC A2_Inside-RH 59.274 % A2_Wall-RH 72.951 % | B2_Soil-T 17.874 degC B2_Soil-RH 100.000 % B2_Wall-T 17.090 degC B2_Ext-T 16.888 degC B2_Int-T 19.641 degC B2_Inside-RH 90.710 % B2_Wall-RH 94.291 % | C2_Soil-T 19.961 degC C2_Soil-RH 100.000 % C2_Ext-T 20.206 degC C2_Int-T 20.170 degC C2_Inside-RH 78.106 degC | 2 | |
| 3 | A3_Soil-T 19.230 degC A3_Soil-RH 100.000 % A3_Wall-T 19.558 degC A3_Ext-T 18.981 degC A3_Int-T 19.425 degC A3_Inside-RH 59.940 % A3_Wall-RH 88.533 % | B3_Soil-T 18.360 degC B3_Soil-RH 100.000 % B3_Wall-T 17.498 degC B3_Ext-T 17.364 degC B3_Int-T 19.617 degC B3_Inside-RH 89.458 % B3_Wall-RH 66.152 % | C3_Soil-T 21.799 degC C3_Soil-RH 100.000 % C3_Ext-T 21.014 degC C3_Int-T 20.384 degC C3_Inside-RH 100.000 degC | 3 | |
| No | A | B | C | Alt5 | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-37: Average soil temperature of S1-Alt5

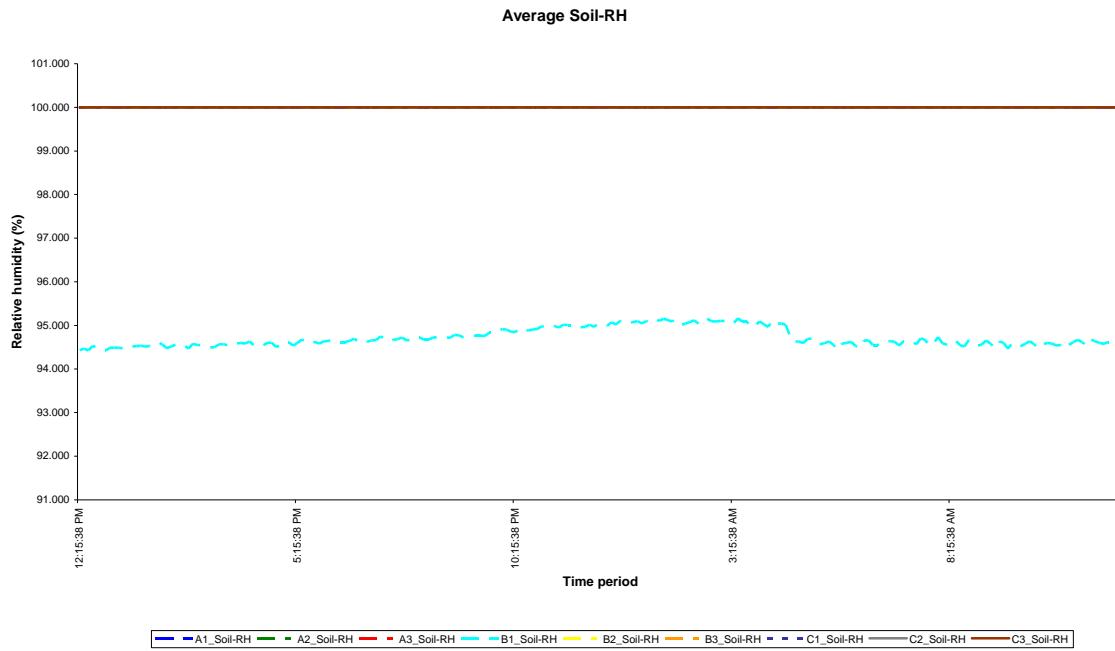


Figure B-38: Average soil relative humidity of S1-Alt5

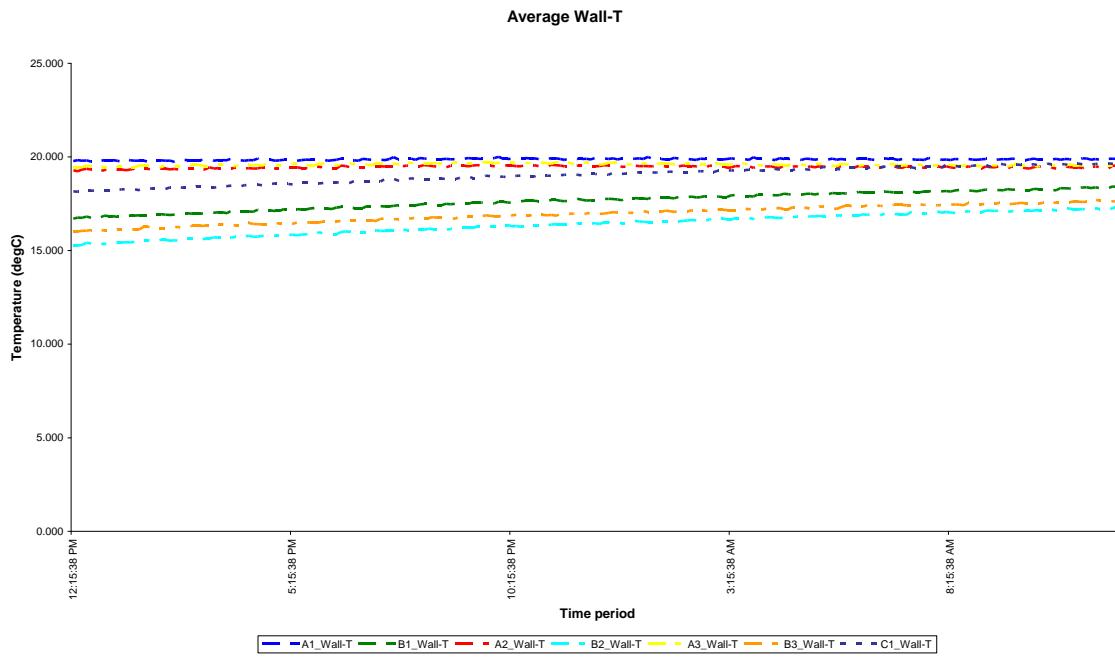


Figure B-39: Average wall temperature of S1-Alt5

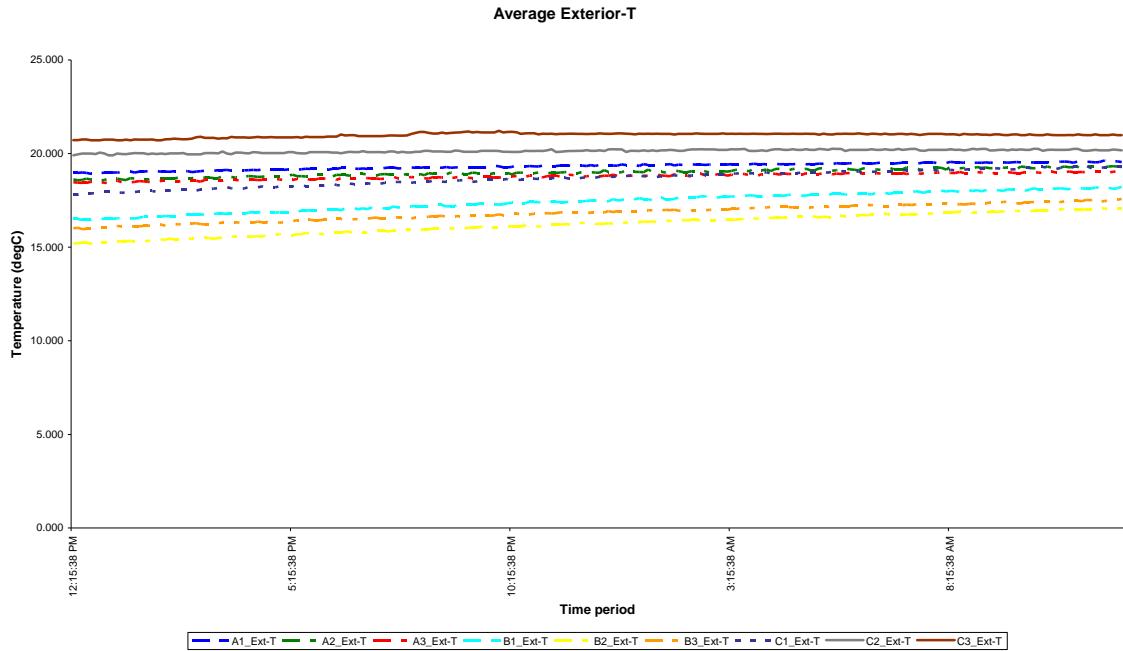


Figure B-40: Average exterior temperature of S1-Alt5



Figure B-41: Average interior temperature of S1-Alt5

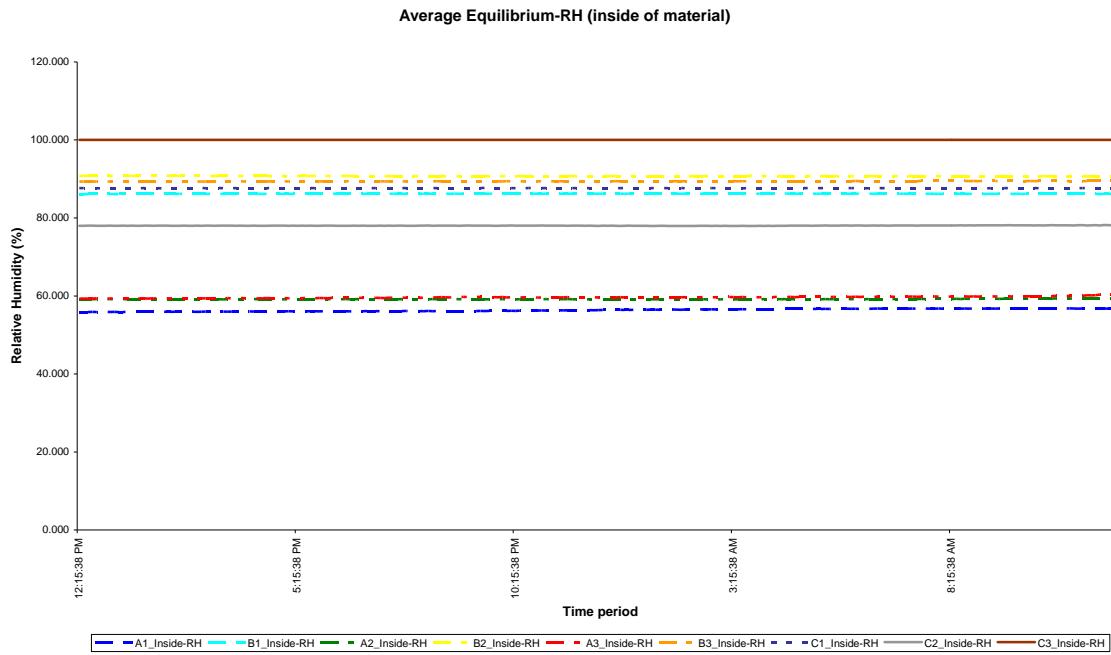


Figure B-42: Average equilibrium of relative humidity in a cavity of S1-Alt5

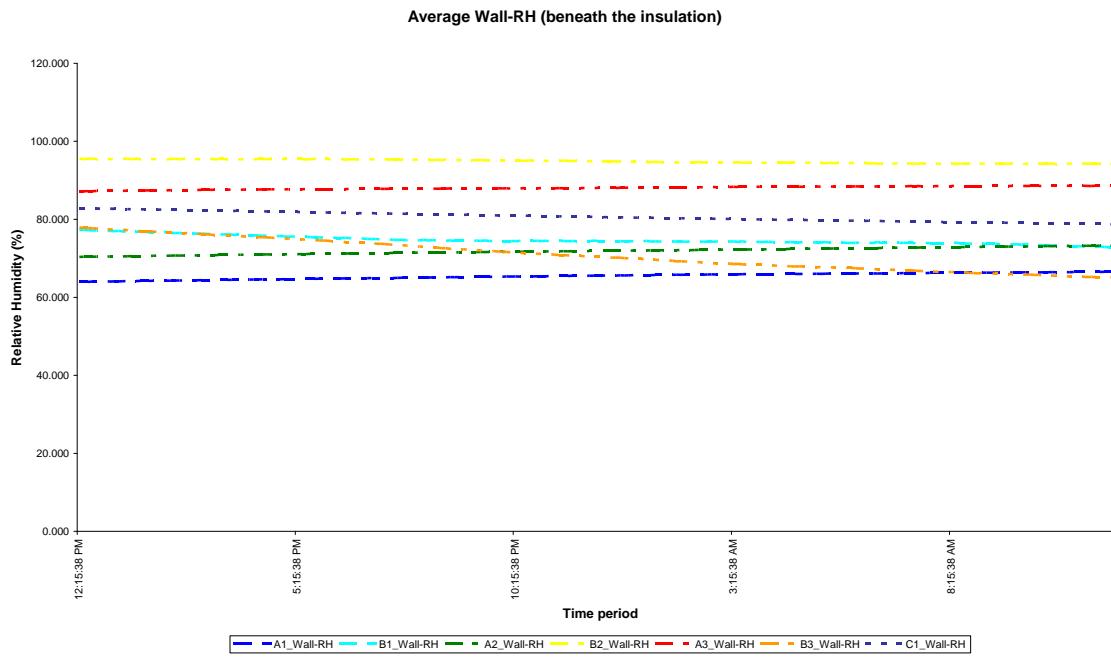


Figure B-43: Average wall relative humidity beneath the insulation of S1-Alt5

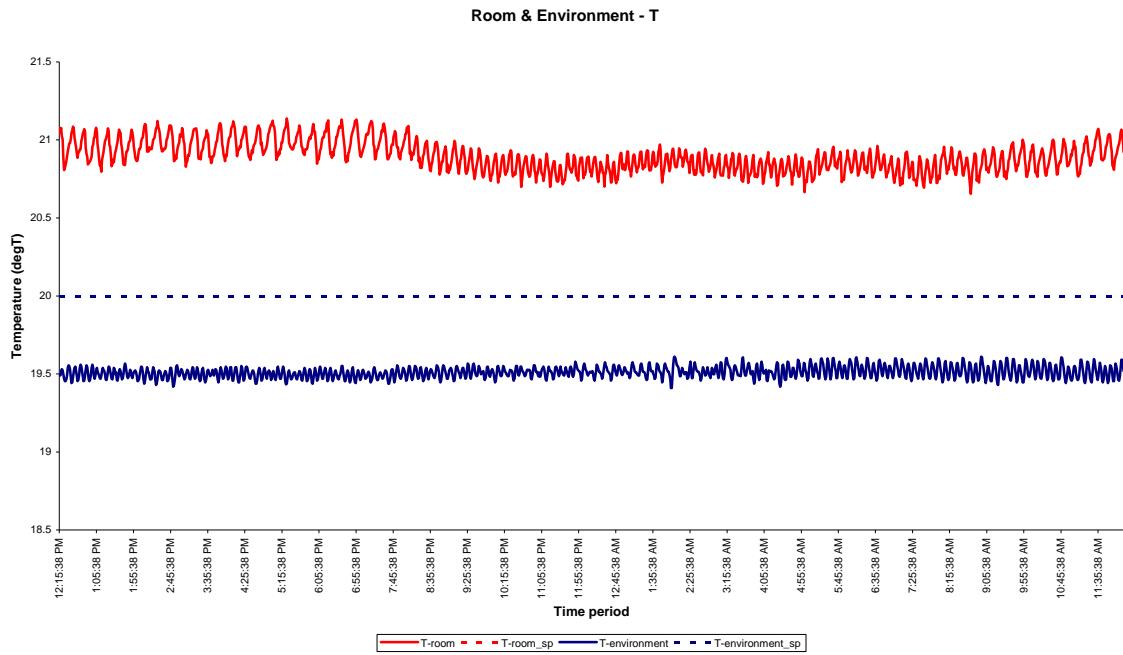


Figure B-44: Temperature of the room and environmental side during S1-Alt5

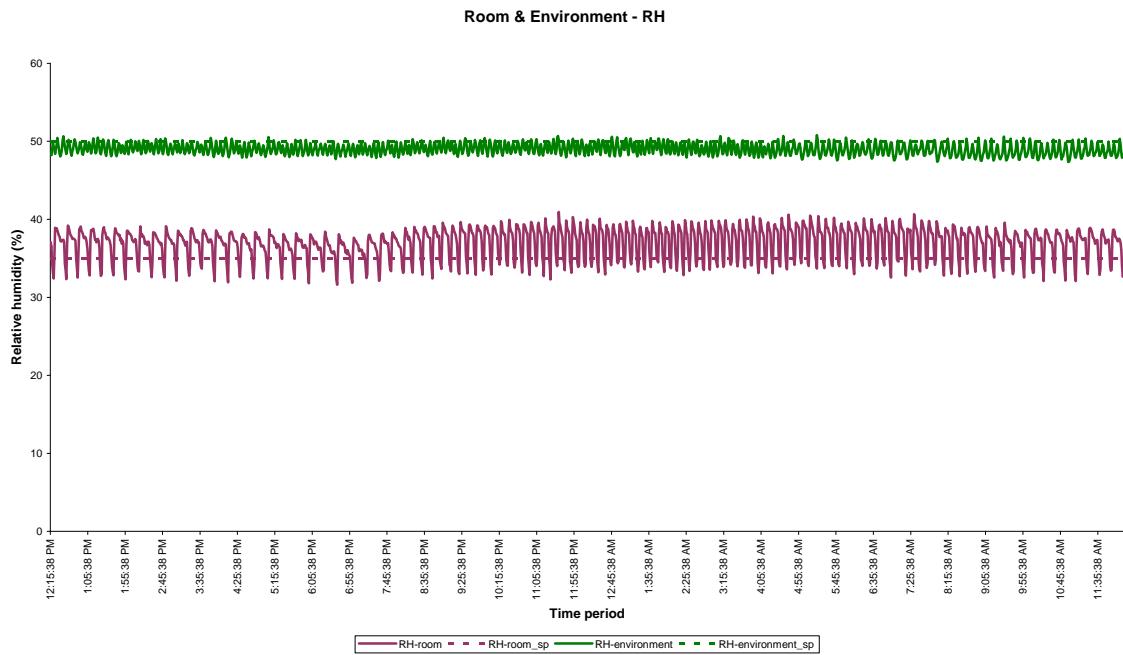


Figure B-45: Relative humidity of the room and environmental side during S1-Alt5

Test cycle: **S1 – Alt6**
Table B-6: Average data during the last 24 hours for each specimen of S1-Alt6

| Specimen Measurement Data | | | | Control Loop Data | |
|---------------------------|--|--|--|-------------------|------|
| B-G | A | B | C | Sand | |
| 1 | A1_Soil-T 19.578 degC A1_Soil-RH 98.514 % A1_Wall-T 20.172 degC A1_Ext-T 19.808 degC A1_Int-T 19.886 degC A1_Inside-RH 59.651 % A1_Wall-RH 71.394 % | B1_Soil-T 19.826 degC B1_Soil-RH 94.729 % B1_Wall-T 19.795 degC B1_Ext-T 19.645 degC B1_Int-T 19.189 degC B1_Inside-RH 86.283 % B1_Wall-RH 79.847 % | C1_Soil-T 20.400 degC C1_Soil-RH 100.000 % C1_Wall-T 20.602 degC C1_Ext-T 20.301 degC C1_Int-T 19.461 degC C1_Inside-RH 87.614 % C1_Wall-RH 76.355 % | 1 | |
| 2 | A2_Soil-T 19.429 degC A2_Soil-RH 100.000 % A2_Wall-T 19.785 degC A2_Ext-T 19.685 degC A2_Int-T 19.484 degC A2_Inside-RH 62.048 % A2_Wall-RH 77.469 % | B2_Soil-T 19.183 degC B2_Soil-RH 100.000 % B2_Wall-T 19.330 degC B2_Ext-T 19.056 degC B2_Int-T 19.205 degC B2_Inside-RH 91.189 % B2_Wall-RH 90.814 % | C2_Soil-T 20.222 degC C2_Soil-RH 100.000 % C2_Ext-T 20.161 degC C2_Int-T 19.682 degC C2_Inside-RH 79.456 degC | 2 | |
| 3 | A3_Soil-T 19.428 degC A3_Soil-RH 100.000 % A3_Wall-T 19.932 degC A3_Ext-T 19.425 degC A3_Int-T 19.656 degC A3_Inside-RH 64.422 % A3_Wall-RH 86.394 % | B3_Soil-T 19.488 degC B3_Soil-RH 100.000 % B3_Wall-T 19.418 degC B3_Ext-T 19.054 degC B3_Int-T 19.516 degC B3_Inside-RH 88.229 % B3_Wall-RH 70.221 % | C3_Soil-T 21.652 degC C3_Soil-RH 100.000 % C3_Ext-T 20.880 degC C3_Int-T 20.213 degC C3_Inside-RH 100.000 degC | 3 | |
| No | A | B | C | | Alt6 |

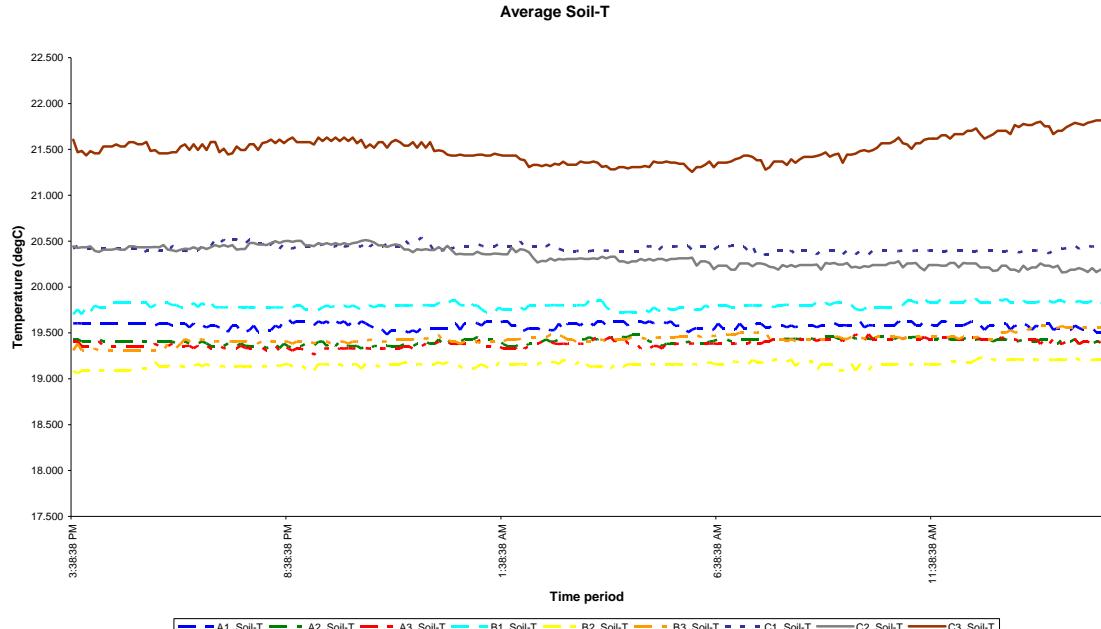
* Measured pressure difference between Room Side & Environmental Side

Remarks

Type: B-G
 Soil type: Sand
 Damp proofing: No
 Alternative: Alt6

Legend

T - Temperature (degC)
 RH - Relative Humidity (%)
 SP - Setpoint (either T or RH)


Figure B-46: Average soil temperature of S1-Alt6

Insulated Concrete Masonry Below-grade Walls

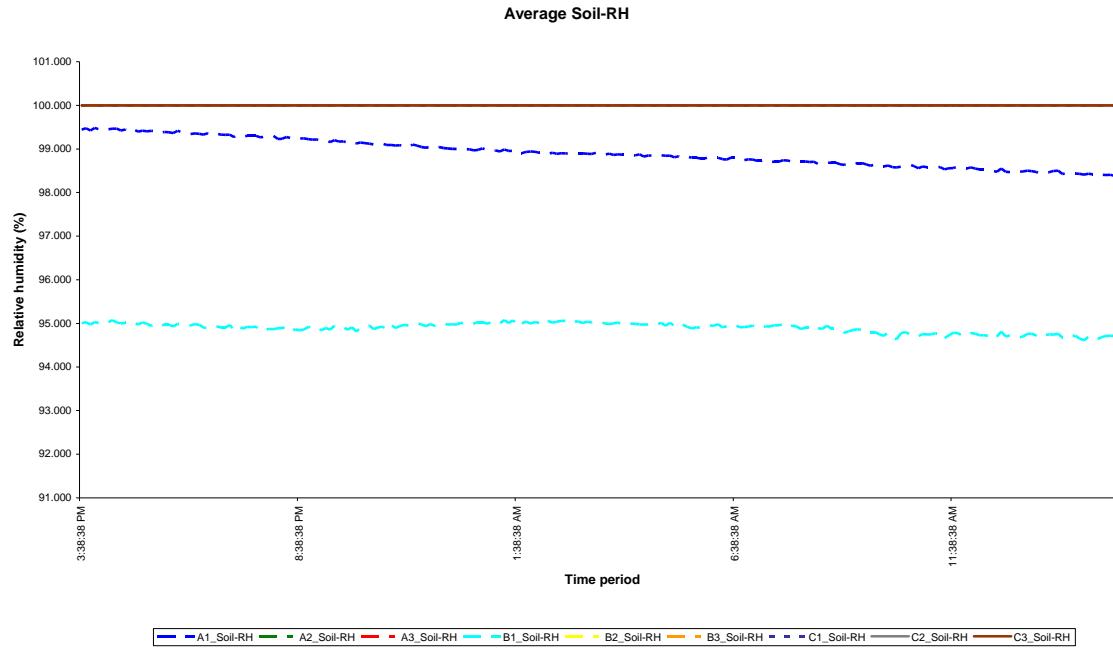


Figure B-47: Average soil relative humidity of S1-Alt6

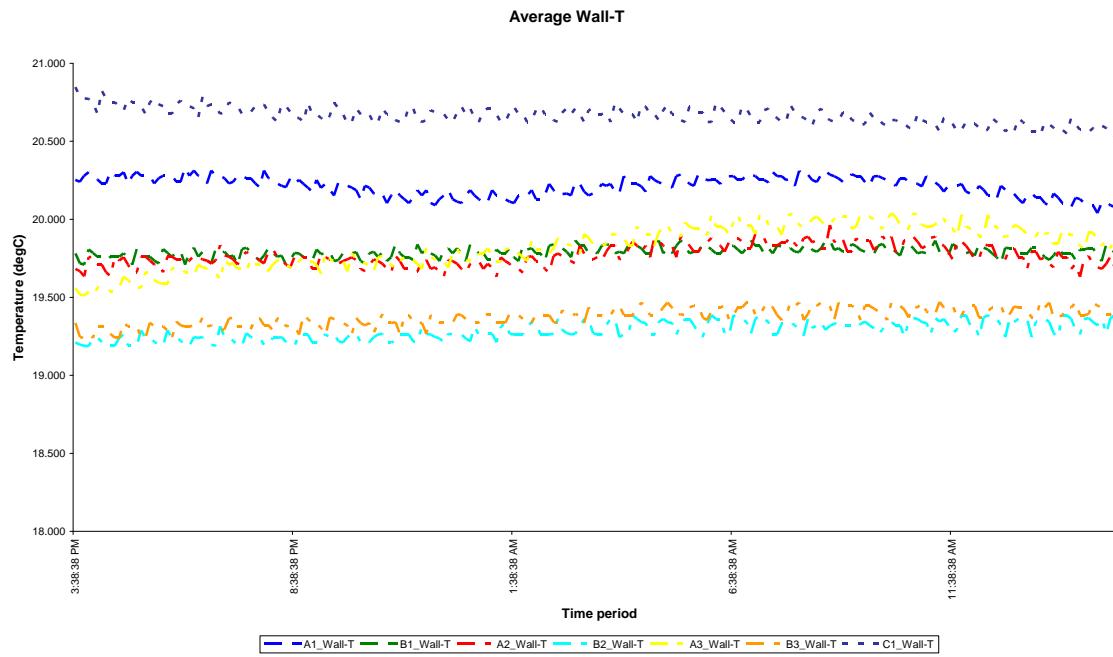


Figure B-48: Average wall temperature of S1-Alt6

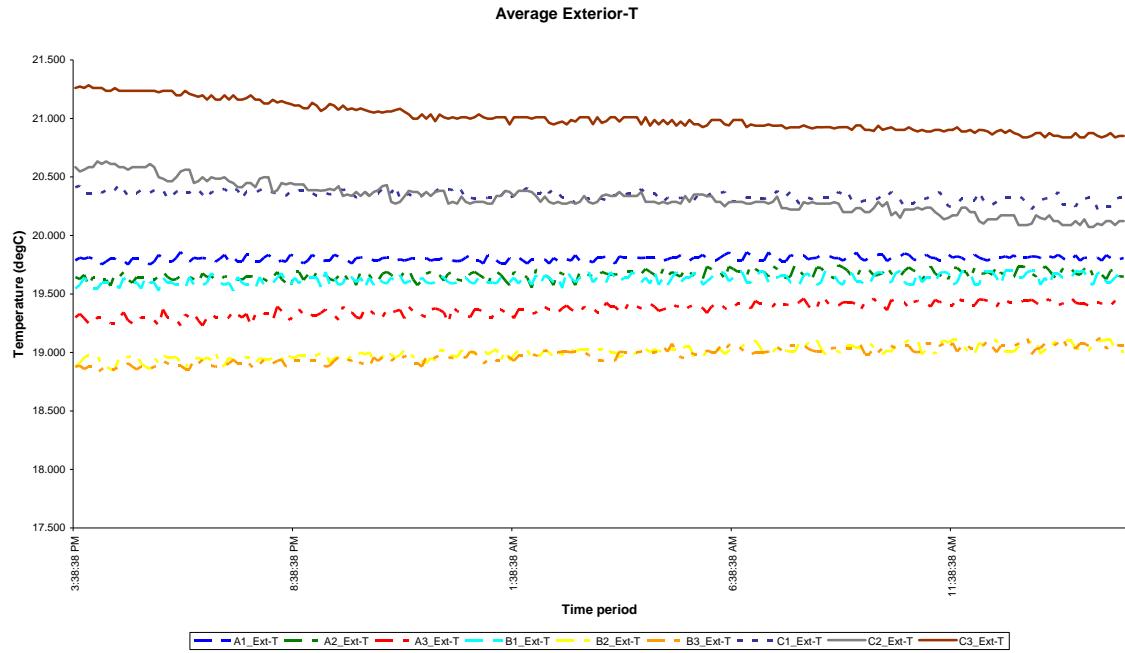


Figure B-49: Average exterior temperature of S1-Alt6

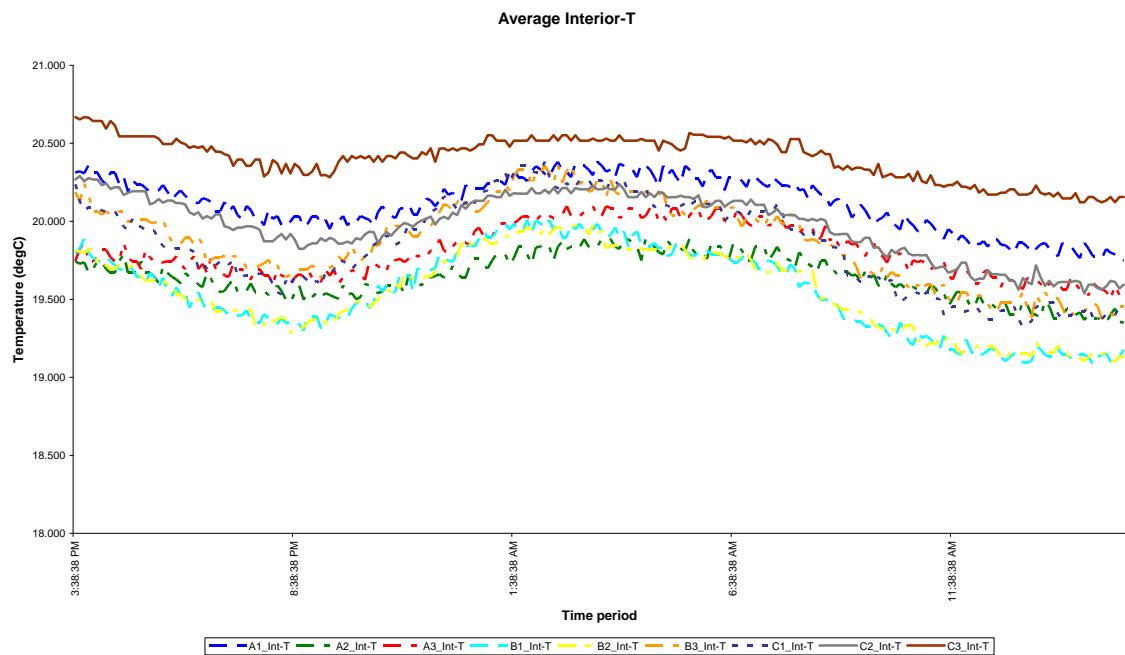


Figure B-50: Average interior temperature of S1-Alt6

Insulated Concrete Masonry Below-grade Walls

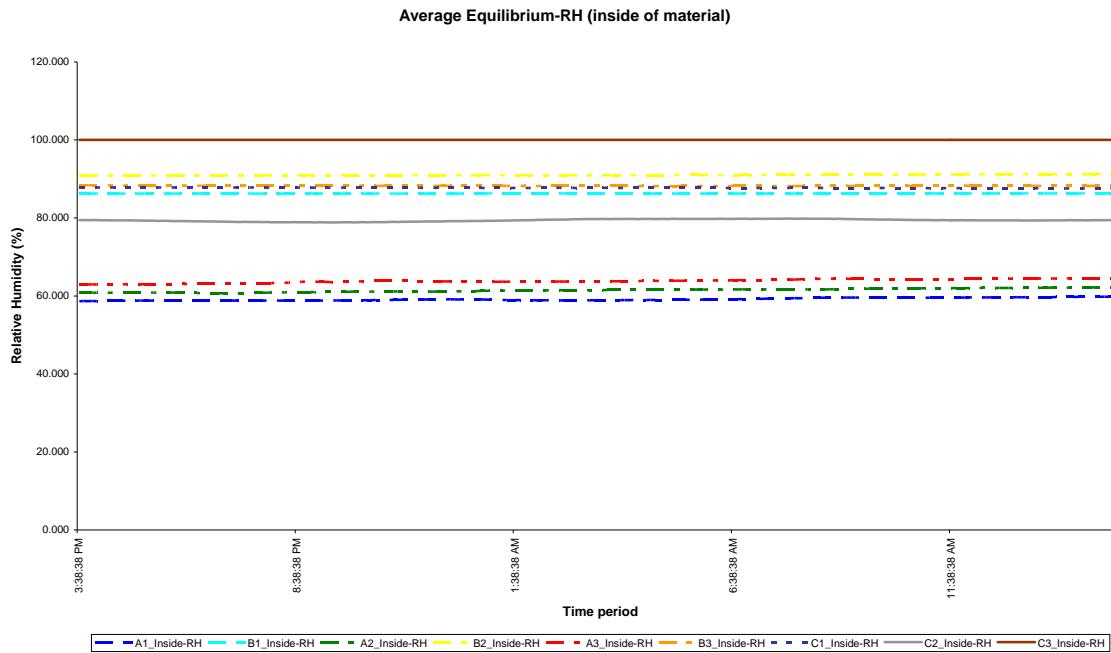


Figure B-51: Average equilibrium of relative humidity in a cavity of S1-Alt6

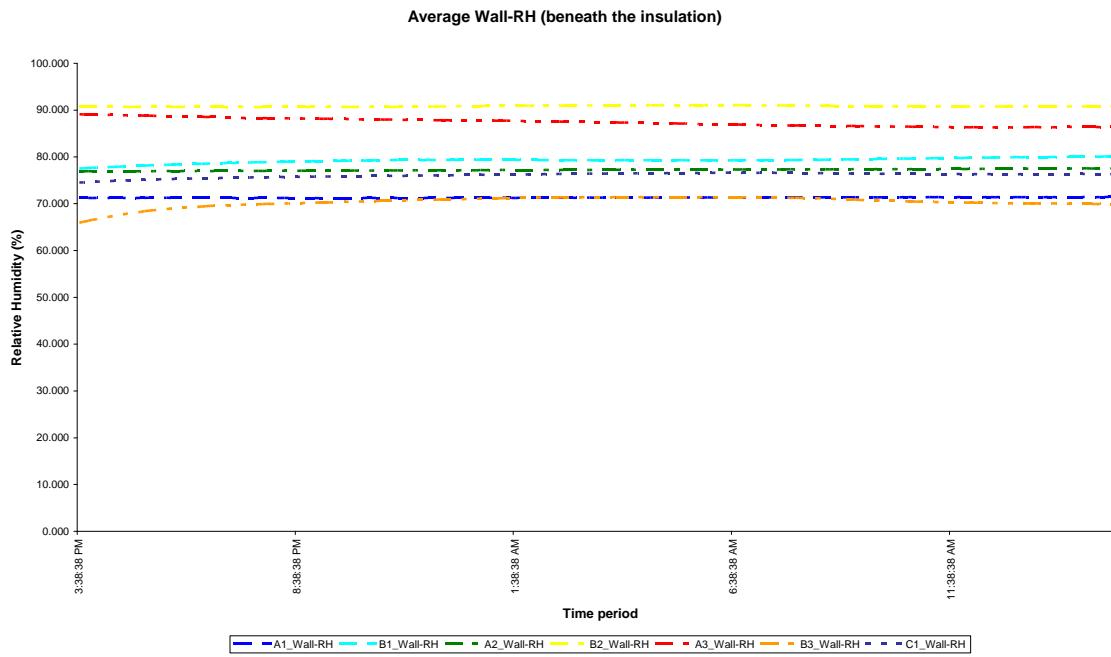


Figure B-52: Average wall relative humidity beneath the insulation of S1-Alt6

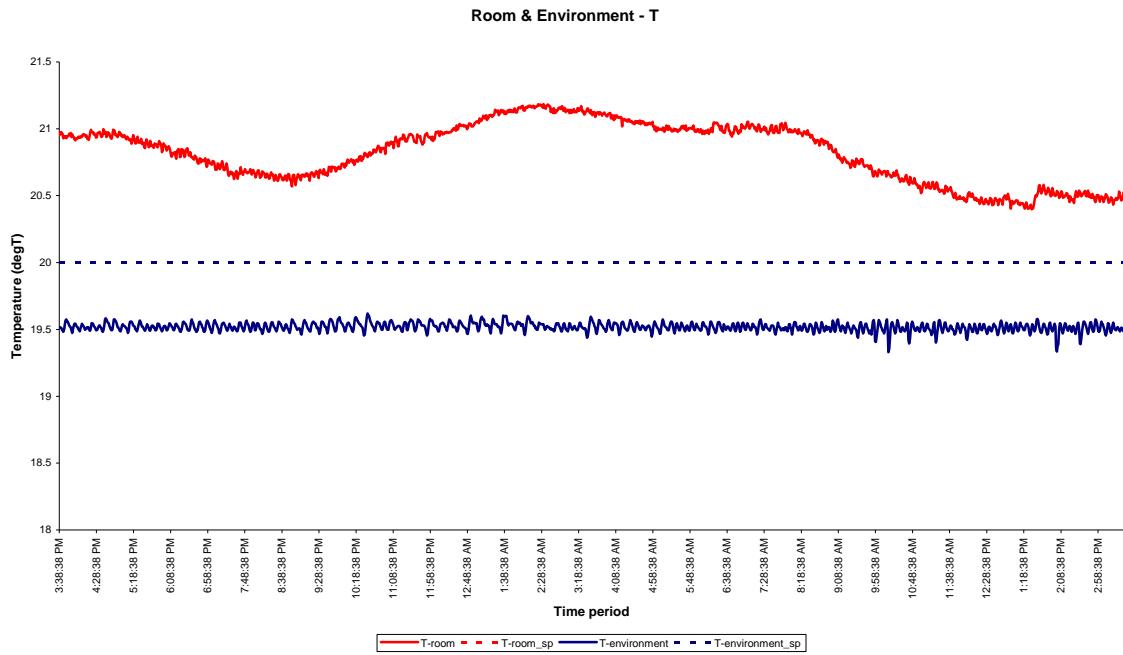


Figure B-53: Temperature of the room and environmental side during S1-Alt6

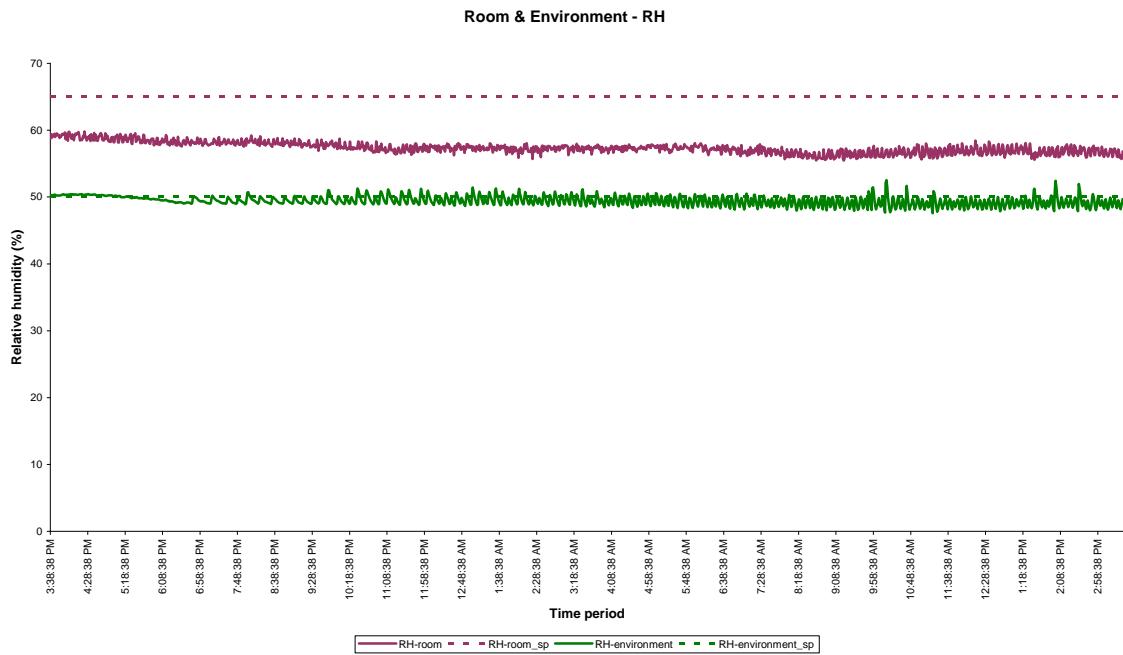


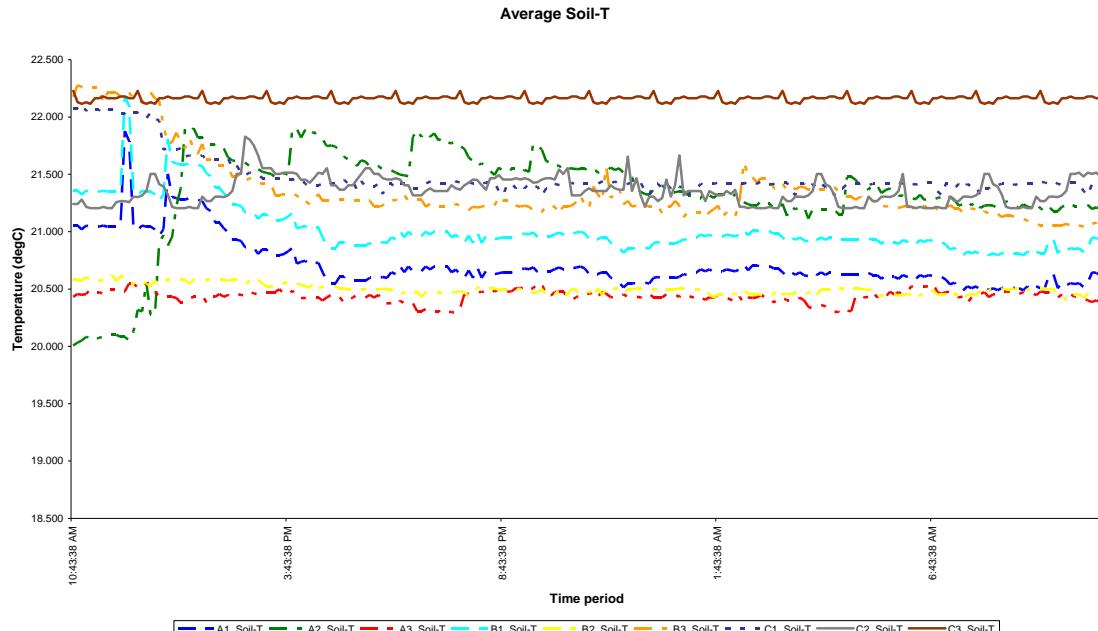
Figure B-54: Relative humidity of the room and environmental side during S1-Alt6

Test cycle: S1 – Alt7

Table B-7: Average data during the last 24 hours for each specimen of S1-Alt7

| Specimen Measurement Data | | | | Control Loop Data | |
|---------------------------|---|--|--|-------------------|------|
| B-G | A | B | C | Sand | |
| 1 | A1_Soil-T 20.567 degC A1_Soil-RH 100.000 % A1_Wall-T 18.683 degC A1_Ext-T 20.027 degC A1_Int-T 18.282 degC A1_Inside-RH 69.127 % A1_Wall-RH 72.543 % | B1_Soil-T 20.871 degC B1_Soil-RH 100.000 % B1_Wall-T 20.075 degC B1_Ext-T 20.143 degC B1_Int-T 18.603 degC B1_Inside-RH 85.470 % B1_Wall-RH 72.221 % | C1_Soil-T 21.407 degC C1_Soil-RH 100.000 % C1_Wall-T 21.102 degC C1_Ext-T 20.931 degC C1_Int-T 19.774 degC C1_Inside-RH 88.448 % C1_Wall-RH 77.833 % | 1 | |
| 2 | A2_Soil-T 21.273 degC A2_Soil-RH 100.000 % A2_Wall-T 18.343 degC A2_Ext-T 20.079 degC A2_Int-T 17.862 degC A2_Inside-RH 66.181 % A2_Wall-RH 81.701 % | B2_Soil-T 20.469 degC B2_Soil-RH 100.000 % B2_Wall-T 19.845 degC B2_Ext-T 19.790 degC B2_Int-T 18.206 degC B2_Inside-RH 92.199 % B2_Wall-RH 80.687 % | C2_Soil-T 21.307 degC C2_Soil-RH 100.000 % C2_Ext-T 20.388 degC C2_Int-T 19.524 degC C2_Inside-RH 82.484 degC | 2 | |
| 3 | A3_Soil-T 20.447 degC A3_Soil-RH 100.000 % A3_Wall-T 18.629 degC A3_Ext-T 19.663 degC A3_Int-T 18.067 degC A3_Inside-RH 69.093 % A3_Wall-RH 101.351 % | B3_Soil-T 21.167 degC B3_Soil-RH 100.000 % B3_Wall-T 19.724 degC B3_Ext-T 19.606 degC B3_Int-T 18.515 degC B3_Inside-RH 89.069 % B3_Wall-RH 69.114 % | C3_Soil-T 22.160 degC C3_Soil-RH 100.000 % C3_Ext-T 20.606 degC C3_Int-T 19.875 degC C3_Inside-RH 100.000 degC | 3 | |
| No | A | B | C | | Alt7 |

* Measured pressure difference between Room Side & Environmental Side


Figure B-55: Average soil temperature of S1-Alt7

Insulated Concrete Masonry Below-grade Walls

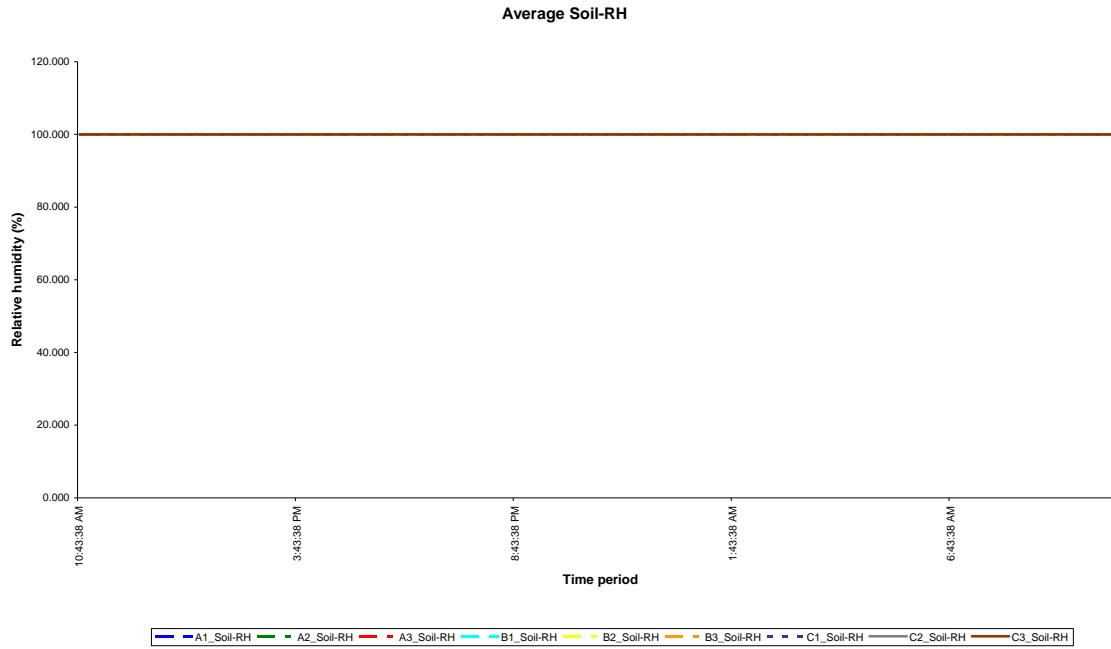


Figure B-56: Average soil relative humidity of S1-Alt7

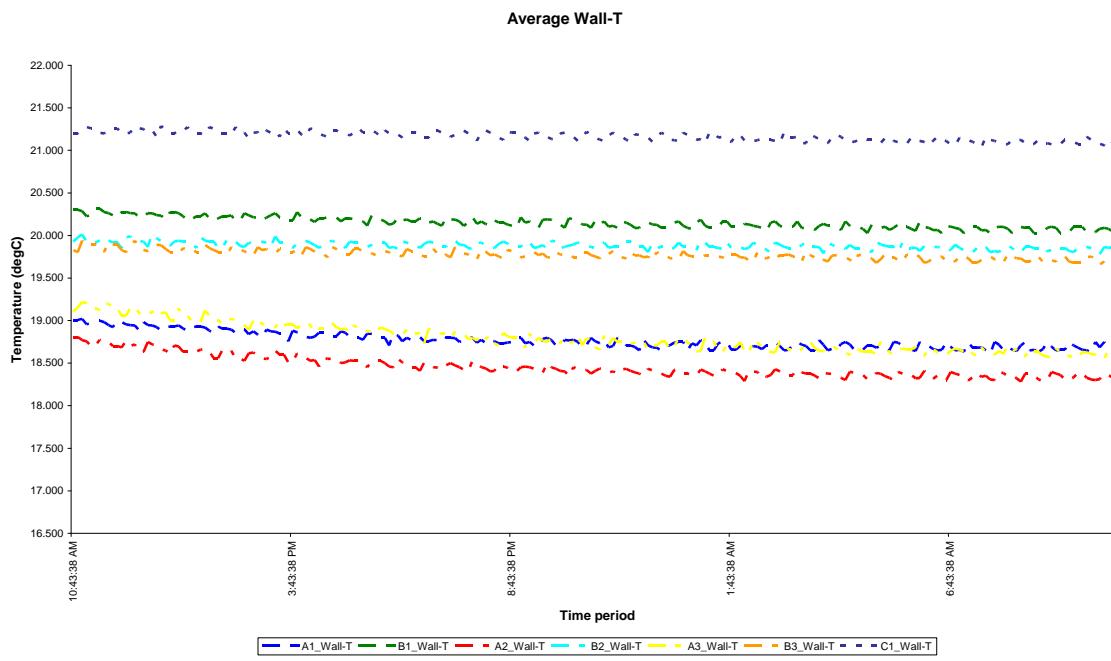


Figure B-57: Average wall temperature of S1-Alt7

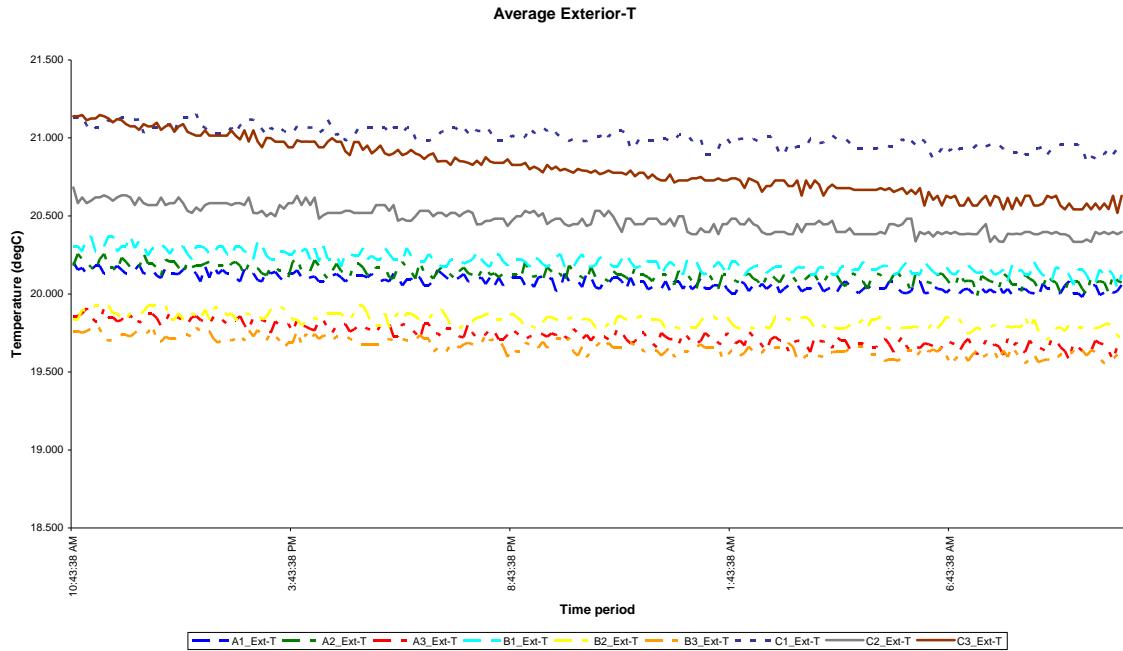


Figure B-58: Average exterior temperature of S1-Alt7

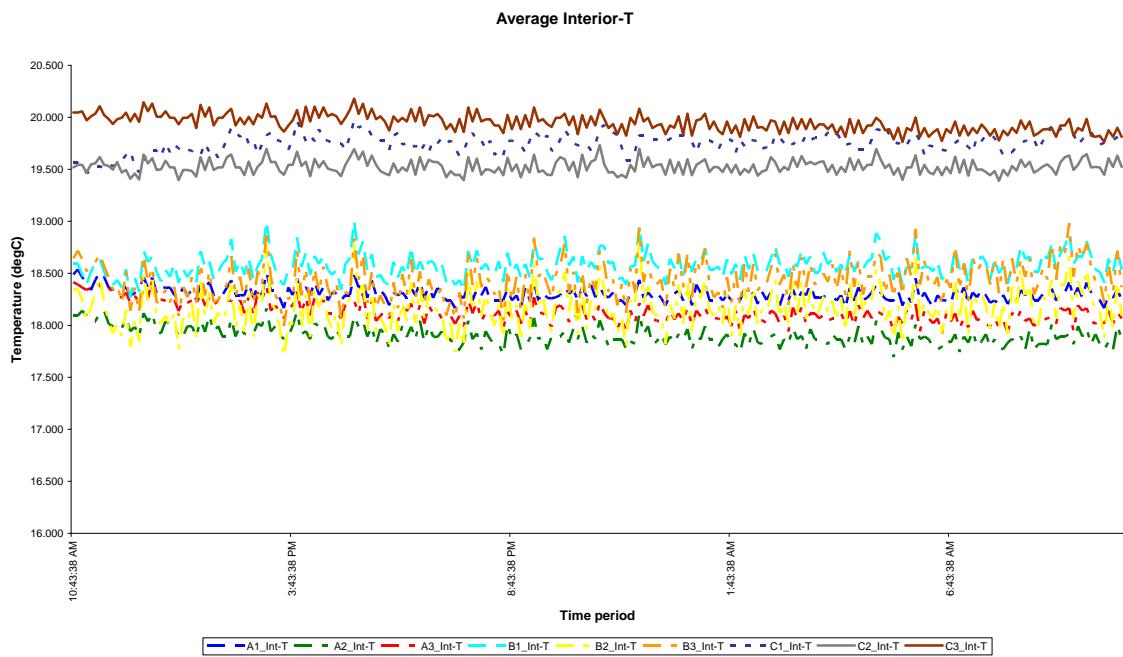


Figure B-59: Average interior temperature of S1-Alt7

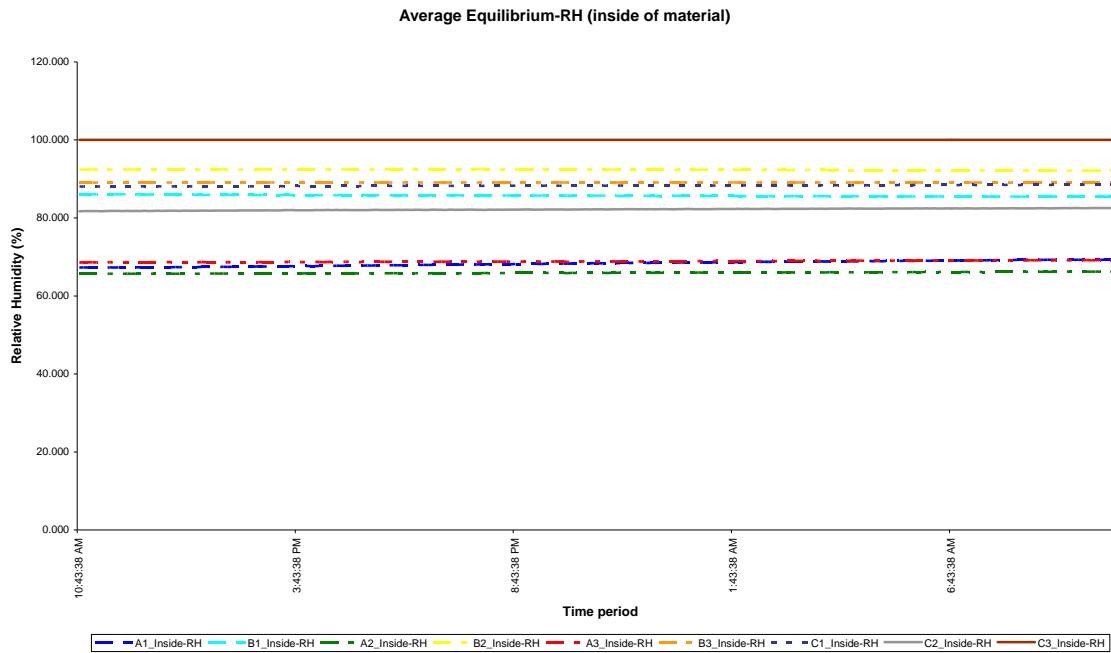


Figure B-60: Average equilibrium of relative humidity in a cavity of S1-Alt7

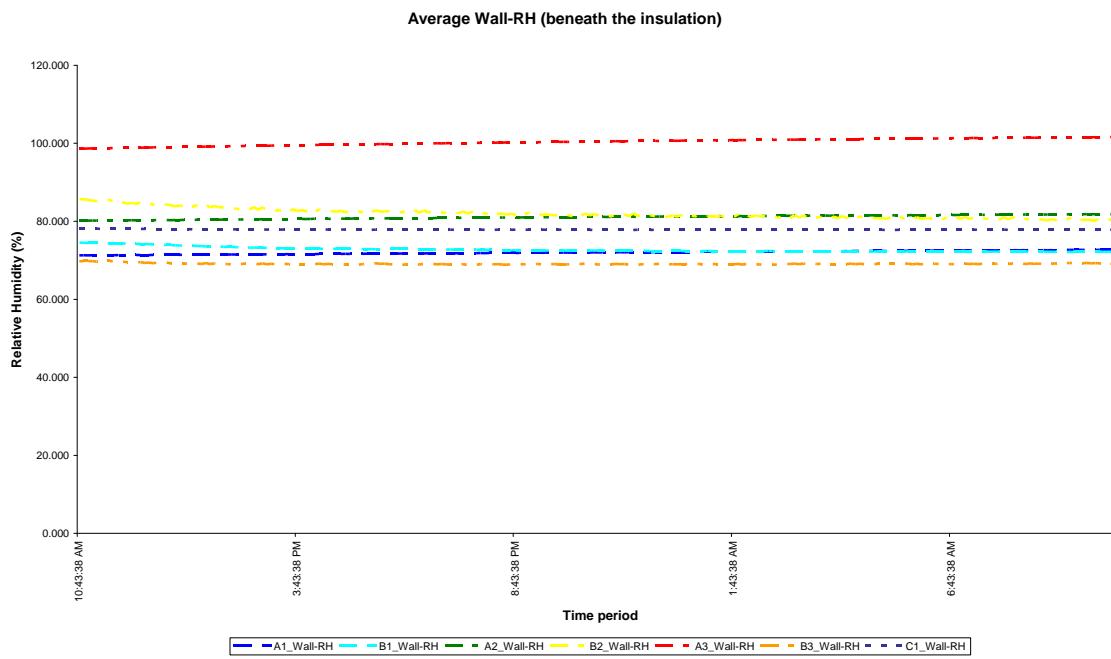


Figure B-61: Average wall relative humidity beneath the insulation of S1-Alt7

Insulated Concrete Masonry Below-grade Walls

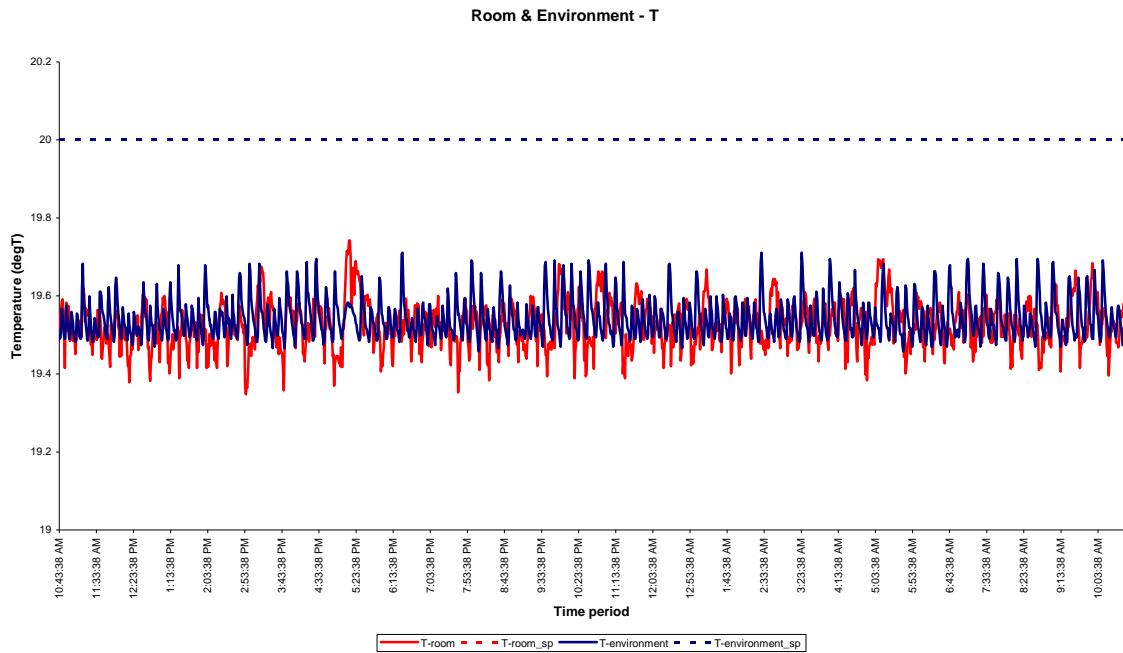


Figure B-62: Temperature of the room and environmental side during S1-Alt7

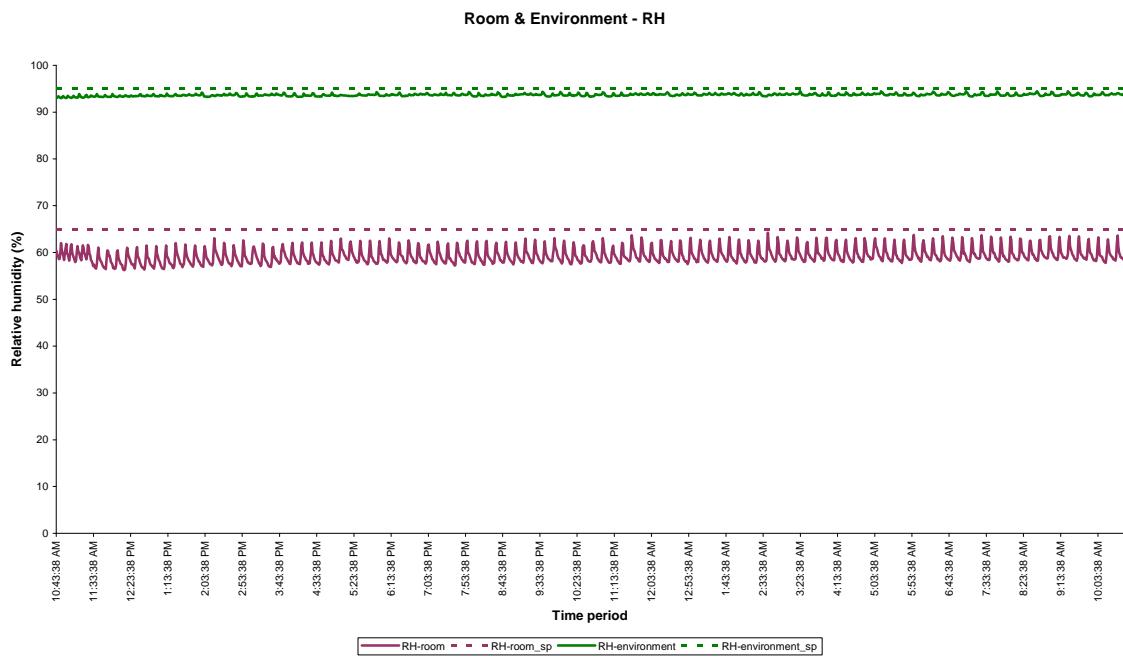
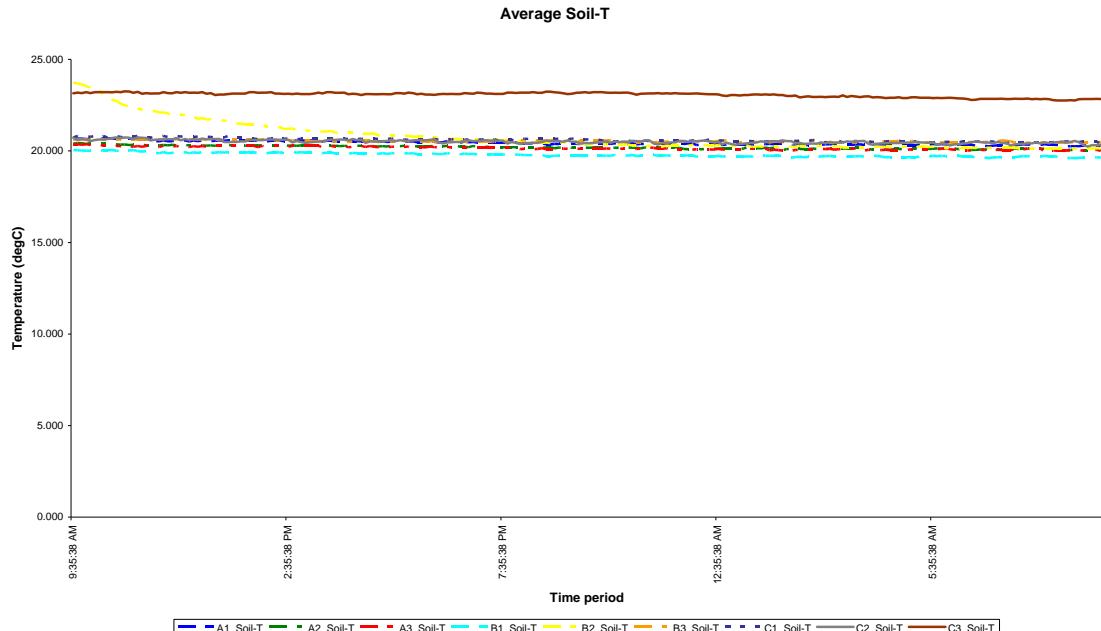


Figure B-63: Relative humidity of the room and environmental side during S1-Alt7

Test cycle: **S1 – Alt8**
Table B-8: Average data during the last 24 hours for each specimen of S1-Alt8

| Specimen Measurement Data | | | | Control Loop Data |
|---------------------------|---|--|--|-------------------|
| B-G | A | B | C | Sand |
| 1 | A1_Soil-T 20.322 degC A1_Soil-RH 100.000 % A1_Wall-T 19.508 degC A1_Ext-T 20.578 degC A1_Int-T 19.196 degC A1_Inside-RH 67.310 % A1_Wall-RH 74.372 % | B1_Soil-T 19.676 degC B1_Soil-RH 100.000 % B1_Wall-T 20.286 degC B1_Ext-T 20.281 degC B1_Int-T 19.308 degC B1_Inside-RH 81.774 % B1_Wall-RH 57.588 % | C1_Soil-T 20.496 degC C1_Soil-RH 100.000 % C1_Wall-T 20.812 degC C1_Ext-T 20.503 degC C1_Int-T 20.431 degC C1_Inside-RH 88.984 % C1_Wall-RH 69.038 % | 1 |
| 2 | A2_Soil-T 20.091 degC A2_Soil-RH 100.000 % A2_Wall-T 18.999 degC A2_Ext-T 20.235 degC A2_Int-T 18.563 degC A2_Inside-RH 63.152 % A2_Wall-RH 81.492 % | B2_Soil-T 20.172 degC B2_Soil-RH 100.000 % B2_Wall-T 20.033 degC B2_Ext-T 19.931 degC B2_Int-T 18.982 degC B2_Inside-RH 88.565 % B2_Wall-RH 73.095 % | C2_Soil-T 20.428 degC C2_Soil-RH 100.000 % C2_Ext-T 20.876 degC C2_Int-T 20.259 degC C2_Inside-RH 80.567 degC | 2 |
| 3 | A3_Soil-T 20.062 degC A3_Soil-RH 100.000 % A3_Wall-T 19.226 degC A3_Ext-T 19.901 degC A3_Int-T 18.713 degC A3_Inside-RH 67.015 % A3_Wall-RH 100.000 % | B3_Soil-T 20.485 degC B3_Soil-RH 100.000 % B3_Wall-T 20.126 degC B3_Ext-T 19.970 degC B3_Int-T 18.656 degC B3_Inside-RH 86.620 % B3_Wall-RH 43.162 % | C3_Soil-T 22.867 degC C3_Soil-RH 100.000 % C3_Ext-T 22.057 degC C3_Int-T 21.021 degC C3_Inside-RH 100.000 degC | 3 |
| No | A | B | C | Alt8 |

* Measured pressure difference between Room Side & Environmental Side


Figure B-64: Average soil temperature of S1-Alt8

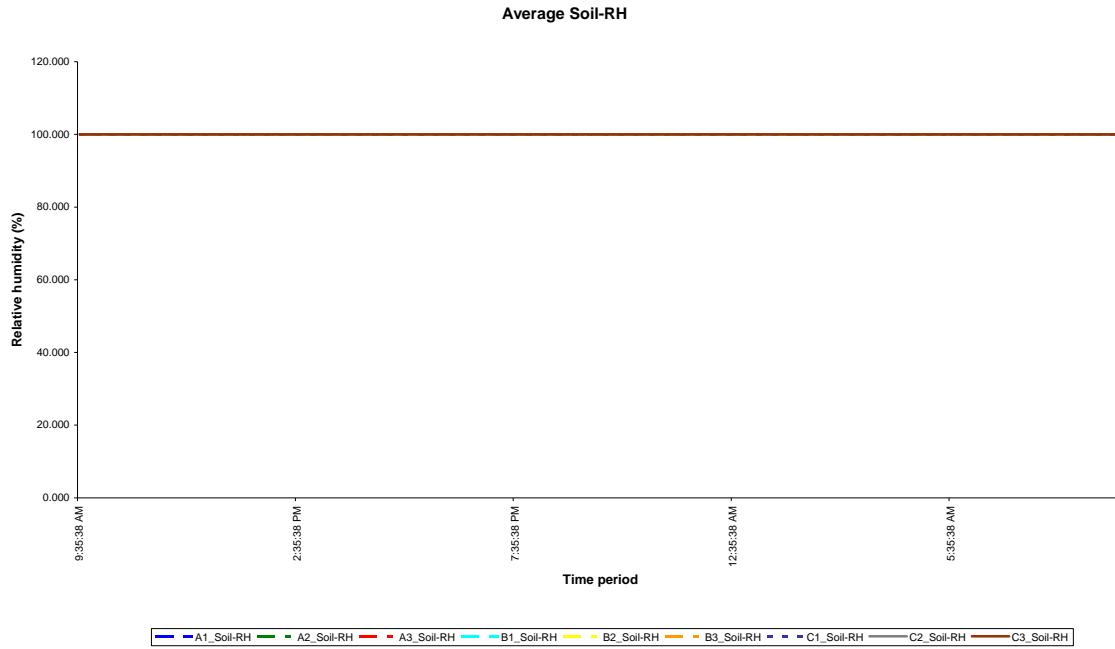


Figure B-65: Average soil relative humidity of S1-Alt8

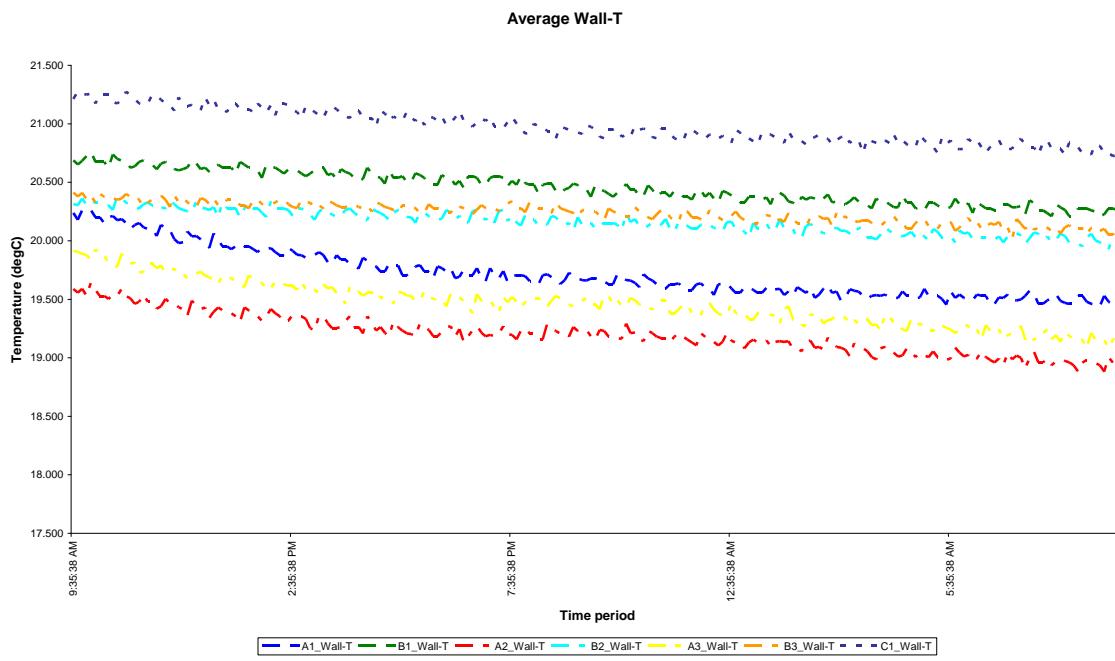


Figure B-66: Average wall temperature of S1-Alt8

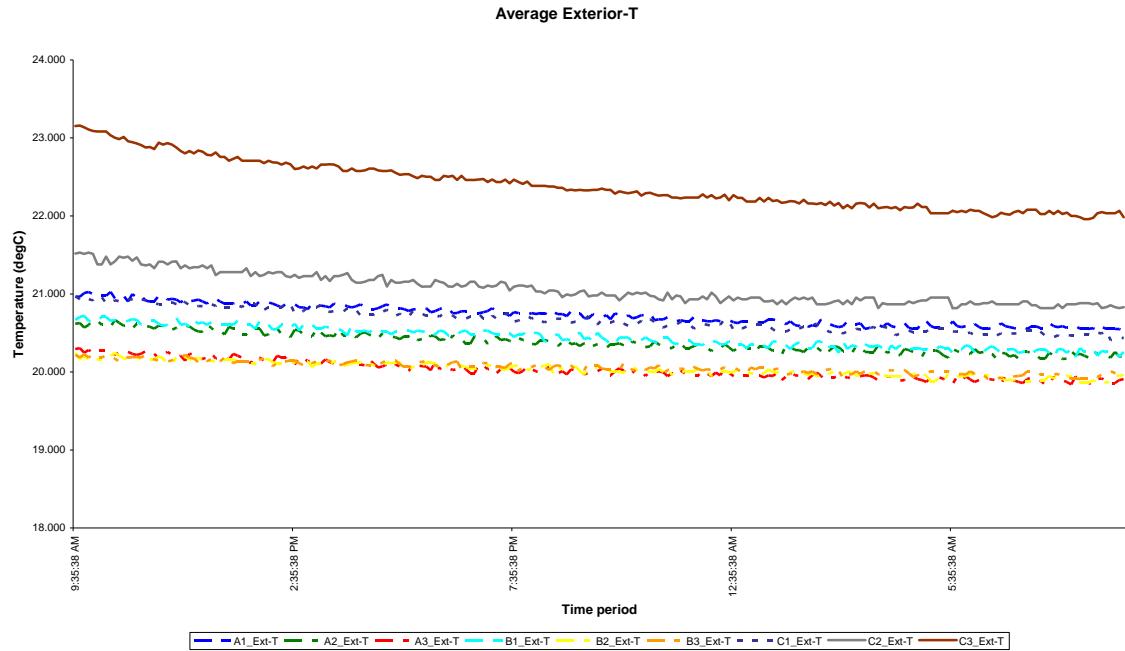


Figure B-67: Average exterior temperature of S1-Alt8

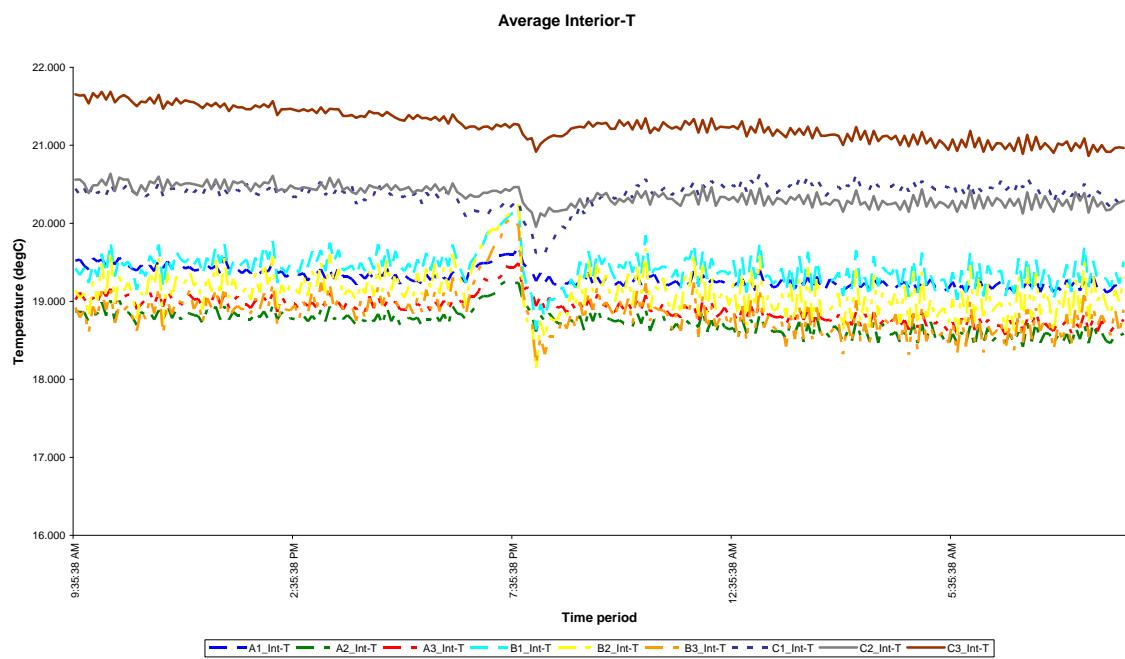


Figure B-68: Average interior temperature of S1-Alt8

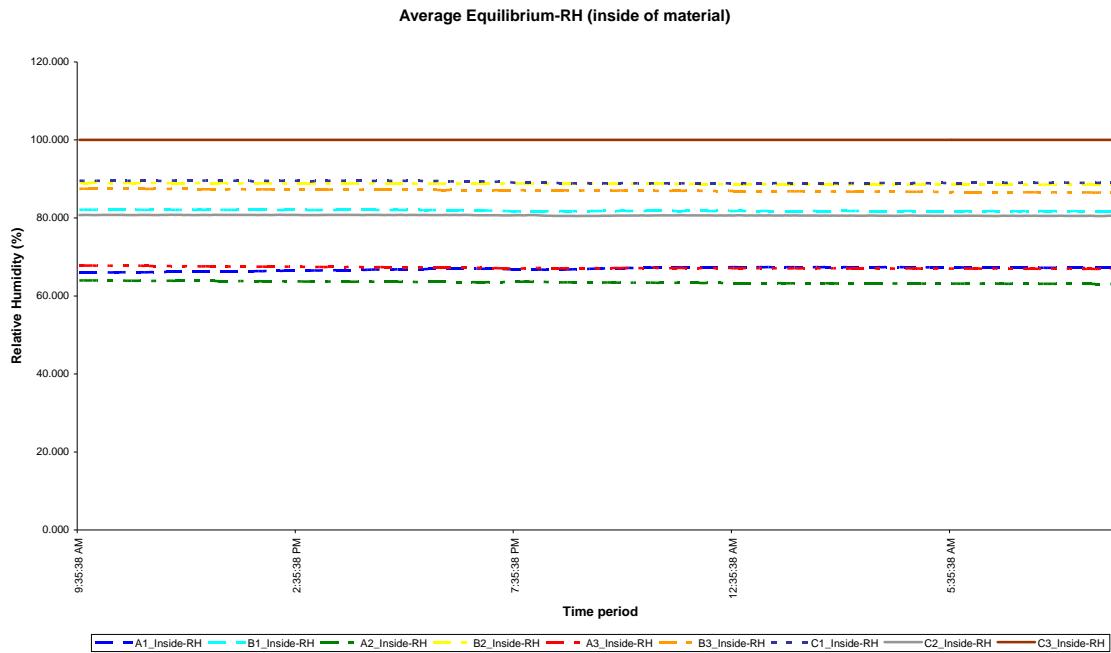


Figure B-69: Average equilibrium of relative humidity in a cavity of S1-Alt8

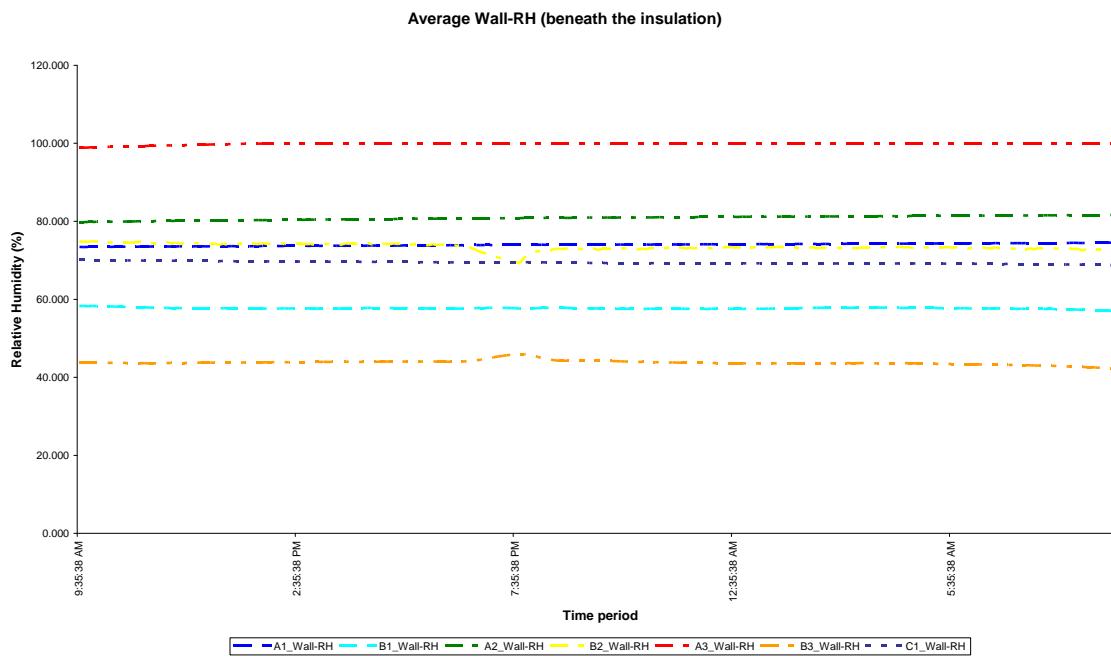


Figure B-70: Average wall relative humidity beneath the insulation of S1-Alt8

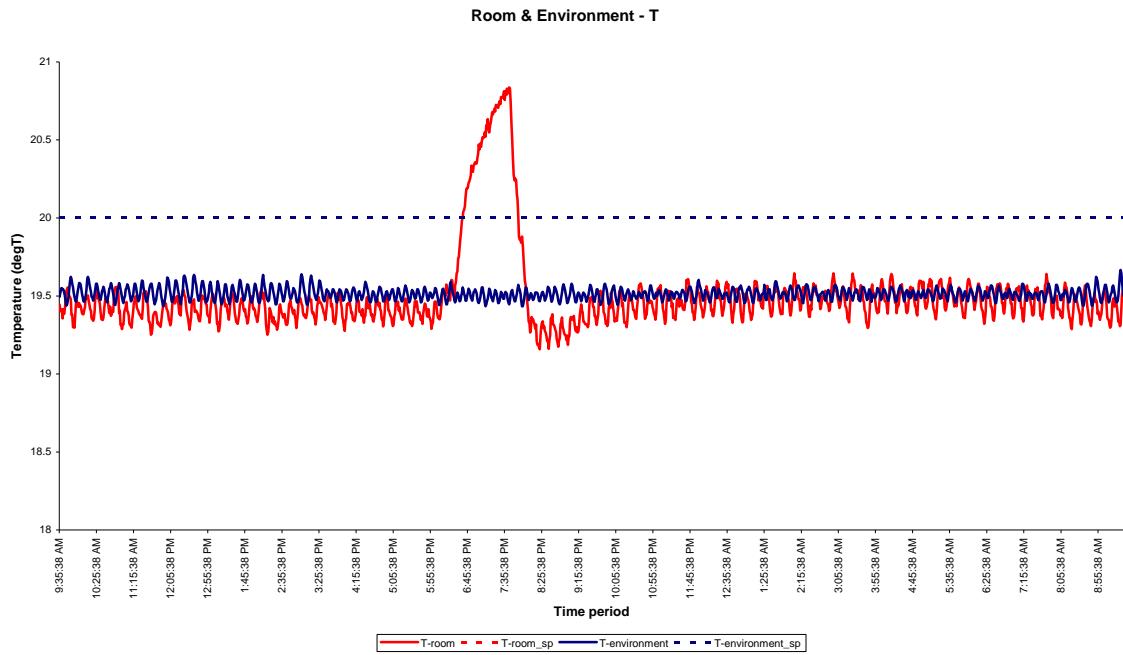


Figure B-71: Temperature of the room and environmental side during S1-Alt8

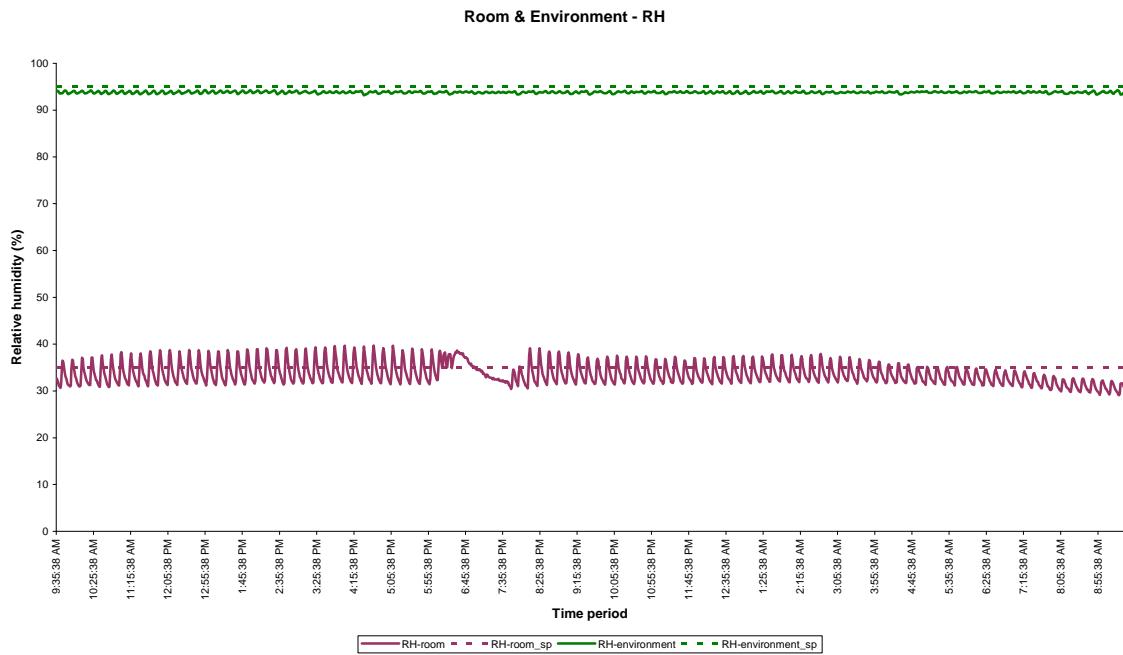


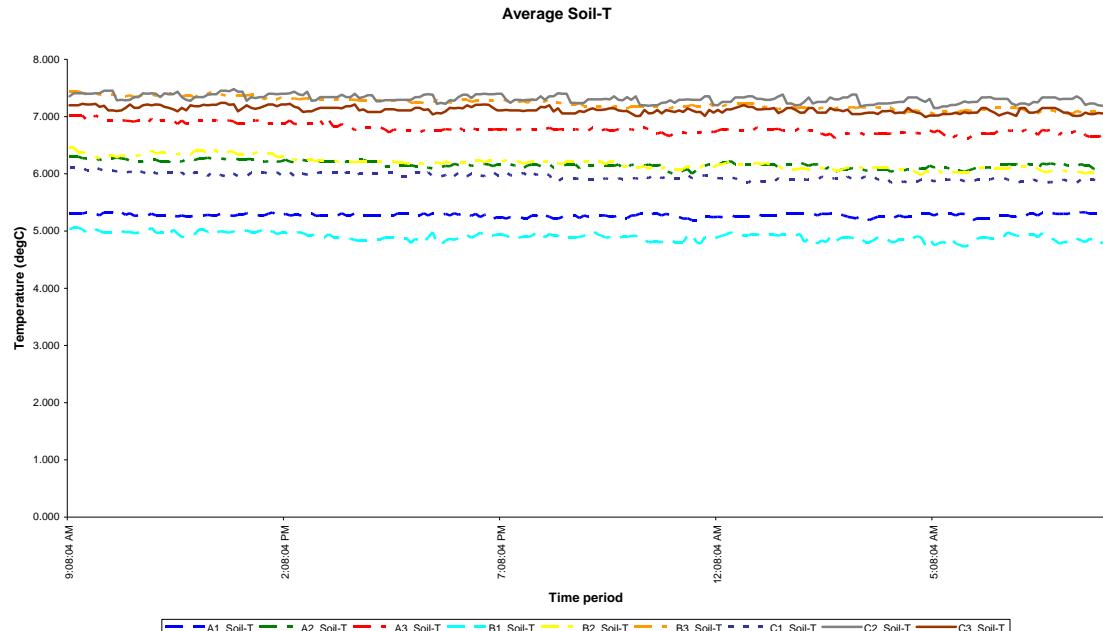
Figure B-72: Relative humidity of the room and environmental side during S1-Alt8

Measurement series: **C1 (Clay; no dampproofing)**

 Test cycle: **C1 – Alt1**
Table B-9: Average data during the last 24 hours for each specimen of C1-Alt1

| Specimen Measurement Data | | | | | Control Loop Data | | | | |
|---------------------------|--------------|-------------|-----------|--------------|-------------------|-----------------|-------------|------|--|
| B-G | A | | B | | C | | Clay | | |
| 1 | A1_Soil-T | 5.271 degC | B1_Soil-T | 4.853 degC | C1_Soil-T | 5.885 degC | 1 | Clay | |
| | A1_Soil-RH | 100.000 % | | B1_Soil-RH | 100.000 % | C1_Soil-RH | 100.000 % | | |
| | A1_Wall-T | 16.702 degC | | B1_Wall-T | 7.885 degC | C1_Wall-T | 9.146 degC | | |
| | A1_Ext-T | 8.522 degC | | B1_Ext-T | 6.829 degC | C1_Ext-T | 7.466 degC | | |
| | A1_Int-T | 18.452 degC | | B1_Int-T | 18.979 degC | C1_Int-T | 18.741 degC | | |
| | A1_Inside-RH | 42.635 % | | B1_Inside-RH | 75.328 % | C1_Inside-RH | 82.024 % | | |
| 2 | A1_Wall-RH | 55.103 % | | B1_Wall-RH | 70.116 % | C1_Wall-RH | 69.263 % | | |
| | A2_Soil-T | 6.111 degC | B2_Soil-T | 6.066 degC | C2_Soil-T | 7.266 degC | 2 | Clay | |
| | A2_Soil-RH | 99.959 % | | B2_Soil-RH | 100.000 % | C2_Soil-RH | 100.000 % | | |
| | A2_Wall-T | 17.716 degC | | B2_Wall-T | 11.408 degC | C2_Ext-T | 14.312 degC | | |
| | A2_Ext-T | 9.575 degC | | B2_Ext-T | 10.175 degC | C2_Int-T | 18.142 degC | | |
| | A2_Int-T | 18.599 degC | | B2_Int-T | 19.152 degC | C2_Inside-RH | 70.861 degC | | |
| 3 | A2_Inside-RH | 53.689 % | | B2_Inside-RH | 88.059 % | 3 | Clay | Alt1 | |
| | A2_Wall-RH | 57.439 % | | B2_Wall-RH | 74.089 % | | | | |
| | A3_Soil-T | 6.709 degC | B3_Soil-T | 7.110 degC | C3_Soil-T | 7.072 degC | | | |
| | A3_Soil-RH | 100.000 % | | B3_Soil-RH | 100.000 % | C3_Soil-RH | 100.000 % | | |
| | A3_Wall-T | 17.706 degC | | B3_Wall-T | 12.288 degC | C3_Ext-T | 16.207 degC | | |
| | A3_Ext-T | 9.969 degC | | B3_Ext-T | 10.952 degC | C3_Int-T | 17.743 degC | | |
| No | A3_Int-T | 18.633 degC | | B3_Int-T | 18.965 degC | C3_Inside-RH | 99.551 degC | | |
| | A3_Inside-RH | 59.578 % | | B3_Inside-RH | 80.656 % | *Pressure diff. | 1.345 Pa | Alt1 | |
| | A3_Wall-RH | 67.530 % | | B3_Wall-RH | 57.318 % | | | | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-73: Average soil temperature of C1-Alt1

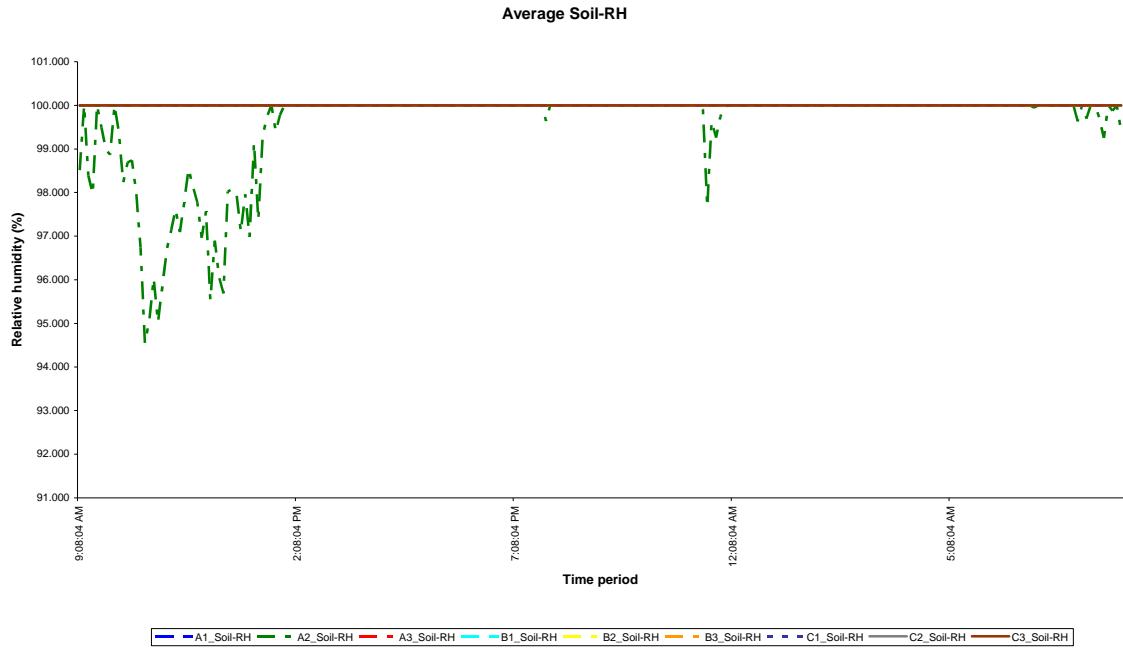


Figure B-74: Average soil relative humidity of C1-Alt1

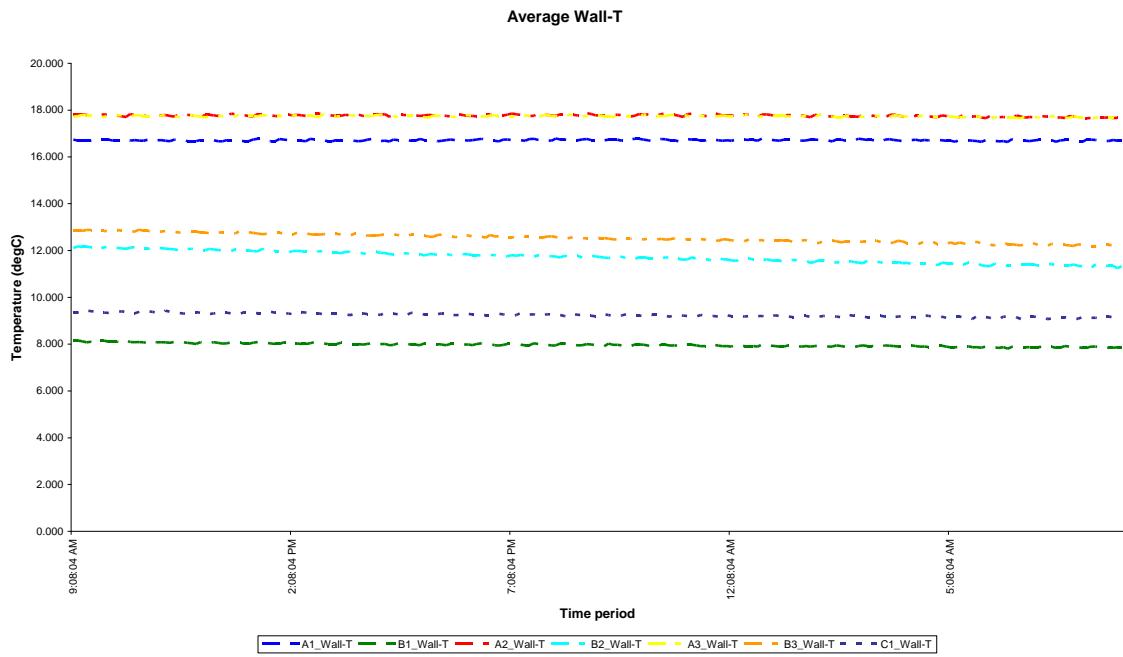


Figure B-75: Average wall temperature of C1-Alt1

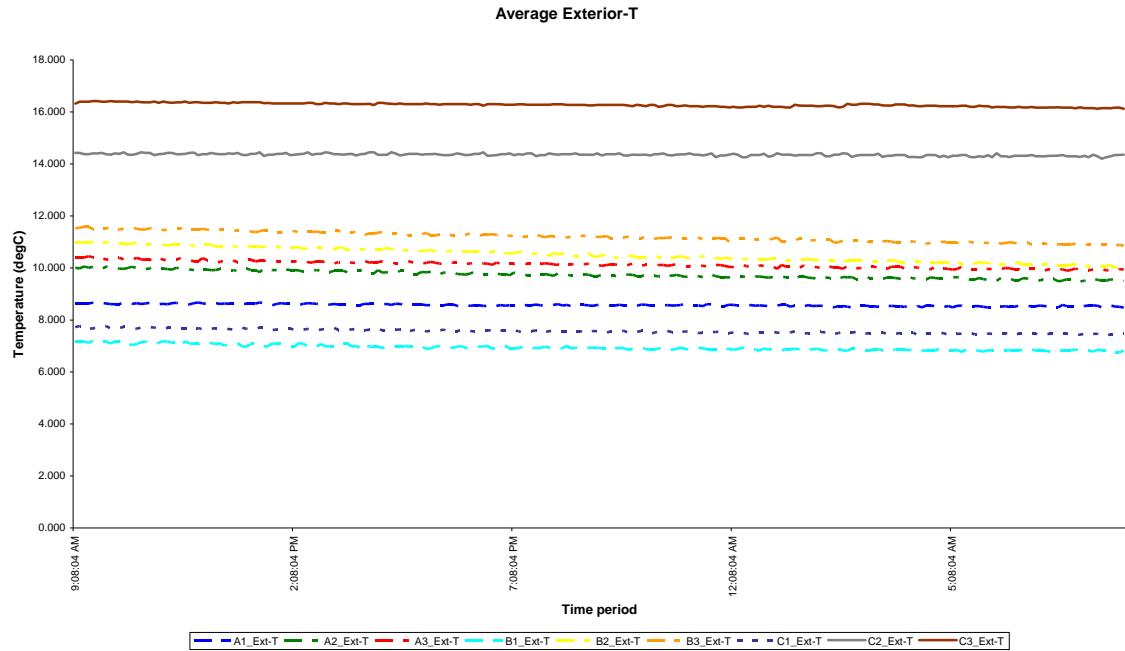


Figure B-76: Average exterior temperature of C1-Alt1

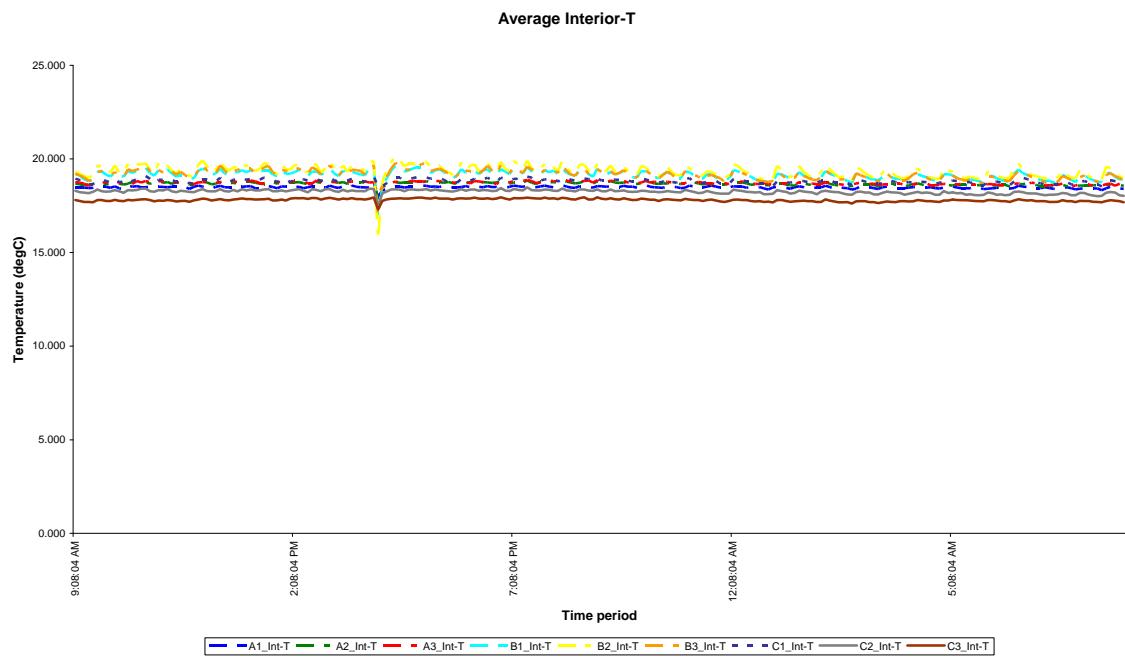


Figure B-77: Average interior temperature of C1-Alt1

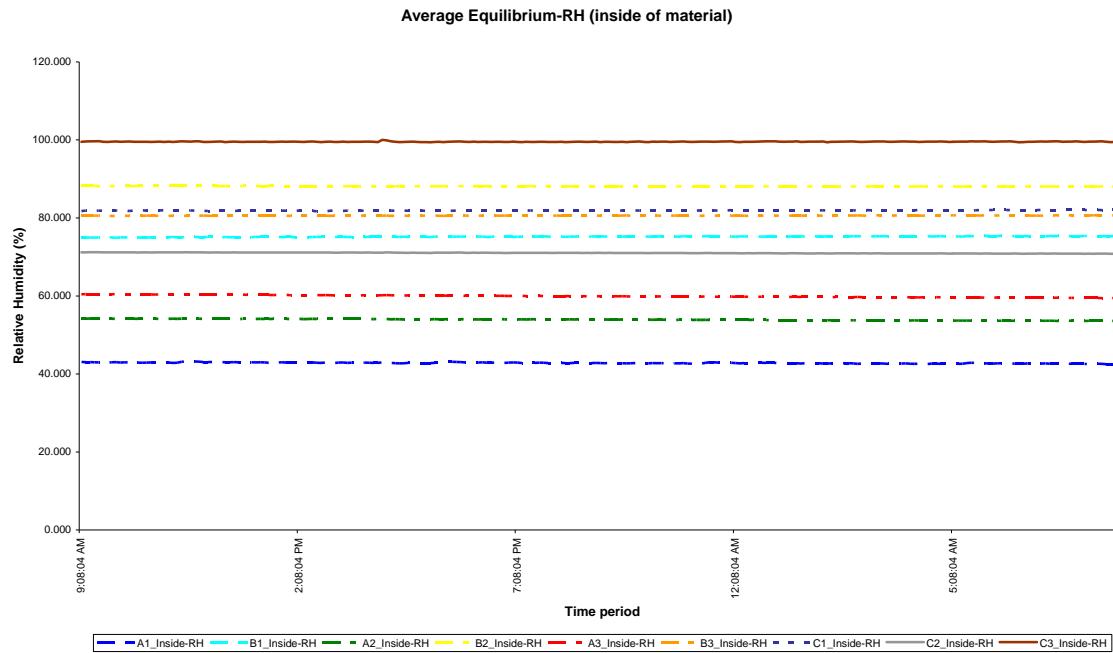


Figure B-78: Average equilibrium of relative humidity in a cavity of C1-Alt1

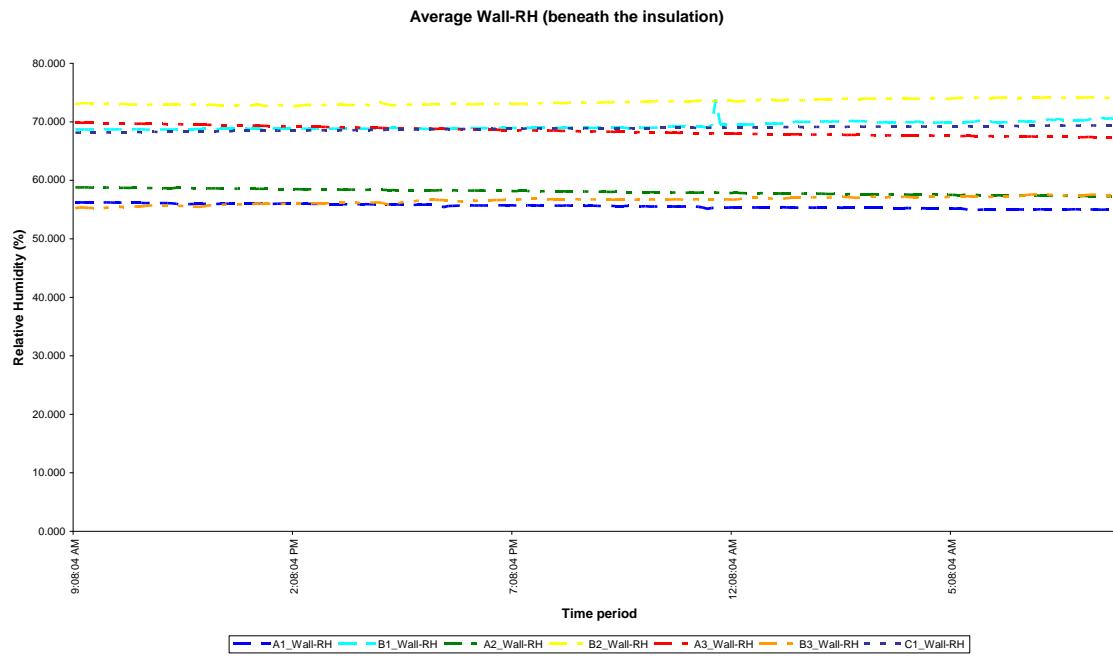


Figure B-79: Average wall relative humidity beneath the insulation of C1-Alt1

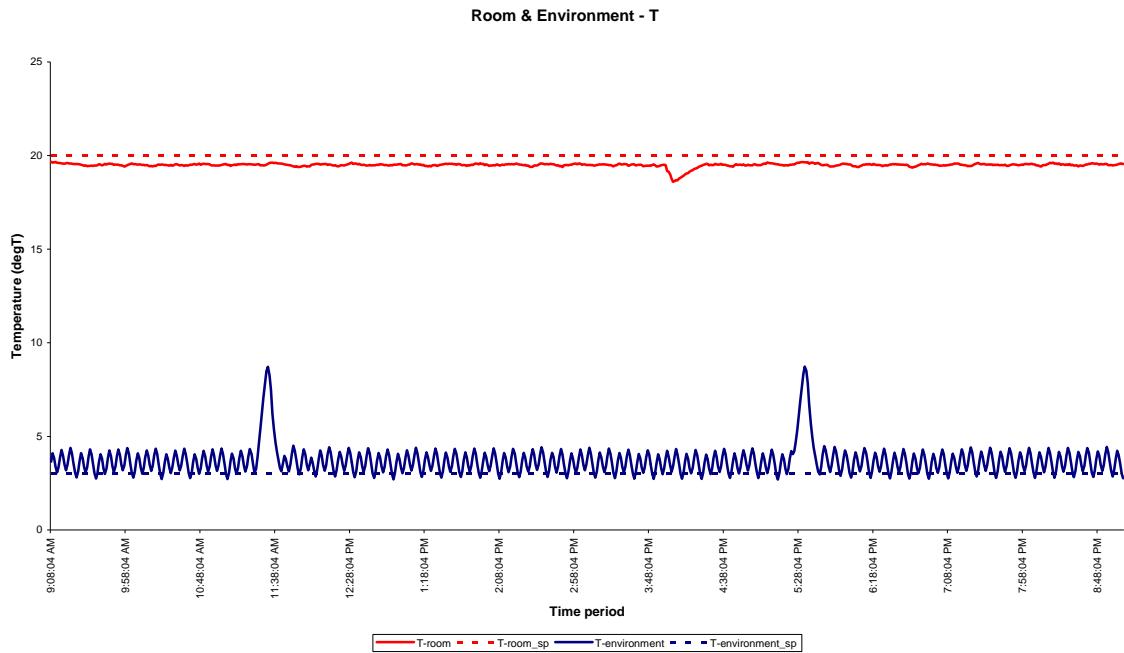


Figure B-80: Temperature of the room and environmental side during C1-Alt1

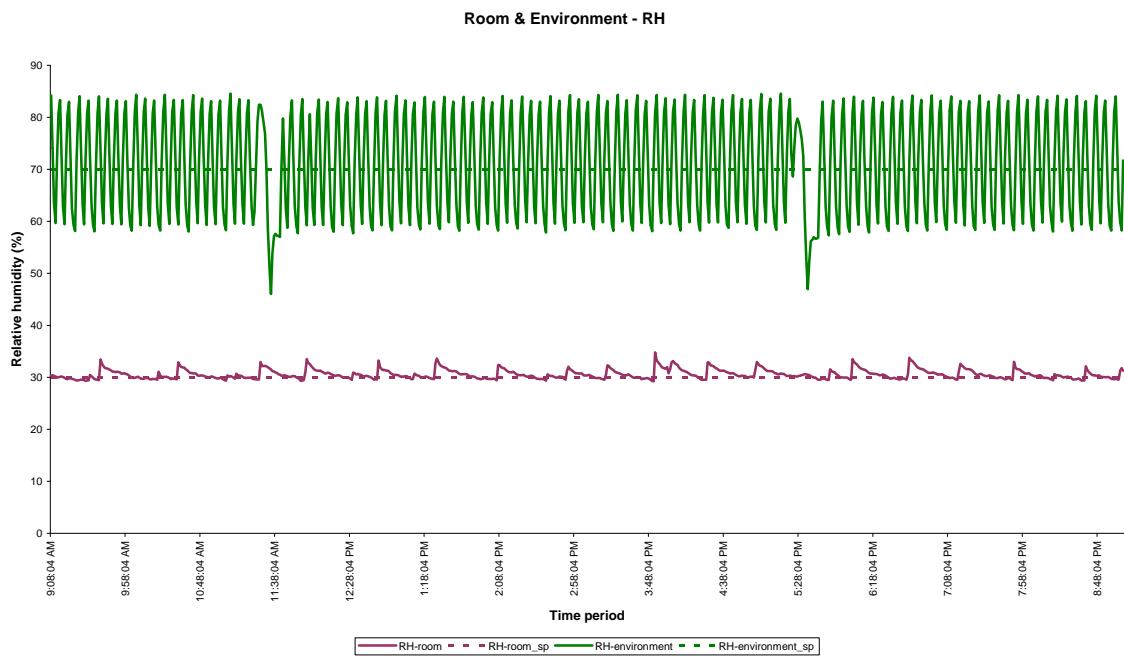


Figure B-81: Relative humidity of the room and environmental side during C1-Alt1

Test cycle: C1 – Alt2

Table B-10: Average data during the last 24 hours for each specimen of C1-Alt2

| Specimen Measurement Data | | | | Control Loop Data | | | |
|---------------------------|-----------------------|-----------------------|--------------------------|-------------------|--|--|--|
| B-G | A | B | C | Clay | | | |
| 1 | A1_Soil-T 5.448 degC | B1_Soil-T 4.962 degC | C1_Soil-T 5.856 degC | 1 | | | |
| | A1_Soil-RH 100.000 % | B1_Soil-RH 100.000 % | C1_Soil-RH 100.000 % | | | | |
| | A1_Wall-T 16.561 degC | B1_Wall-T 7.795 degC | C1_Wall-T 9.084 degC | | | | |
| | A1_Ext-T 8.541 degC | B1_Ext-T 6.704 degC | C1_Ext-T 7.401 degC | | | | |
| | A1_Int-T 18.264 degC | B1_Int-T 18.946 degC | C1_Int-T 18.679 degC | | | | |
| | A1_Inside-RH 52.107 % | B1_Inside-RH 76.634 % | C1_Inside-RH 84.251 % | | | | |
| | A1_Wall-RH 54.603 % | B1_Wall-RH 76.446 % | C1_Wall-RH 84.696 % | | | | |
| | A2_Soil-T 6.058 degC | B2_Soil-T 5.816 degC | C2_Soil-T 7.234 degC | | | | |
| | A2_Soil-RH 100.000 % | B2_Soil-RH 100.000 % | C2_Soil-RH 100.000 % | | | | |
| | A2_Wall-T 17.436 degC | B2_Wall-T 10.506 degC | C2_Ext-T 14.264 degC | | | | |
| 2 | A2_Ext-T 9.189 degC | B2_Ext-T 9.237 degC | C2_Int-T 18.145 degC | 2 | | | |
| | A2_Int-T 18.389 degC | B2_Int-T 19.198 degC | C2_Inside-RH 73.579 degC | | | | |
| | A2_Inside-RH 57.687 % | B2_Inside-RH 88.983 % | | | | | |
| | A2_Wall-RH 55.668 % | B2_Wall-RH 91.597 % | | | | | |
| | A3_Soil-T 6.555 degC | B3_Soil-T 6.839 degC | C3_Soil-T 7.037 degC | | | | |
| | A3_Soil-RH 100.000 % | B3_Soil-RH 100.000 % | C3_Soil-RH 100.000 % | | | | |
| | A3_Wall-T 17.475 degC | B3_Wall-T 11.818 degC | C3_Ext-T 16.051 degC | | | | |
| | A3_Ext-T 9.629 degC | B3_Ext-T 10.464 degC | C3_Int-T 17.661 degC | | | | |
| | A3_Int-T 18.473 degC | B3_Int-T 19.018 degC | C3_Inside-RH 99.517 degC | | | | |
| 3 | A3_Inside-RH 61.584 % | B3_Inside-RH 83.155 % | 3 | | | | |
| | A3_Wall-RH 65.544 % | B3_Wall-RH 92.618 % | | | | | |
| | No | A | B | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
| | | | | Alt2 | | | |

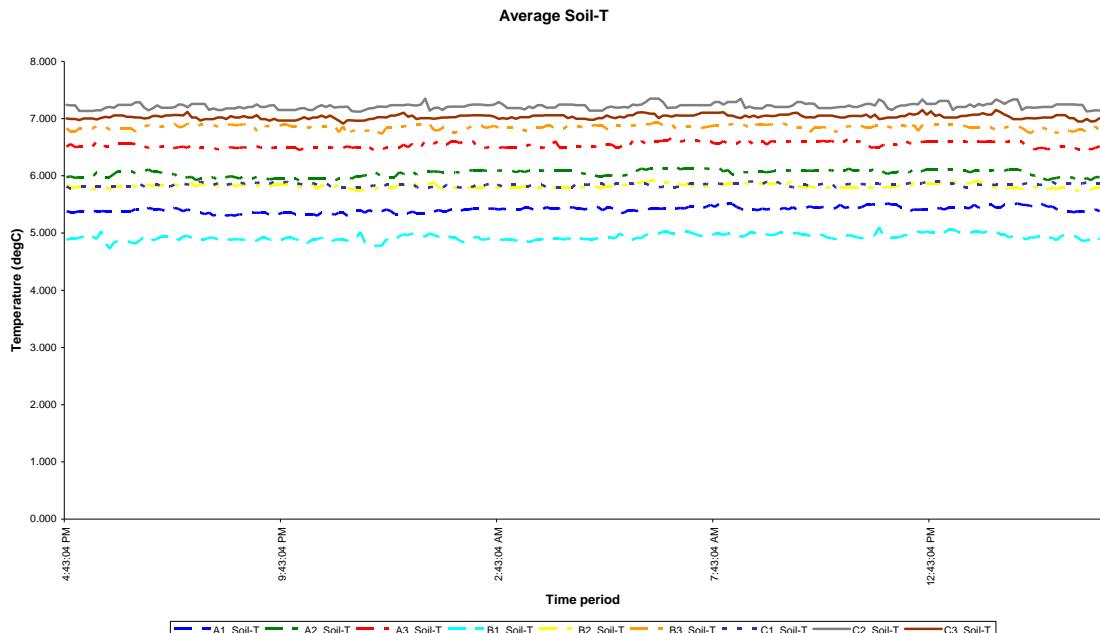
* Measured pressure difference between Room Side & Environmental Side

Remarks

Type: B-G
 Soil type: Clay
 Damp proofing: No
 Alternative: Alt2

Legend

T - Temperature (degC)
 RH - Relative Humidity (%)
 SP - Setpoint (either T or RH)


Figure B-82: Average soil temperature of C1-Alt2

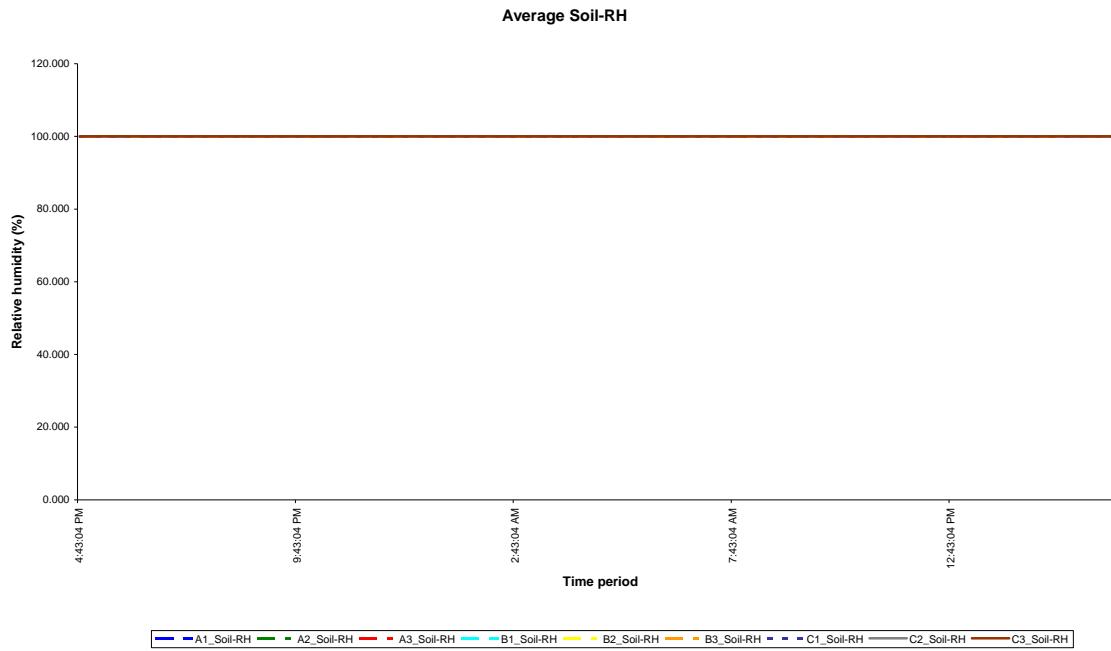


Figure B-83: Average soil relative humidity of C1-Alt2

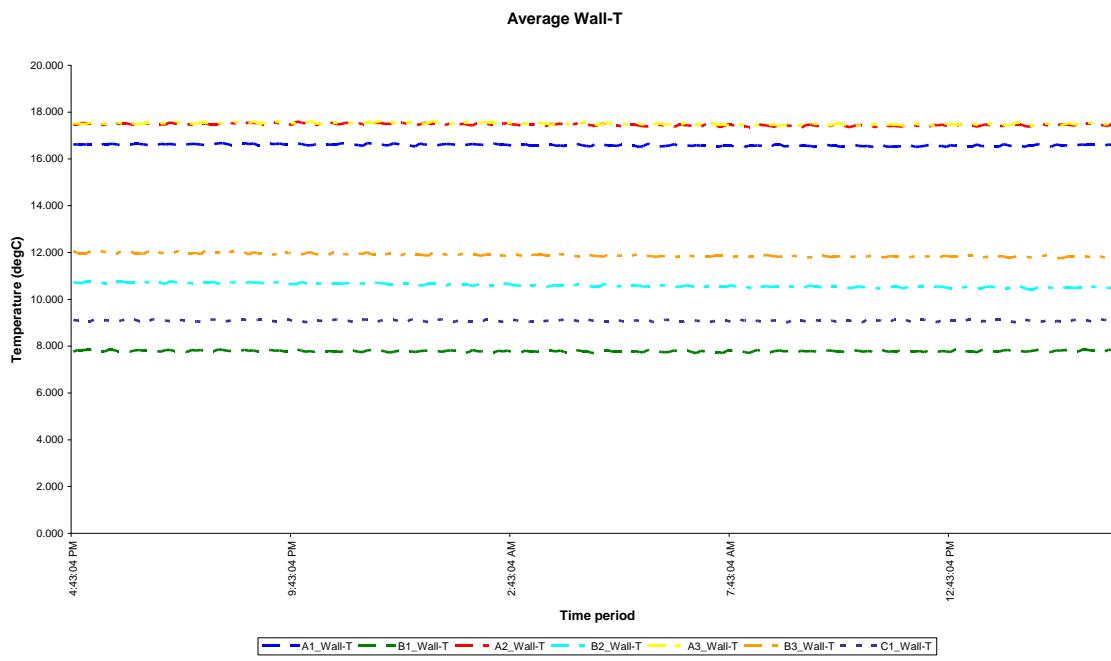


Figure B-84: Average wall temperature of C1-Alt2

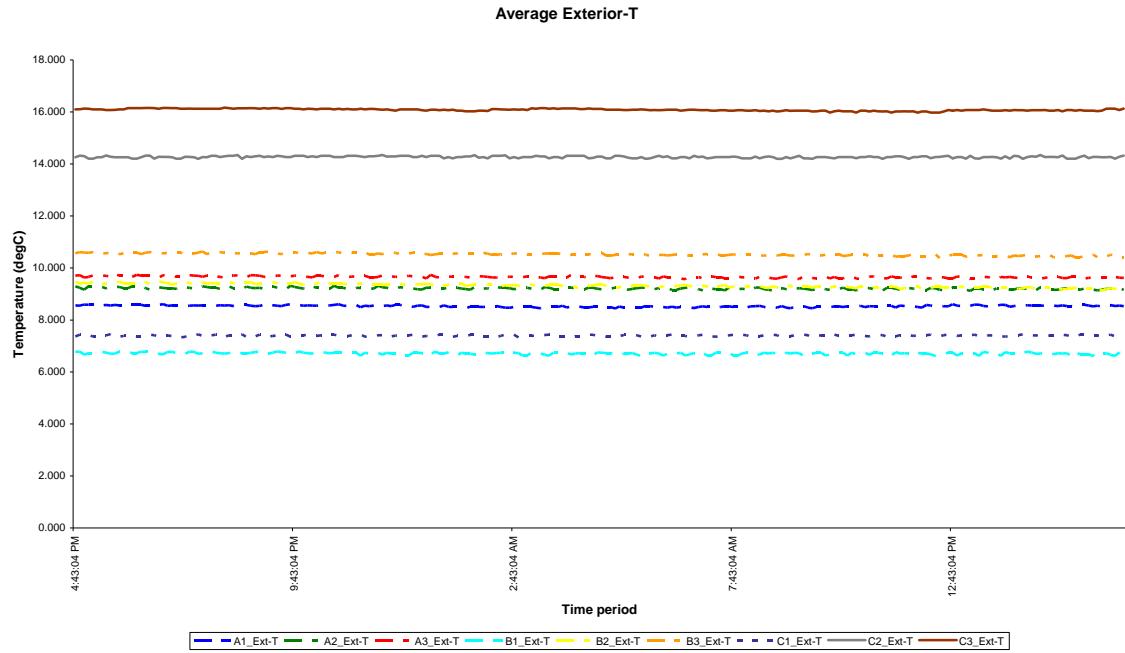


Figure B-85: Average exterior temperature of C1-Alt2

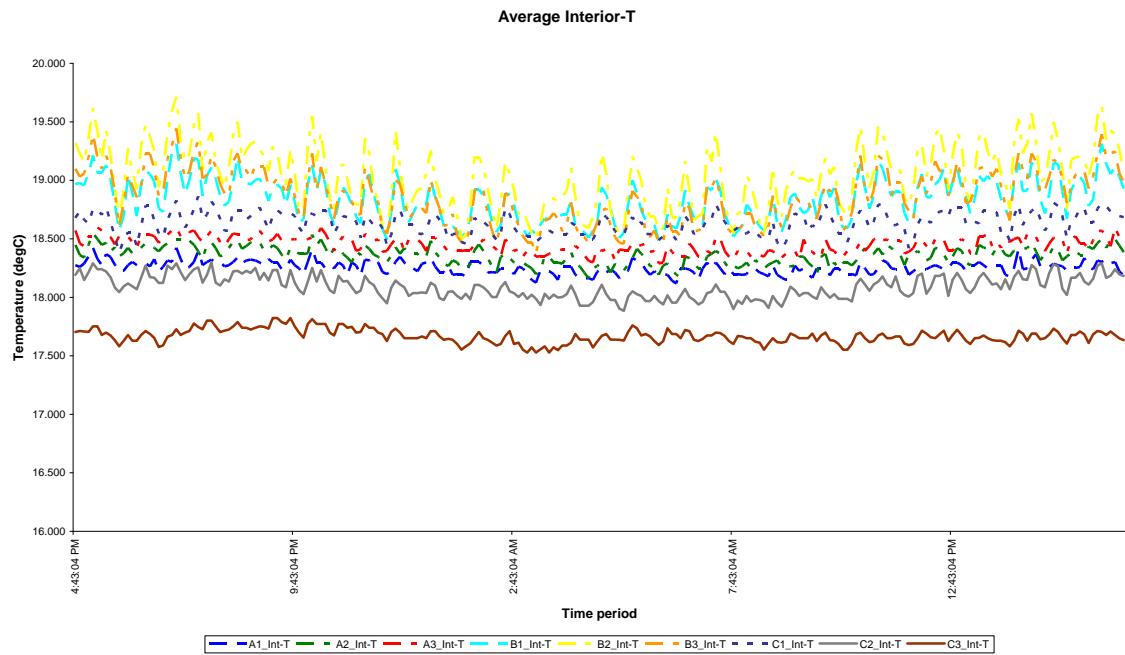


Figure B-86: Average interior temperature of C1-Alt2

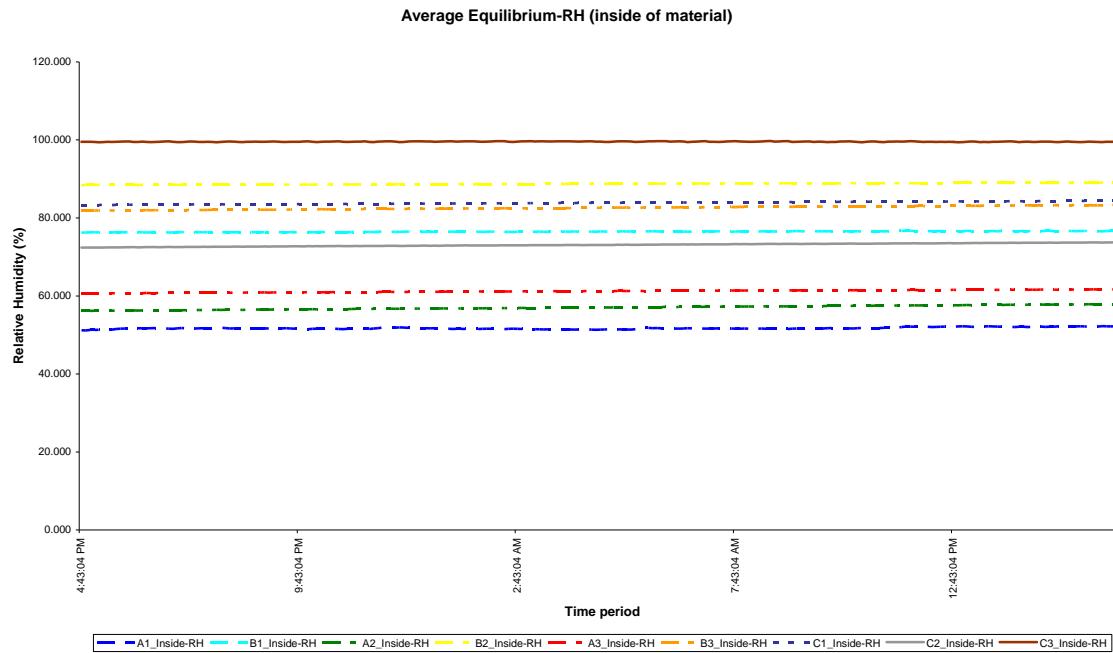


Figure B-87: Average equilibrium of relative humidity in a cavity of C1-Alt2

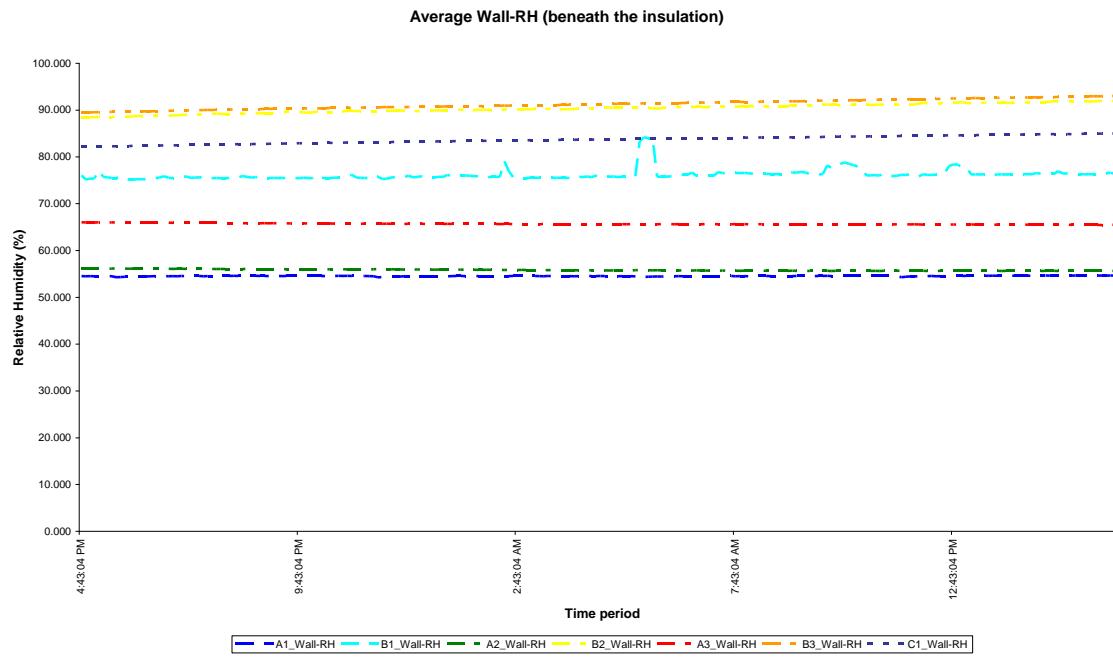


Figure B-88: Average wall relative humidity beneath the insulation of C1-Alt2

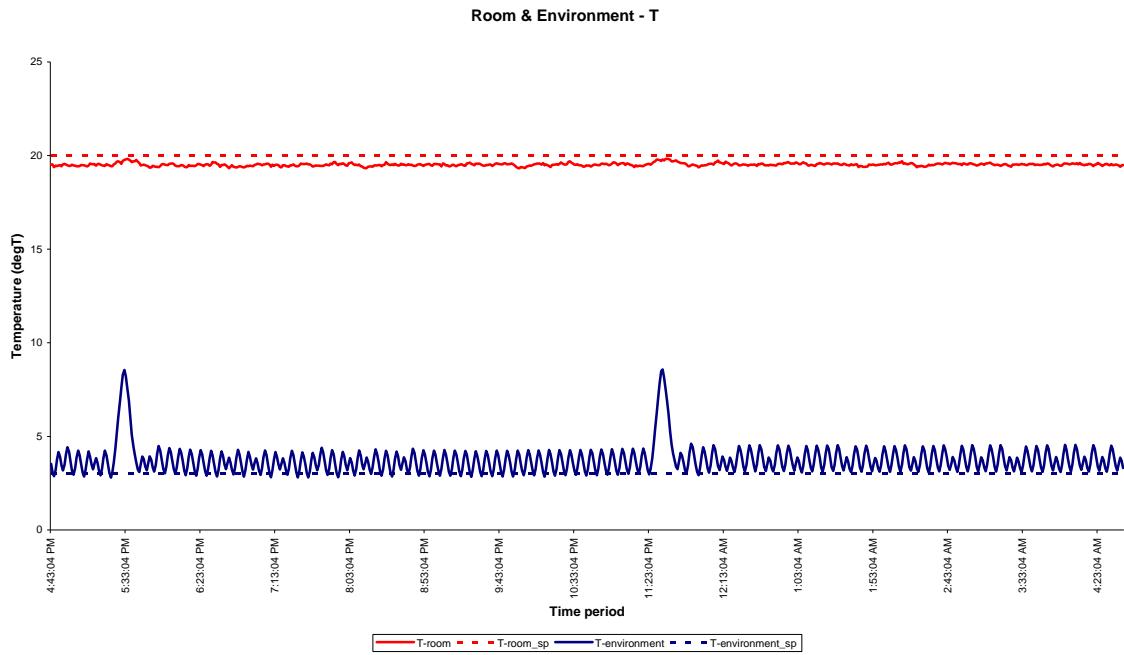


Figure B-89: Temperature of the room and environmental side during C1-Alt2

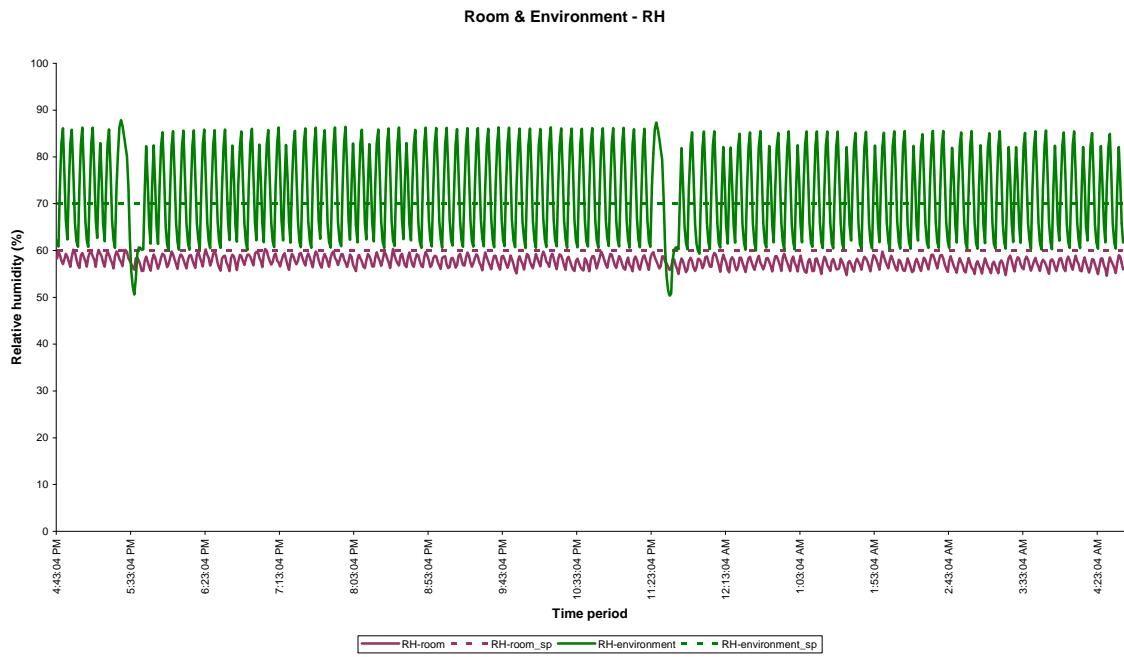


Figure B-90: Relative humidity of the room and environmental side during C1-Alt2

Test cycle: C1 – Alt3

Table B-11: Average data during the last 24 hours for each specimen of C1-Alt3

| Specimen Measurement Data | | | | | Control Loop Data | |
|---------------------------|--|---|---|------|---------------------------|-------------|
| B-G | A | B | C | Clay | Environmental / Room Side | |
| 1 | A1_Soil-T 6.103 degC A1_Soil-RH 100.000 % A1_Wall-T 16.662 degC A1_Ext-T 8.947 degC A1_Int-T 18.238 degC A1_Inside-RH 56.756 % A1_Wall-RH 56.682 % | B1_Soil-T 5.891 degC B1_Soil-RH 100.000 % B1_Wall-T 8.091 degC B1_Ext-T 7.082 degC B1_Int-T 18.881 degC B1_Inside-RH 80.698 % B1_Wall-RH 79.060 % | C1_Soil-T 5.914 degC C1_Soil-RH 100.000 % C1_Wall-T 9.073 degC C1_Ext-T 7.436 degC C1_Int-T 18.513 degC C1_Inside-RH 86.777 % C1_Wall-RH 89.496 % | 1 | T-room | 19.501 degC |
| 2 | A2_Soil-T 6.542 degC A2_Soil-RH 100.000 % A2_Wall-T 17.472 degC A2_Ext-T 9.394 degC A2_Int-T 18.363 degC A2_Inside-RH 60.963 % A2_Wall-RH 57.172 % | B2_Soil-T 6.090 degC B2_Soil-RH 100.000 % B2_Wall-T 10.433 degC B2_Ext-T 9.136 degC B2_Int-T 19.161 degC B2_Inside-RH 90.970 % B2_Wall-RH 97.143 % | C2_Soil-T 7.186 degC C2_Soil-RH 100.000 % C2_Ext-T 14.225 degC C2_Int-T 18.049 degC C2_Inside-RH 76.256 degC | 2 | RH-room | 58.168 % |
| 3 | A3_Soil-T 6.844 degC A3_Soil-RH 100.000 % A3_Wall-T 17.489 degC A3_Ext-T 9.864 degC A3_Int-T 18.427 degC A3_Inside-RH 63.358 % A3_Wall-RH 65.237 % | B3_Soil-T 7.044 degC B3_Soil-RH 100.000 % B3_Wall-T 11.586 degC B3_Ext-T 10.229 degC B3_Int-T 18.995 degC B3_Inside-RH 86.742 % B3_Wall-RH 97.647 % | C3_Soil-T 6.876 degC C3_Soil-RH 100.000 % C3_Ext-T 15.845 degC C3_Int-T 17.469 degC C3_Inside-RH 99.662 degC | 3 | T-room_sp | 20.000 degC |
| No | A | B | C | Alt3 | RH-room_sp | 60.000 % |

* Measured pressure difference between Room Side & Environmental Side


Figure B-91: Average soil temperature of C1-Alt3

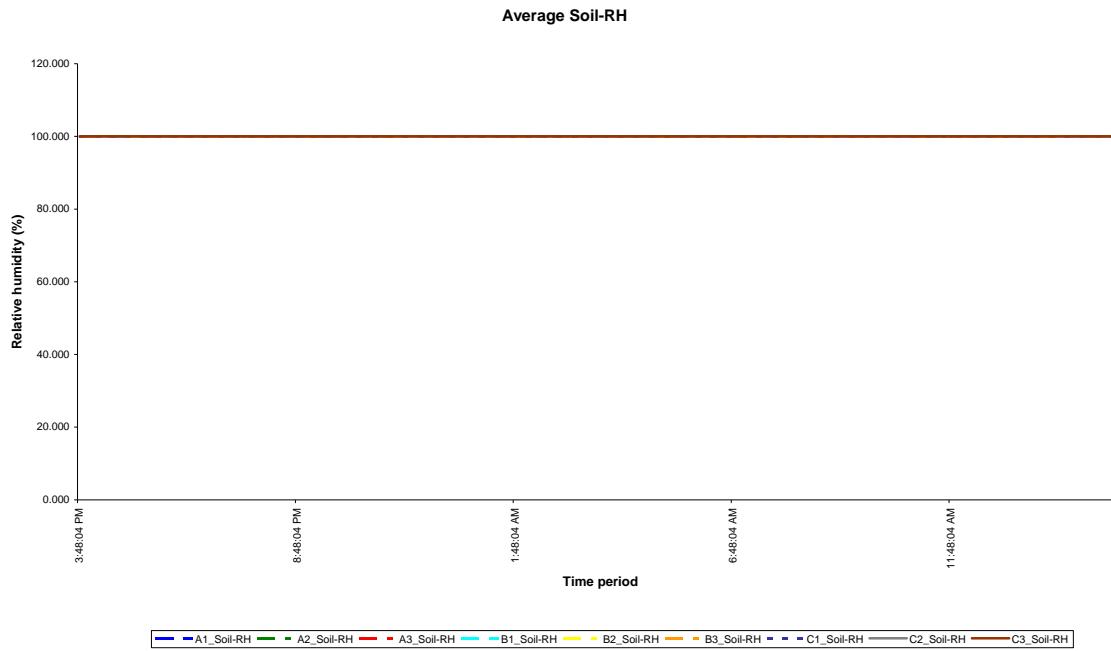


Figure B-92: Average soil relative humidity of C1-Alt3

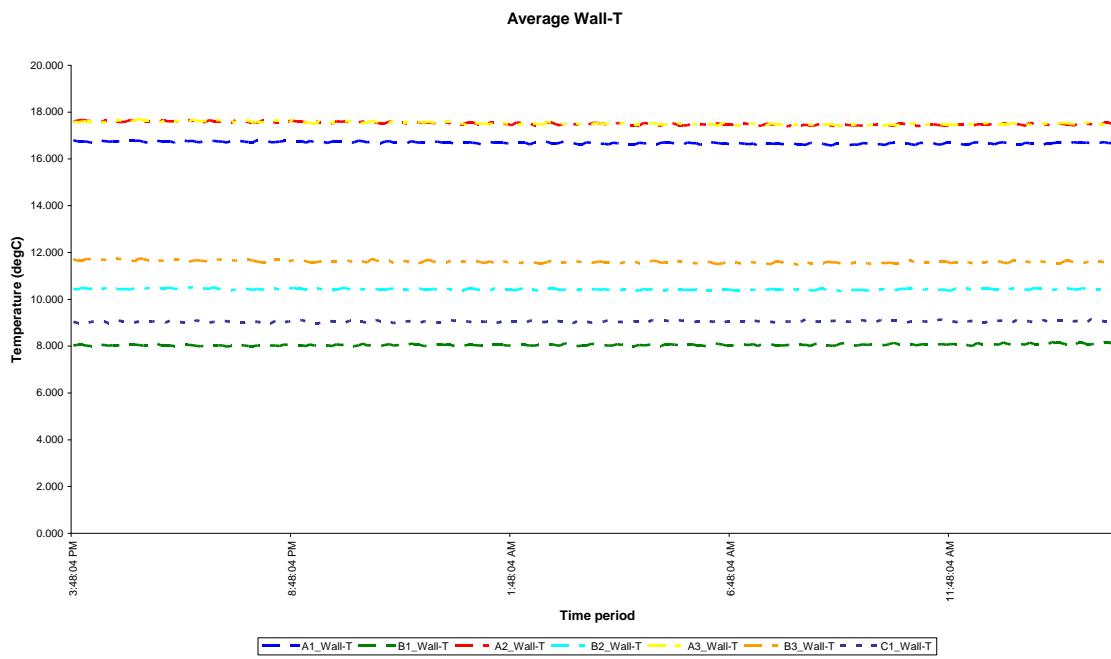


Figure B-93: Average wall temperature of C1-Alt3

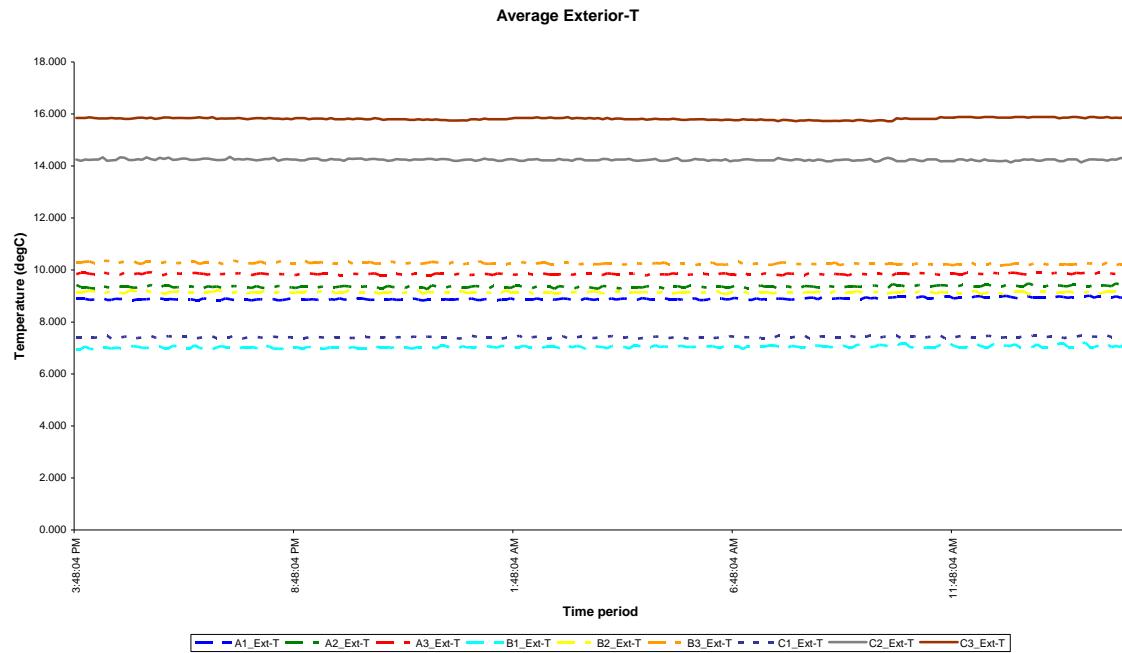


Figure B-94: Average exterior temperature of C1-Alt3

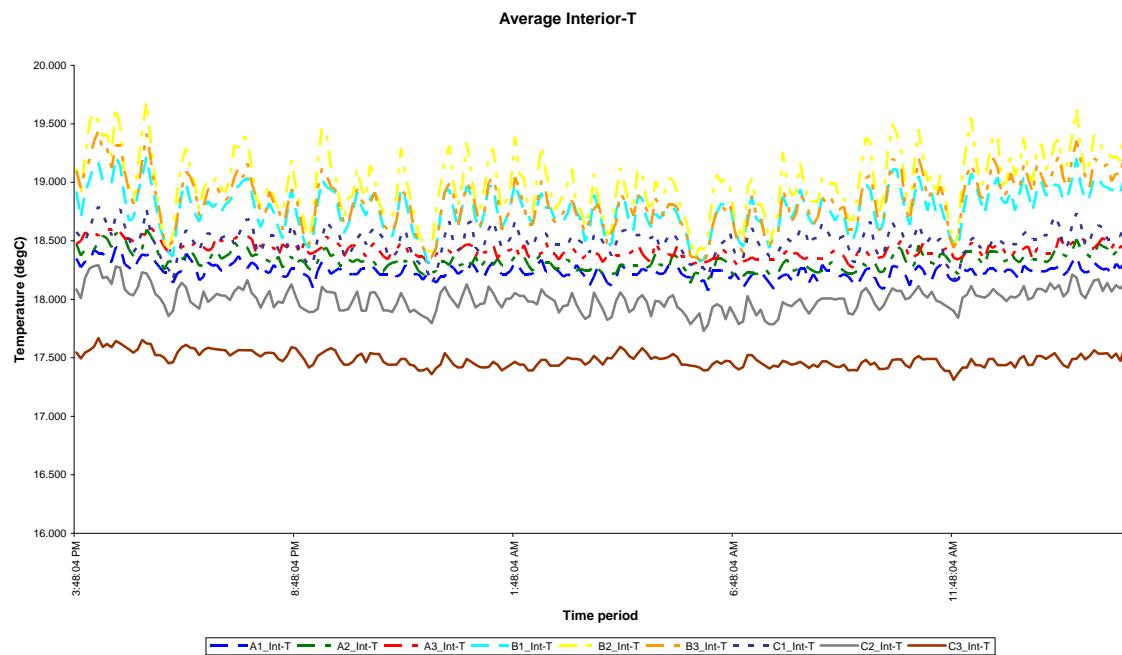


Figure B-95: Average interior temperature of C1-Alt3

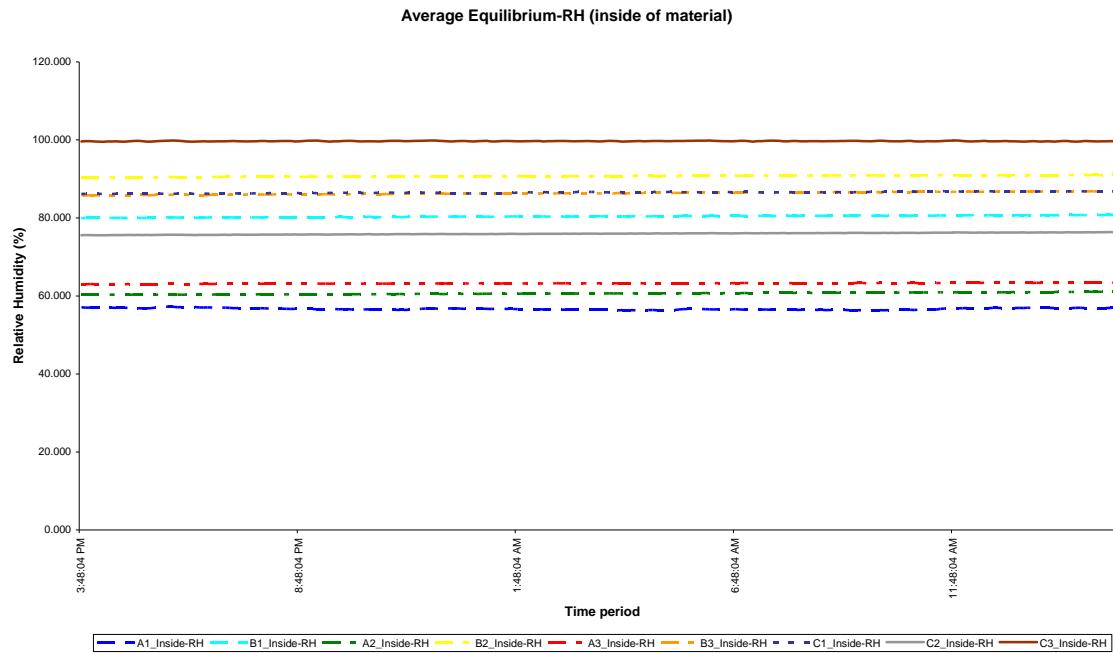


Figure B-96: Average equilibrium of relative humidity in a cavity of C1-Alt3

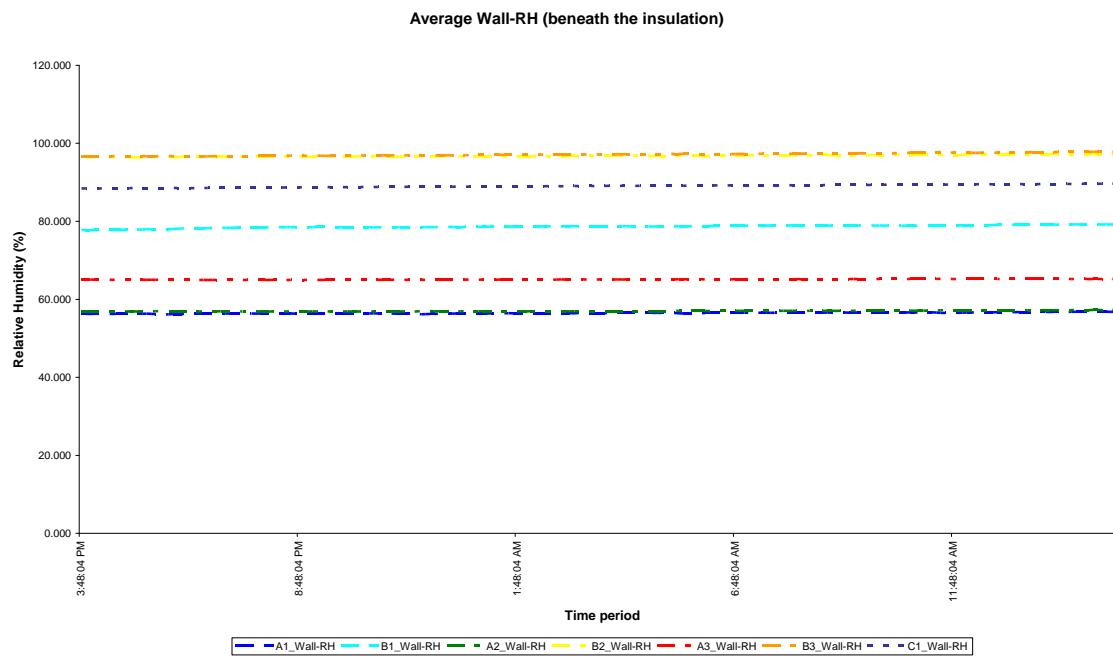


Figure B-97: Average wall relative humidity beneath the insulation of C1-Alt3

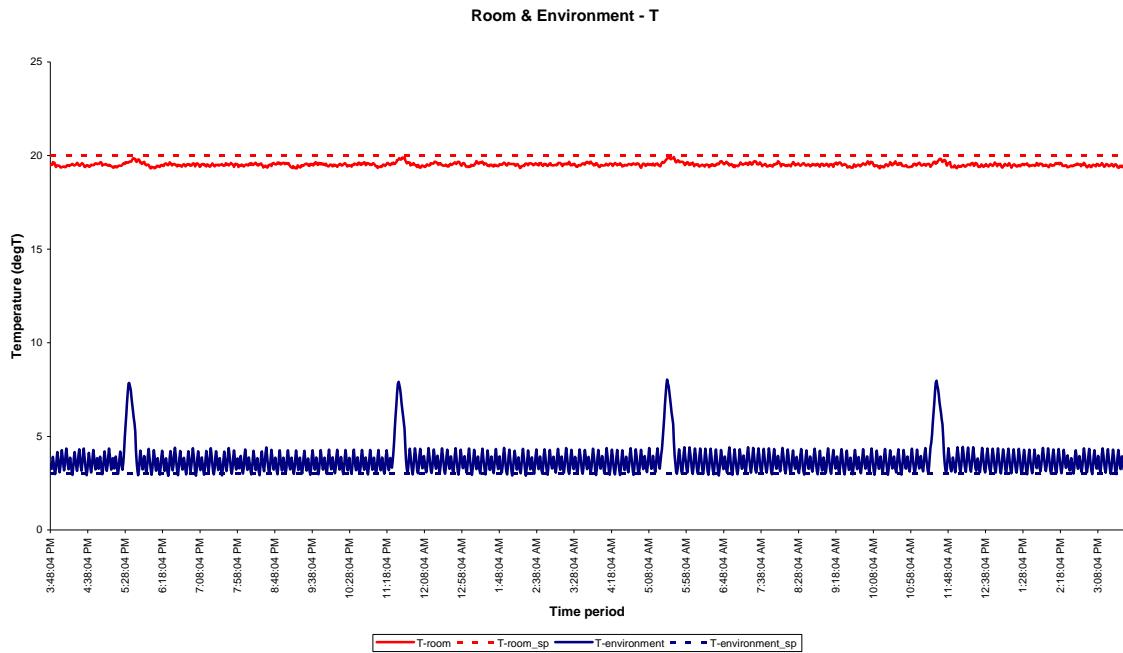


Figure B-98: Temperature of the room and environmental side during C1-Alt3

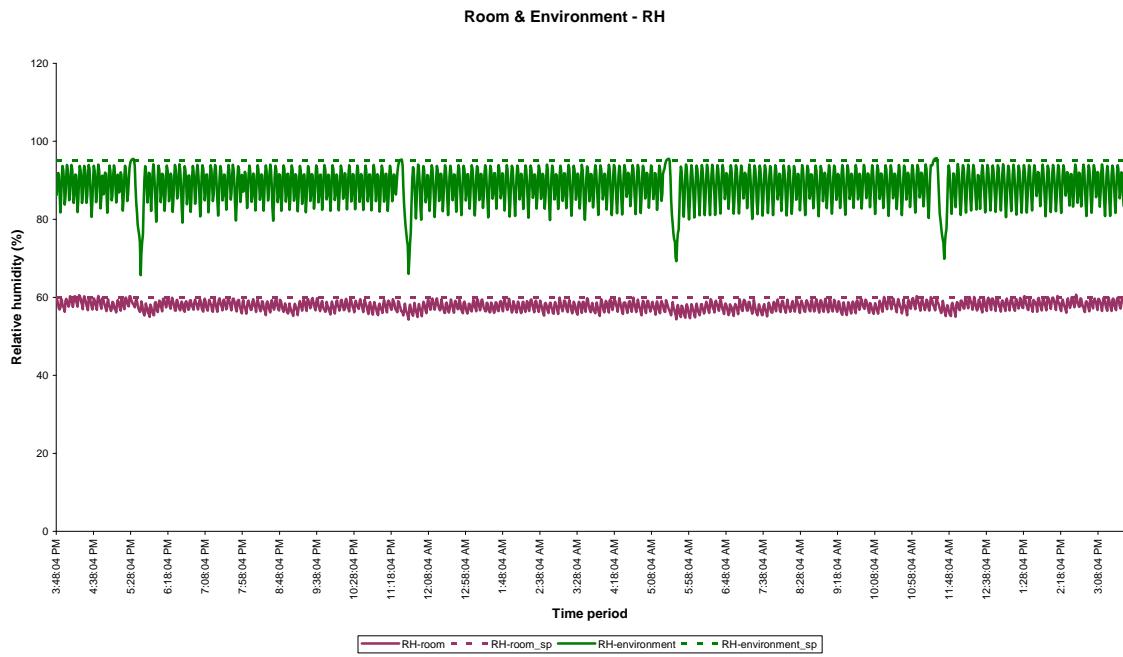


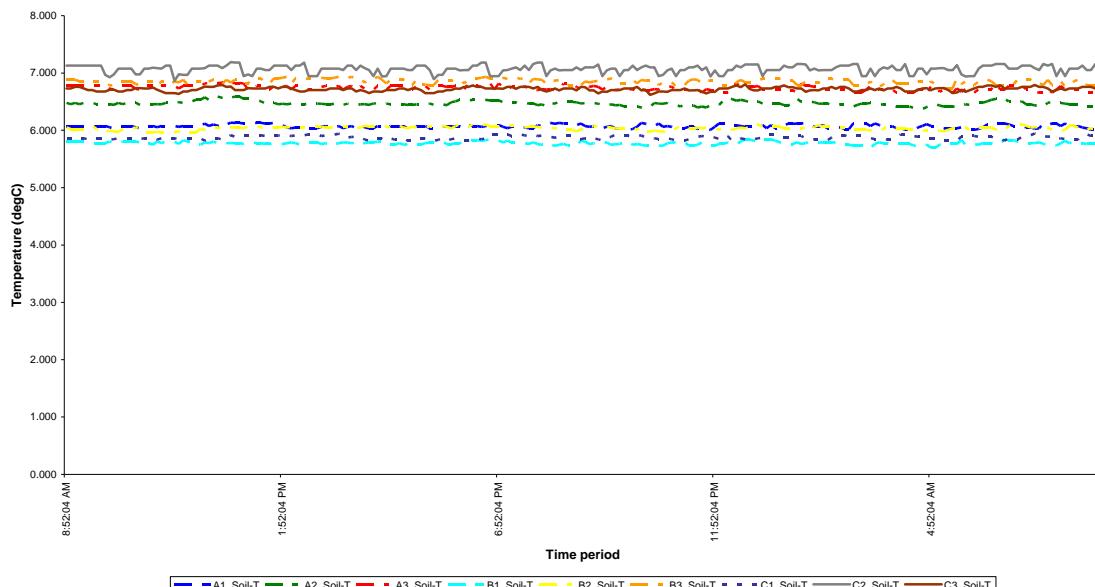
Figure B-99: Relative humidity of the room and environmental side during C1-Alt3

Test cycle: C1 – Alt4

Table B-12: Average data during the last 24 hours for each specimen of C1-Alt4

| Specimen Measurement Data | | | | | Control Loop Data | | | | | | | |
|---------------------------|--------------|-------------|--------------|-------------|-------------------|-------------|------|--|--|--|--|--|
| B-G | A | | B | | C | | Clay | | | | | |
| 1 | A1_Soil-T | 6.067 degC | B1_Soil-T | 5.764 degC | C1_Soil-T | 5.875 degC | 1 | | | | | |
| | A1_Soil-RH | 100.000 % | B1_Soil-RH | 100.000 % | C1_Soil-RH | 100.000 % | | | | | | |
| | A1_Wall-T | 16.653 degC | B1_Wall-T | 8.051 degC | C1_Wall-T | 8.908 degC | | | | | | |
| | A1_Ext-T | 9.010 degC | B1_Ext-T | 7.067 degC | C1_Ext-T | 7.351 degC | | | | | | |
| | A1_Int-T | 18.310 degC | B1_Int-T | 18.887 degC | C1_Int-T | 18.364 degC | | | | | | |
| | A1_Inside-RH | 48.464 % | B1_Inside-RH | 82.025 % | C1_Inside-RH | 88.386 % | | | | | | |
| 2 | A1_Wall-RH | 56.611 % | B1_Wall-RH | 74.710 % | C1_Wall-RH | 82.053 % | 2 | | | | | |
| | A2_Soil-T | 6.451 degC | B2_Soil-T | 6.032 degC | C2_Soil-T | 7.074 degC | | | | | | |
| | A2_Soil-RH | 100.000 % | B2_Soil-RH | 100.000 % | C2_Soil-RH | 100.000 % | | | | | | |
| | A2_Wall-T | 17.580 degC | B2_Wall-T | 10.299 degC | C2_Ext-T | 14.154 degC | | | | | | |
| | A2_Ext-T | 9.474 degC | B2_Ext-T | 9.062 degC | C2_Int-T | 17.964 degC | | | | | | |
| | A2_Int-T | 18.499 degC | B2_Int-T | 19.232 degC | C2_Inside-RH | 74.370 degC | | | | | | |
| 3 | A2_Inside-RH | 57.558 % | B2_Inside-RH | 91.991 % | | | 3 | | | | | |
| | A2_Wall-RH | 57.246 % | B2_Wall-RH | 93.441 % | | | | | | | | |
| | A3_Soil-T | 6.704 degC | B3_Soil-T | 6.822 degC | C3_Soil-T | 6.726 degC | | | | | | |
| | A3_Soil-RH | 100.000 % | B3_Soil-RH | 100.000 % | C3_Soil-RH | 100.000 % | | | | | | |
| | A3_Wall-T | 17.562 degC | B3_Wall-T | 11.071 degC | C3_Ext-T | 15.627 degC | | | | | | |
| | A3_Ext-T | 9.892 degC | B3_Ext-T | 9.854 degC | C3_Int-T | 17.339 degC | | | | | | |
| No | A3_Int-T | 18.537 degC | B3_Int-T | 19.090 degC | C3_Inside-RH | 99.636 degC | Alt4 | | | | | |
| | A3_Inside-RH | 59.636 % | B3_Inside-RH | 88.409 % | *Pressure diff. | | | | | | | |
| | A3_Wall-RH | 64.690 % | B3_Wall-RH | 72.948 % | | | | | | | | |

* Measured pressure difference between Room Side & Environmental Side

Average Soil-T

Figure B-100: Average soil temperature of C1-Alt4

Insulated Concrete Masonry Below-grade Walls

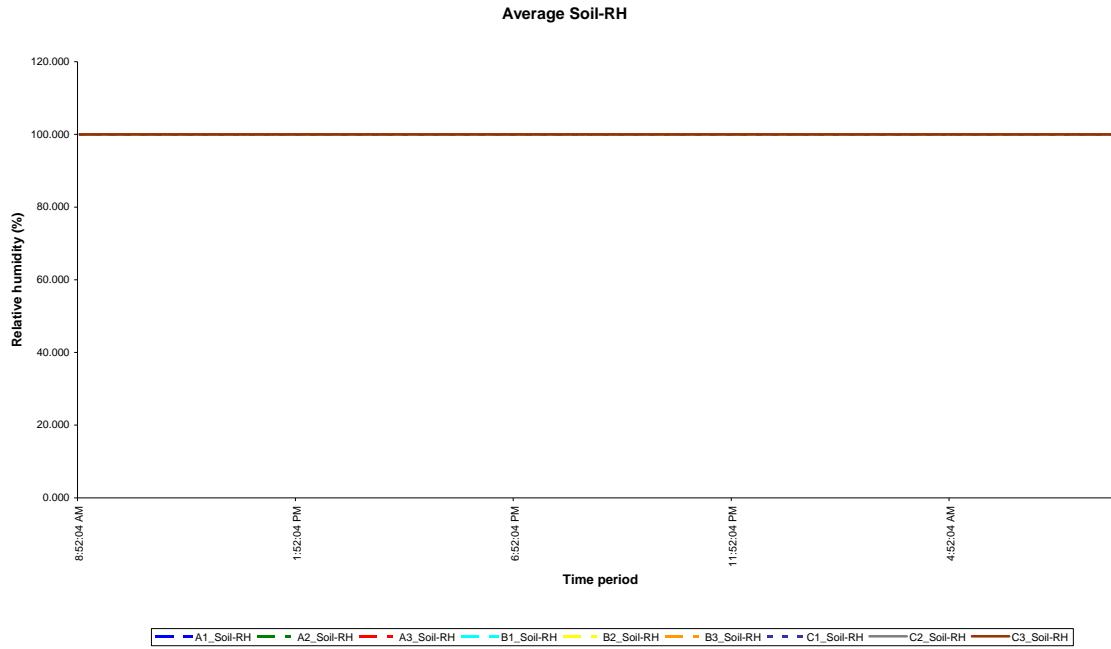


Figure B-101: Average soil relative humidity of C1-Alt4

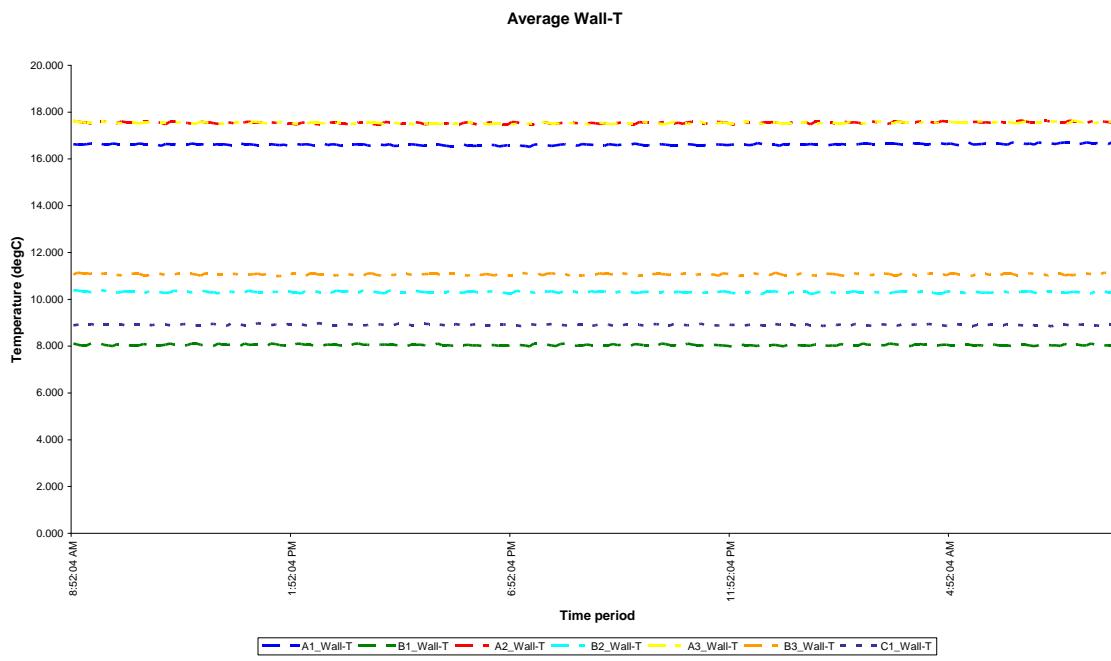


Figure B-102: Average wall temperature of C1-Alt4

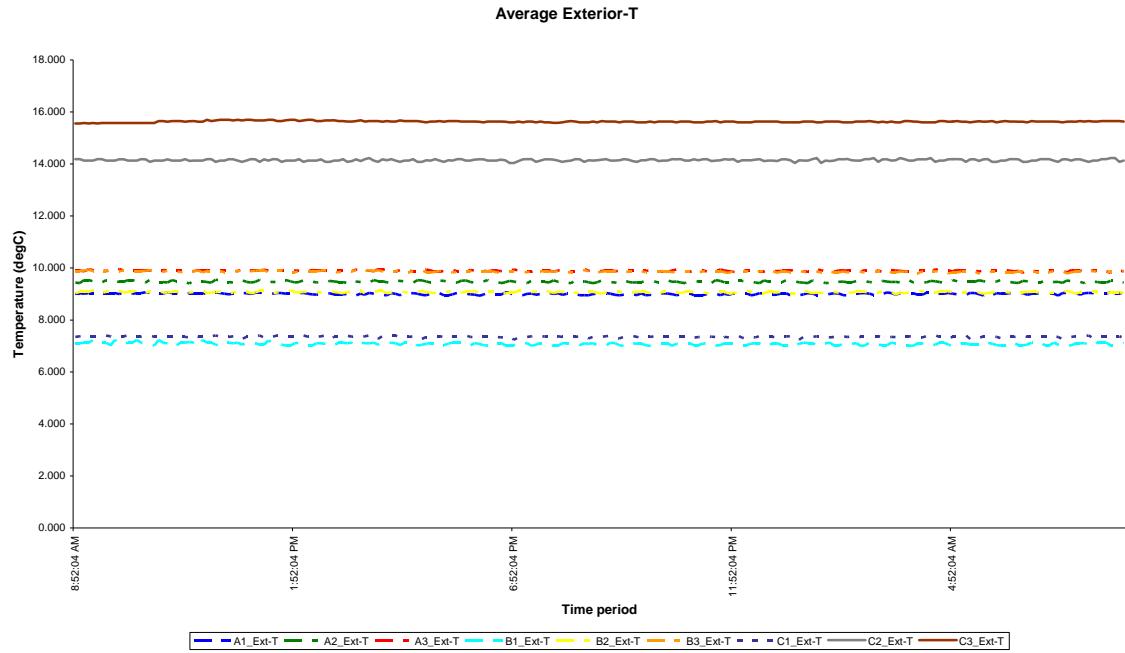


Figure B-103: Average exterior temperature of C1-Alt4

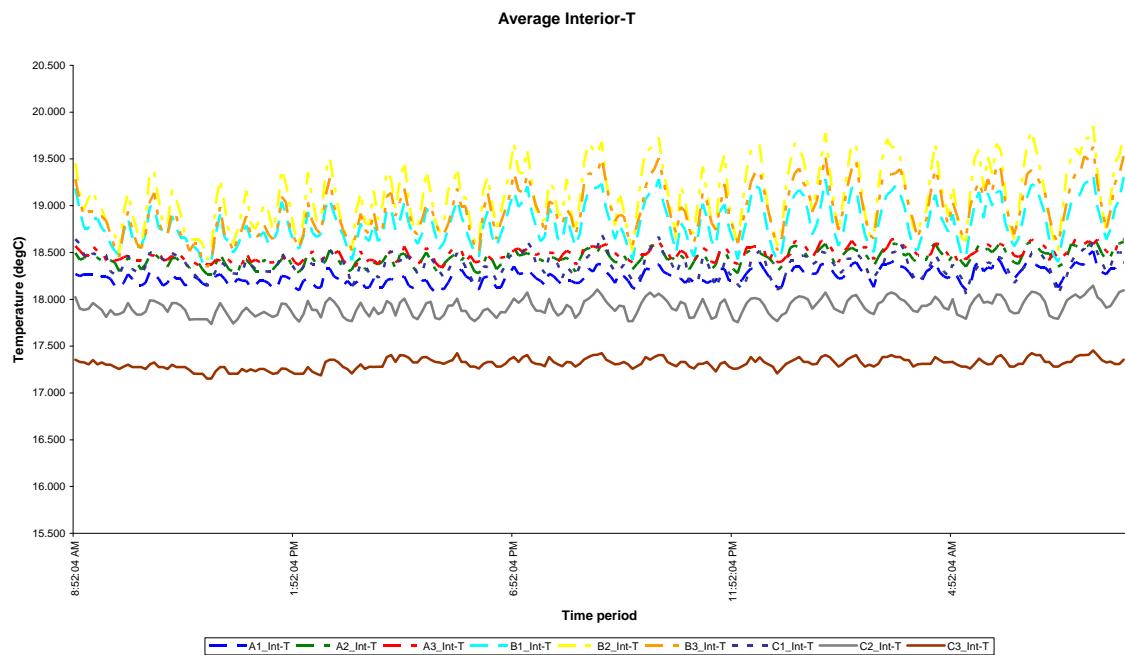


Figure B-104: Average interior temperature of C1-Alt4

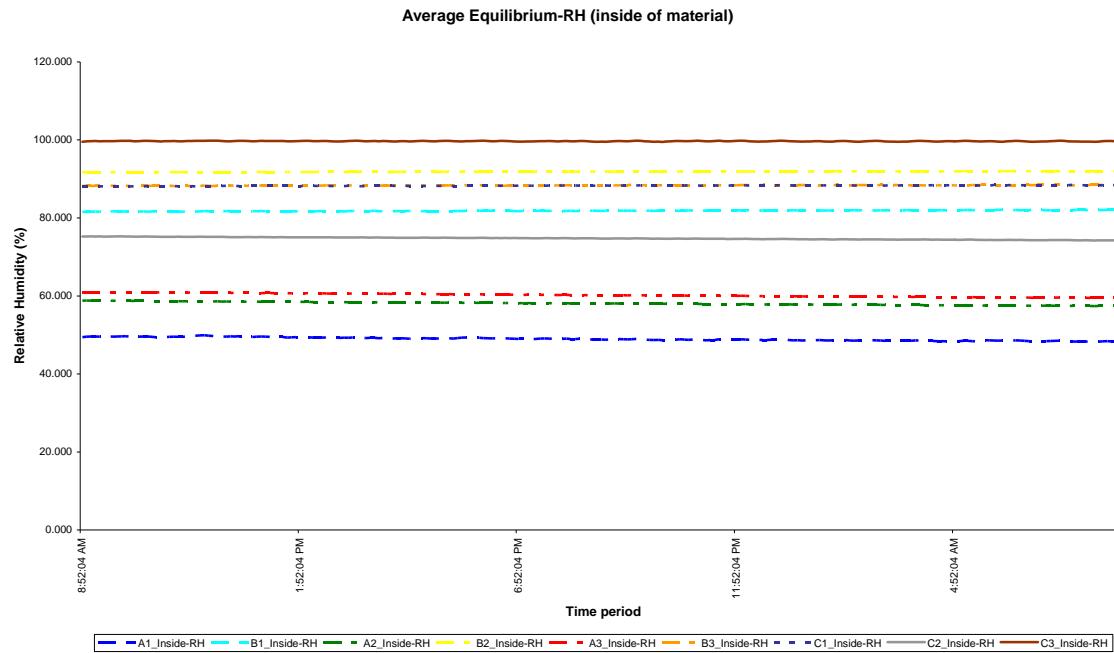


Figure B-105: Average equilibrium of relative humidity in a cavity of C1-Alt4

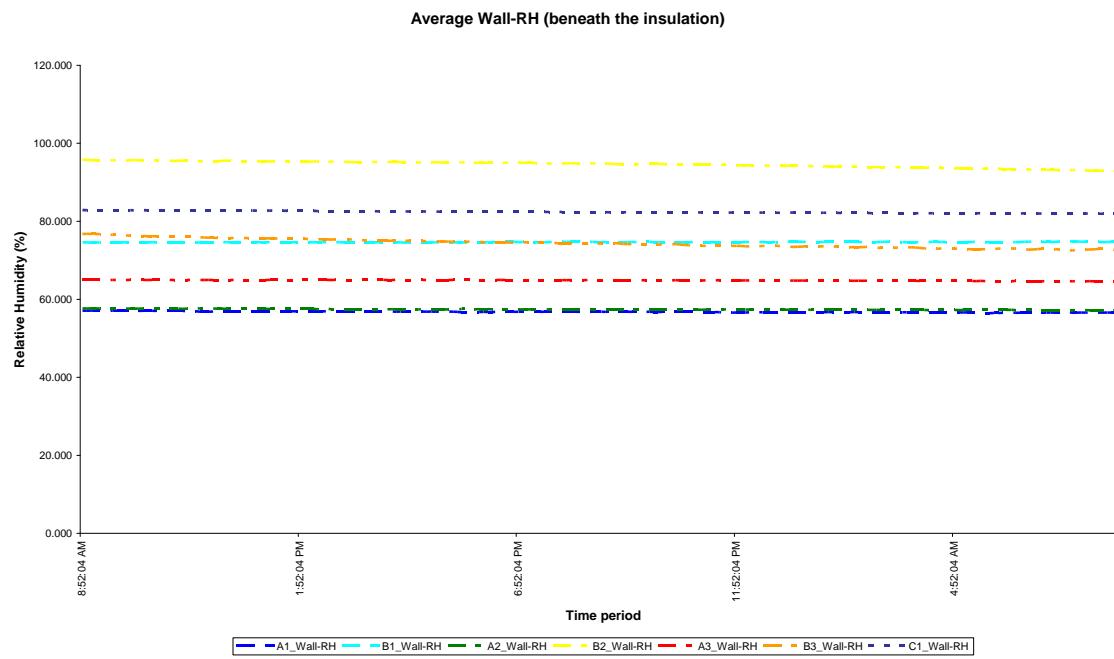


Figure B-106: Average wall relative humidity beneath the insulation of C1-Alt4

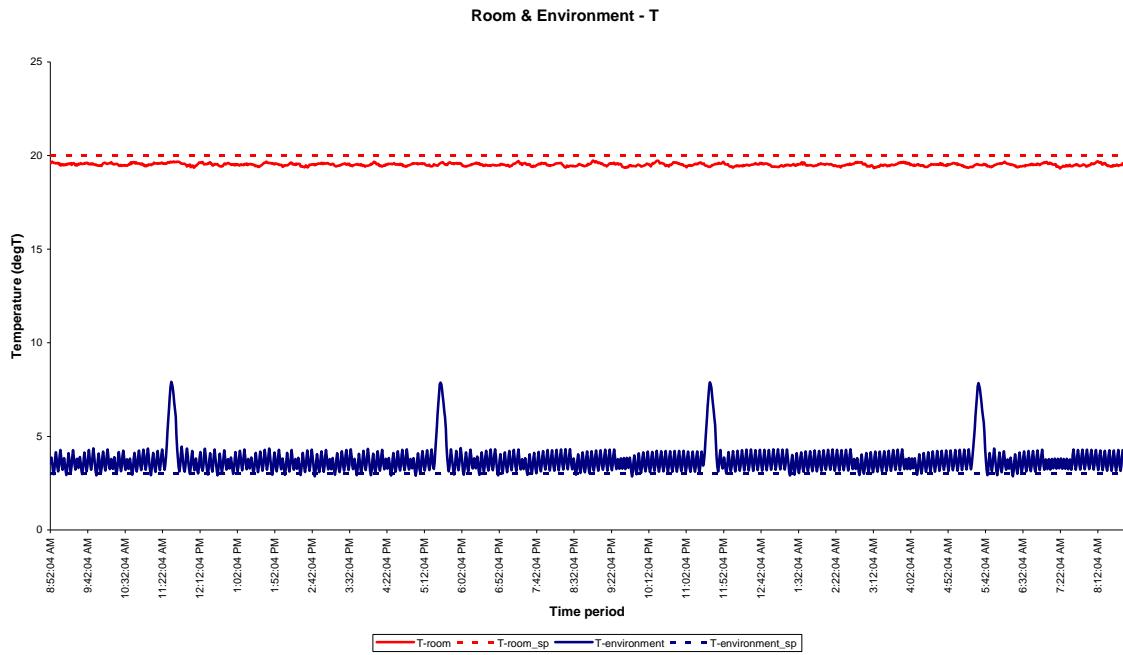


Figure B-107: Temperature of the room and environmental side during C1-Alt4



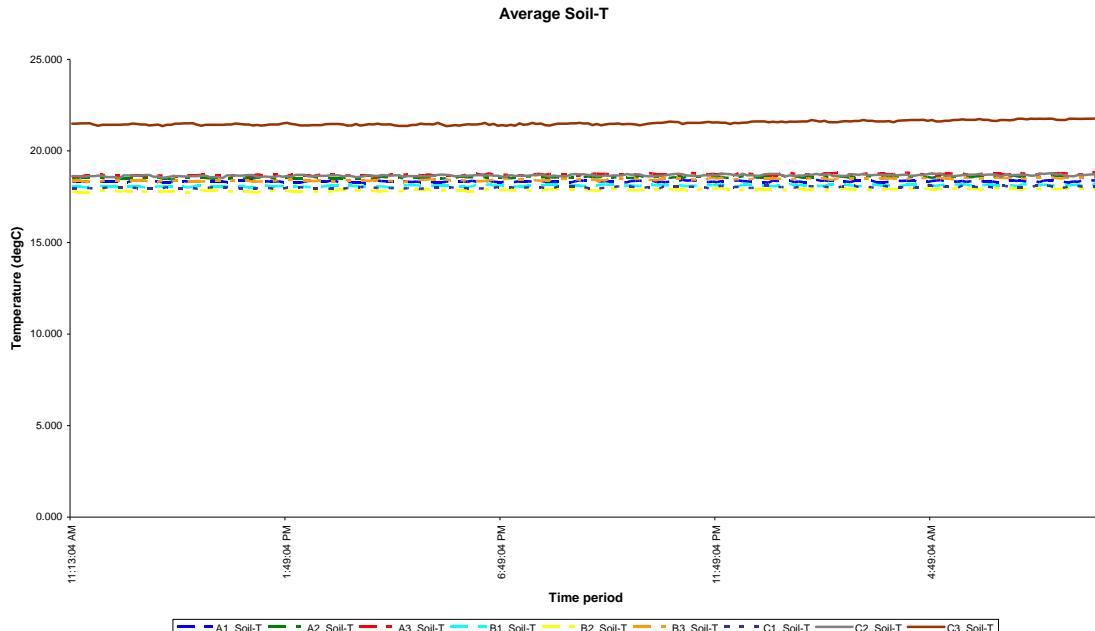
Figure B-108: Relative humidity of the room and environmental side during C1-Alt4

Test cycle: C1 – Alt5

Table B-13: Average data during the last 24 hours for each specimen of C1-Alt5

| Specimen Measurement Data | | | | Control Loop Data | | |
|---------------------------|--|--|--|-------------------|--|--|
| B-G | A | B | C | Clay | | |
| 1 | A1_Soil-T 18.342 degC A1_Soil-RH 100.000 % A1_Wall-T 18.733 degC A1_Ext-T 19.030 degC A1_Int-T 18.828 degC A1_Inside-RH 55.444 % A1_Wall-RH 66.760 % | B1_Soil-T 18.138 degC B1_Soil-RH 100.000 % B1_Wall-T 18.154 degC B1_Ext-T 17.966 degC B1_Int-T 18.987 degC B1_Inside-RH 81.824 % B1_Wall-RH 66.660 % | C1_Soil-T 18.044 degC C1_Soil-RH 100.000 % C1_Wall-T 18.361 degC C1_Ext-T 18.036 degC C1_Int-T 18.697 degC C1_Inside-RH 88.459 % C1_Wall-RH 66.345 % | 1 | T-room 19.510 degC RH-room 27.751 % T-room_sp 20.000 degC RH-room_sp 30.000 % T-environment 19.443 degC RH-environment 49.641 % T-environment_sp 20.000 degC RH-environment_sp 50.000 % | |
| 2 | A2_Soil-T 18.596 degC A2_Soil-RH 100.000 % A2_Wall-T 18.581 degC A2_Ext-T 18.560 degC A2_Int-T 18.554 degC A2_Inside-RH 56.455 % A2_Wall-RH 75.235 % | B2_Soil-T 17.927 degC B2_Soil-RH 100.000 % B2_Wall-T 17.414 degC B2_Ext-T 17.057 degC B2_Int-T 18.885 degC B2_Inside-RH 91.984 % B2_Wall-RH 87.266 % | C2_Soil-T 18.691 degC C2_Soil-RH 100.000 % C2_Ext-T 18.736 degC C2_Int-T 18.649 degC C2_Inside-RH 73.101 degC | 2 | Type: B-G Soil type: Clay Damp proofing: No Alternative: Alt5 | |
| 3 | A3_Soil-T 18.746 degC A3_Soil-RH 100.000 % A3_Wall-T 18.689 degC A3_Ext-T 18.472 degC A3_Int-T 18.663 degC A3_Inside-RH 60.005 % A3_Wall-RH 98.430 % | B3_Soil-T 18.510 degC B3_Soil-RH 99.781 % B3_Wall-T 17.766 degC B3_Ext-T 17.541 degC B3_Int-T 18.672 degC B3_Inside-RH 84.412 % B3_Wall-RH 44.563 % | C3_Soil-T 21.692 degC C3_Soil-RH 100.000 % C3_Ext-T 19.548 degC C3_Int-T 19.004 degC C3_Inside-RH 100.000 degC | 3 | T - Temperature (degC) RH - Relative Humidity (%) SP - Setpoint (either T or RH) | |
| No | A | B | C | Alt5 | | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-109: Average soil temperature of C1-Alt5

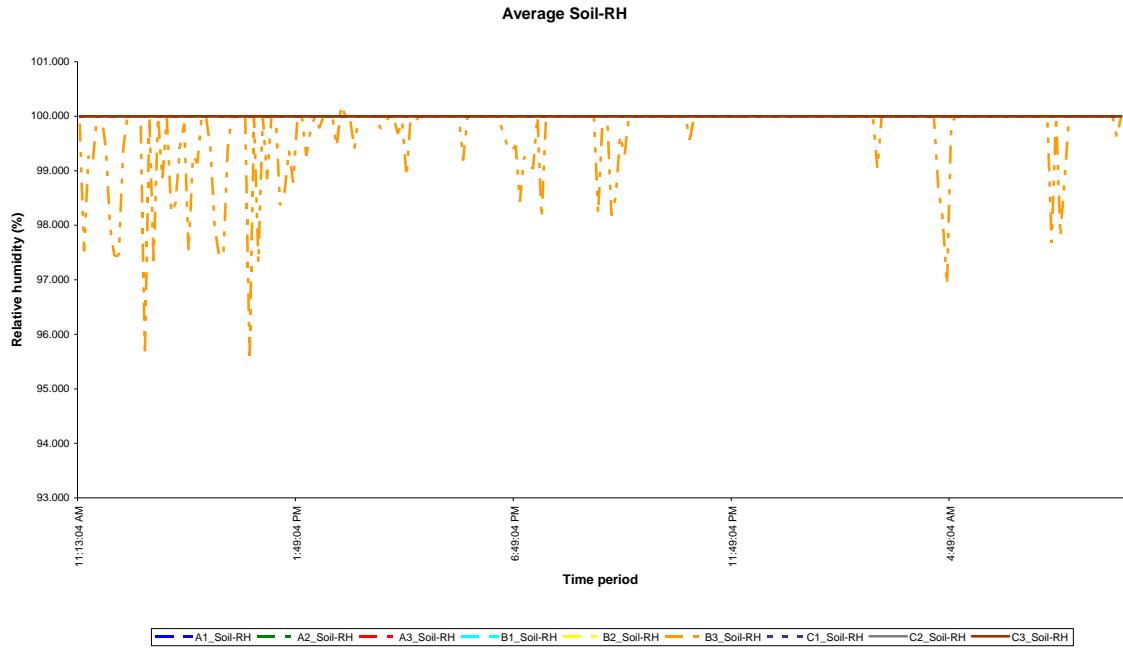


Figure B-110: Average soil relative humidity of C1-Alt5

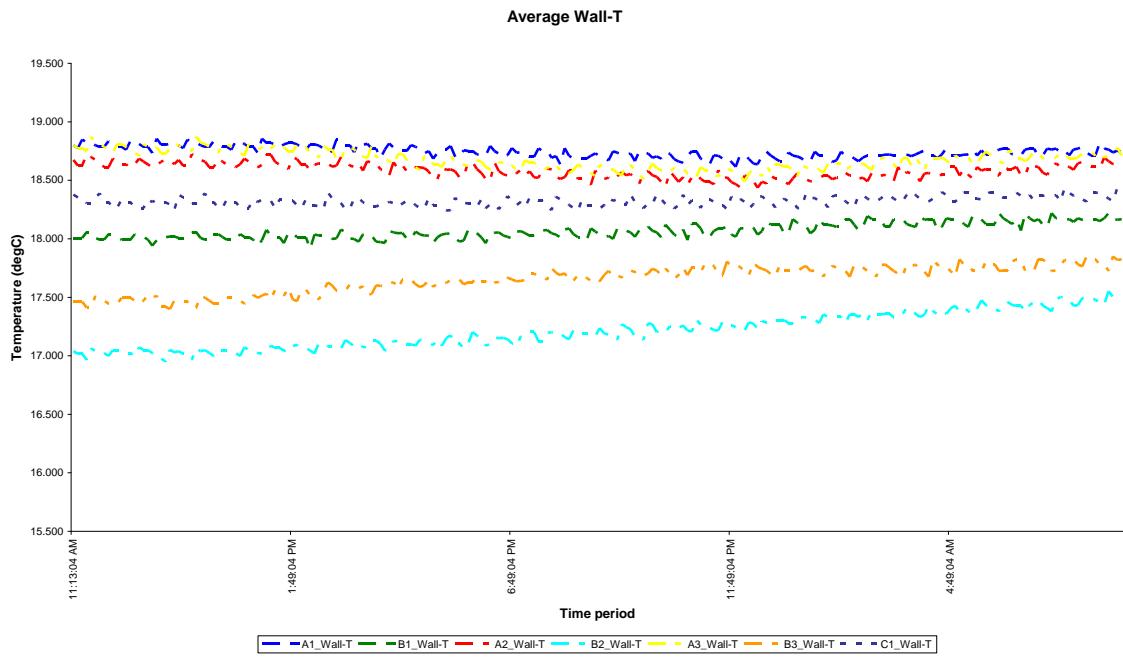


Figure B-111: Average wall temperature of C1-Alt5

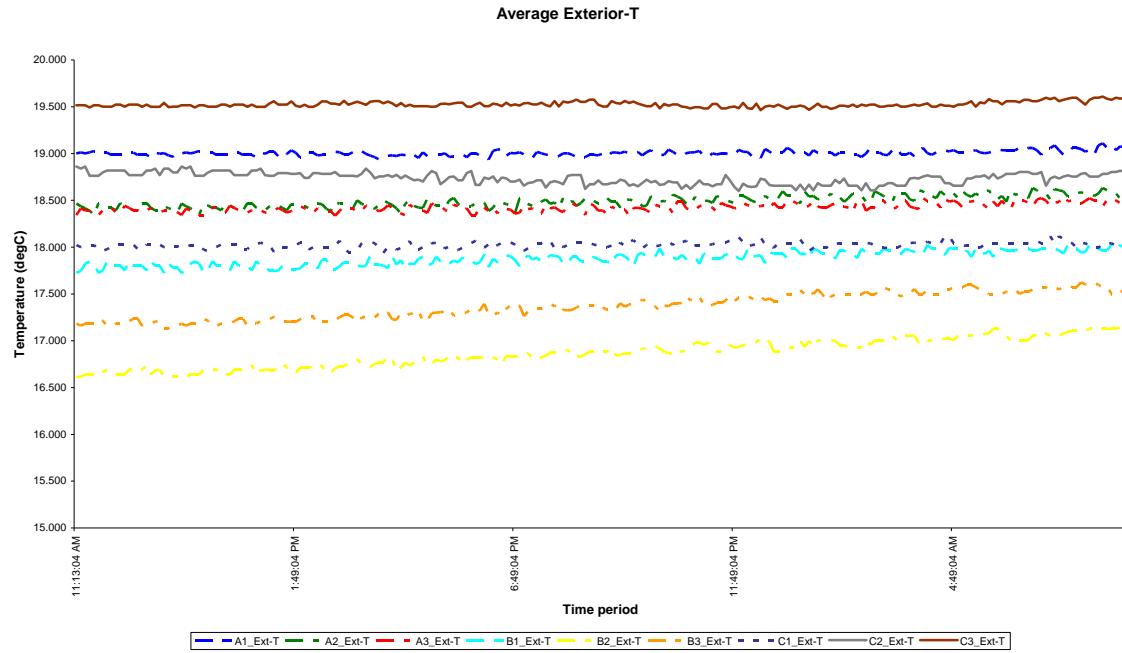


Figure B-112: Average exterior temperature of C1-Alt5

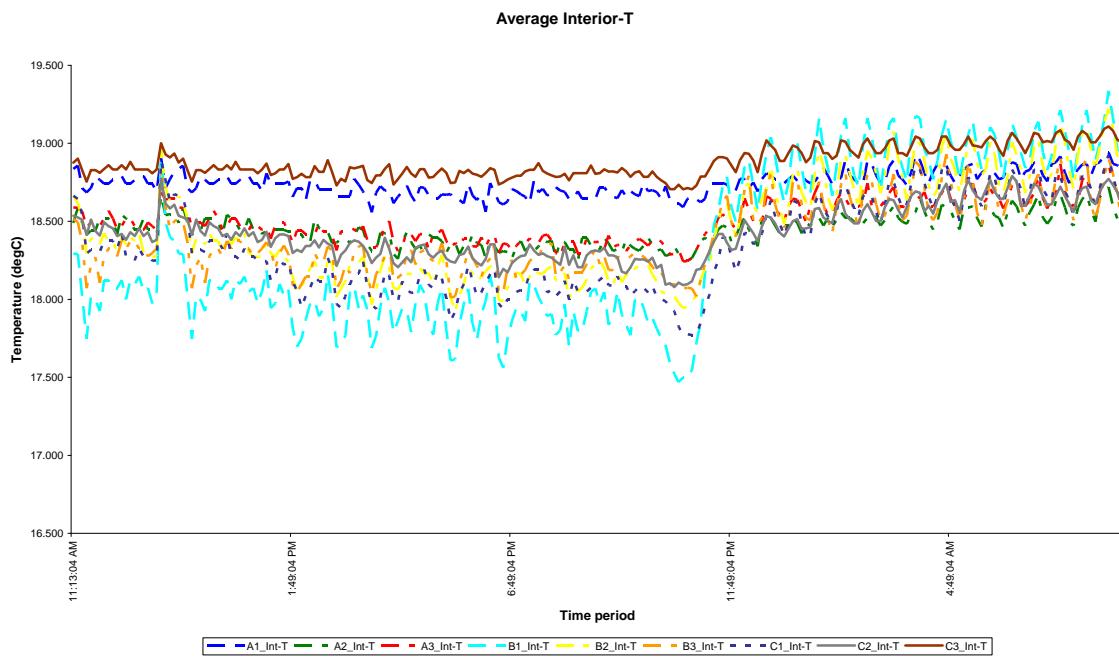


Figure B-113: Average interior temperature of C1-Alt5

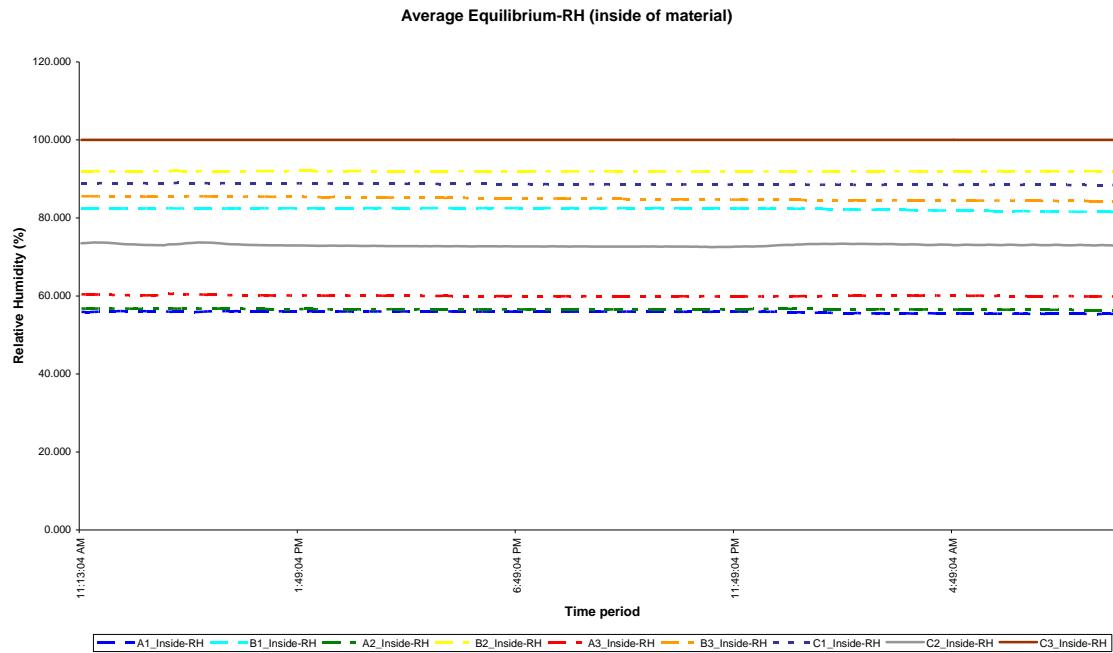


Figure B-114: Average equilibrium of relative humidity in a cavity of C1-Alt5

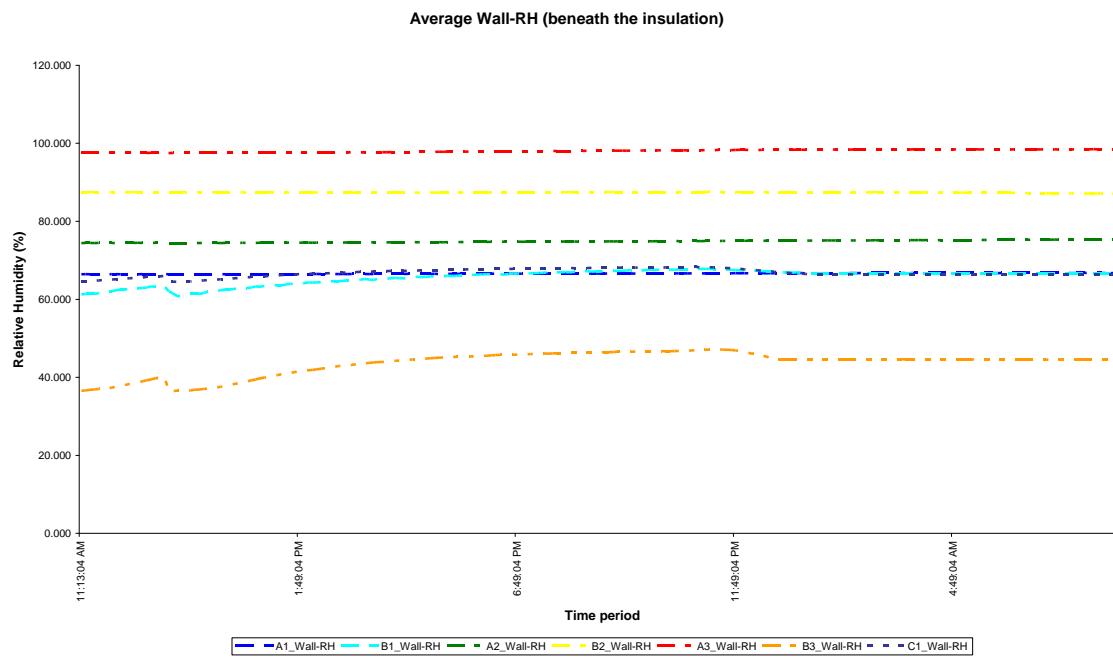


Figure B-115: Average wall relative humidity beneath the insulation of C1-Alt5

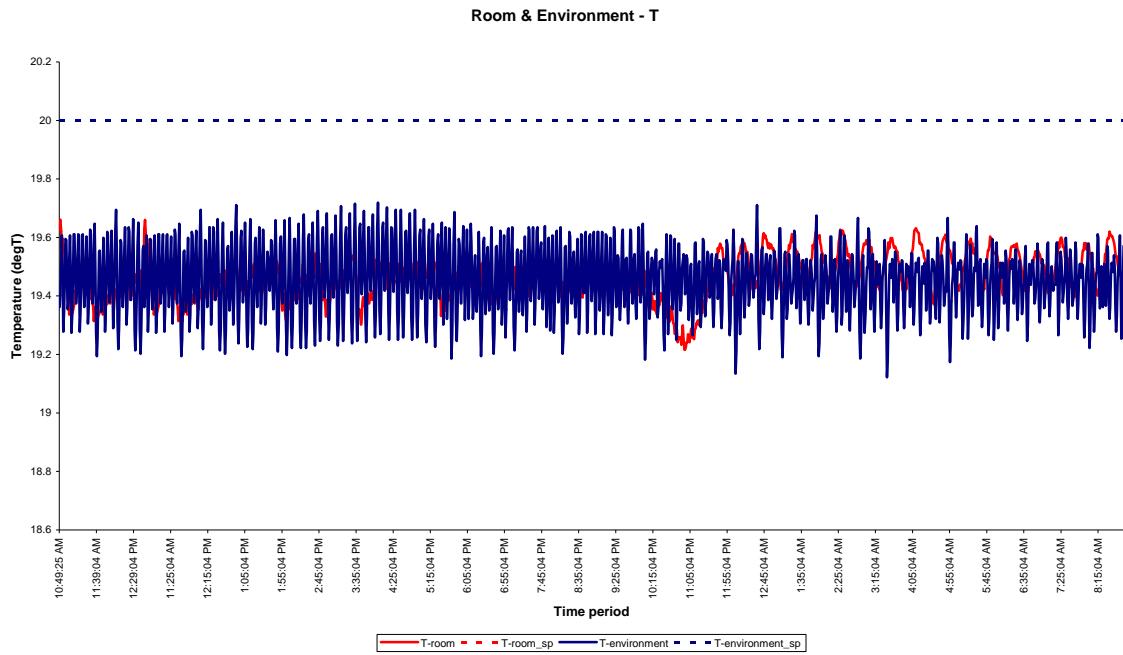


Figure B-116: Temperature of the room and environmental side during C1-Alt5

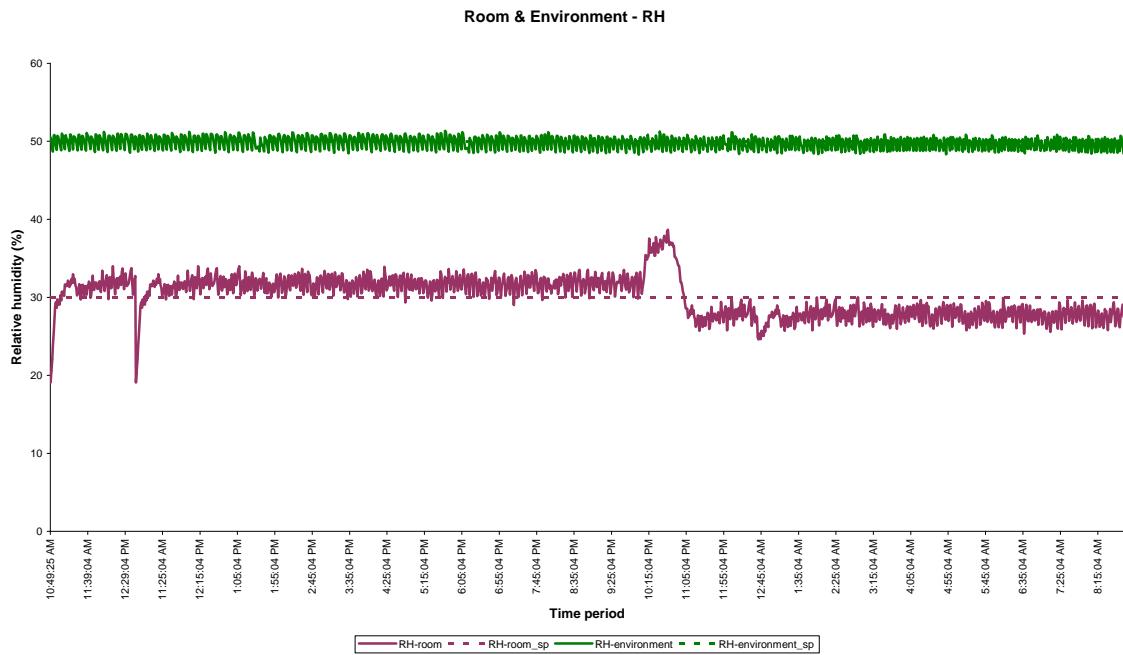


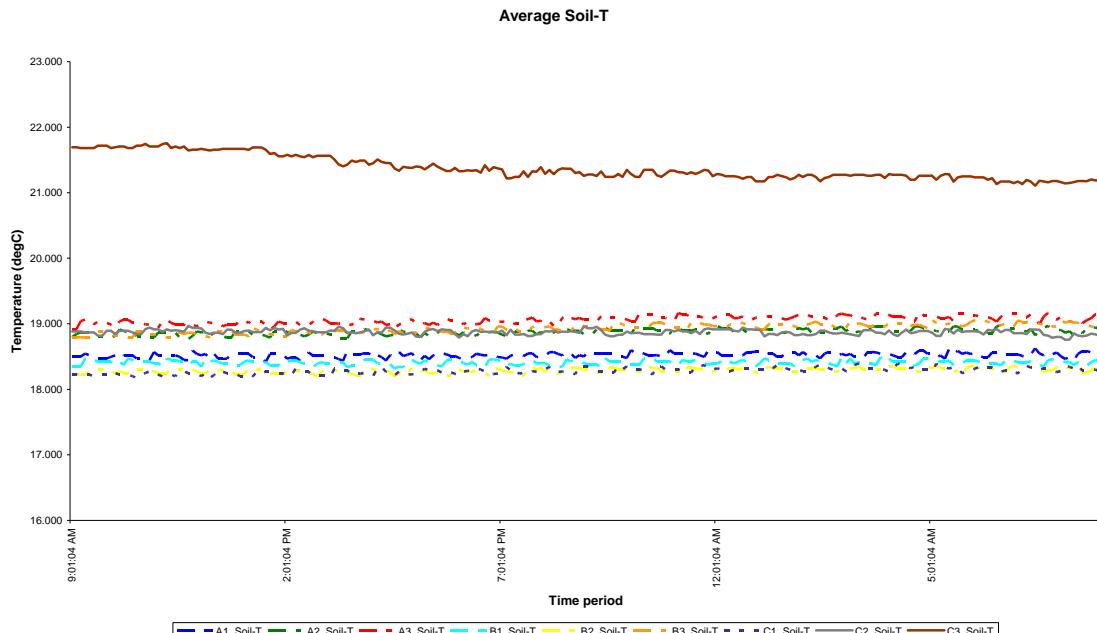
Figure B-117: Relative humidity of the room and environmental side during C1-Alt5

Test cycle: C1 – Alt6

Table B-14: Average data during the last 24 hours for each specimen of C1-Alt6

| Specimen Measurement Data | | | | Control Loop Data | | |
|---------------------------|--|--|--|-------------------|--|--|
| B-G | A | B | C | Clay | | |
| 1 | A1_Soil-T 18.535 degC A1_Soil-RH 100.000 % A1_Wall-T 18.645 degC A1_Ext-T 19.101 degC A1_Int-T 18.529 degC A1_Inside-RH 60.662 % A1_Wall-RH 67.717 % | B1_Soil-T 18.414 degC B1_Soil-RH 100.000 % B1_Wall-T 18.496 degC B1_Ext-T 18.349 degC B1_Int-T 18.680 degC B1_Inside-RH 82.128 % B1_Wall-RH 74.633 % | C1_Soil-T 18.316 degC C1_Soil-RH 100.000 % C1_Wall-T 18.609 degC C1_Ext-T 18.294 degC C1_Int-T 18.449 degC C1_Inside-RH 88.078 % C1_Wall-RH 76.833 % | 1 | | |
| 2 | A2_Soil-T 18.909 degC A2_Soil-RH 100.000 % A2_Wall-T 18.512 degC A2_Ext-T 18.815 degC A2_Int-T 18.286 degC A2_Inside-RH 60.079 % A2_Wall-RH 76.887 % | B2_Soil-T 18.311 degC B2_Soil-RH 100.000 % B2_Wall-T 18.161 degC B2_Ext-T 17.835 degC B2_Int-T 18.661 degC B2_Inside-RH 91.547 % B2_Wall-RH 85.828 % | C2_Soil-T 18.859 degC C2_Soil-RH 100.000 % C2_Ext-T 18.866 degC C2_Int-T 18.610 degC C2_Inside-RH 74.597 degC | 2 | | |
| 3 | A3_Soil-T 19.103 degC A3_Soil-RH 100.000 % A3_Wall-T 18.669 degC A3_Ext-T 18.723 degC A3_Int-T 18.408 degC A3_Inside-RH 64.856 % A3_Wall-RH 99.940 % | B3_Soil-T 18.996 degC B3_Soil-RH 100.000 % B3_Wall-T 18.588 degC B3_Ext-T 18.289 degC B3_Int-T 18.580 degC B3_Inside-RH 84.288 % B3_Wall-RH 71.781 % | C3_Soil-T 21.216 degC C3_Soil-RH 100.000 % C3_Ext-T 19.684 degC C3_Int-T 18.914 degC C3_Inside-RH 100.000 degC | 3 | | |
| No | A | B | C | Alt6 | | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-118: Average soil temperature of C1-Alt6

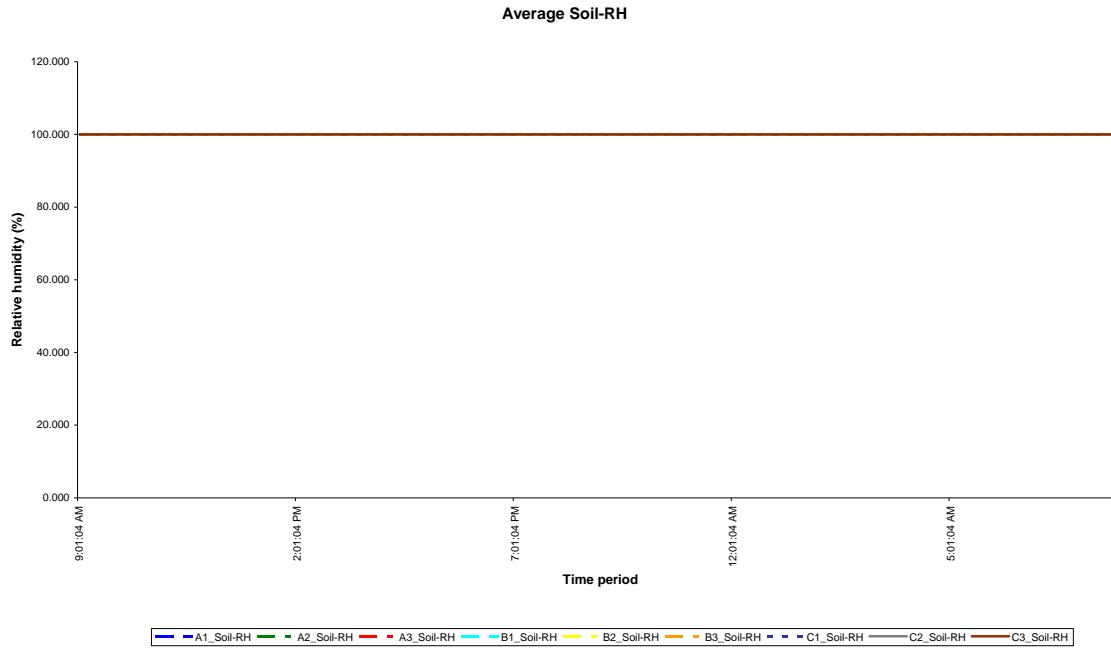


Figure B-119: Average soil relative humidity of C1-Alt6

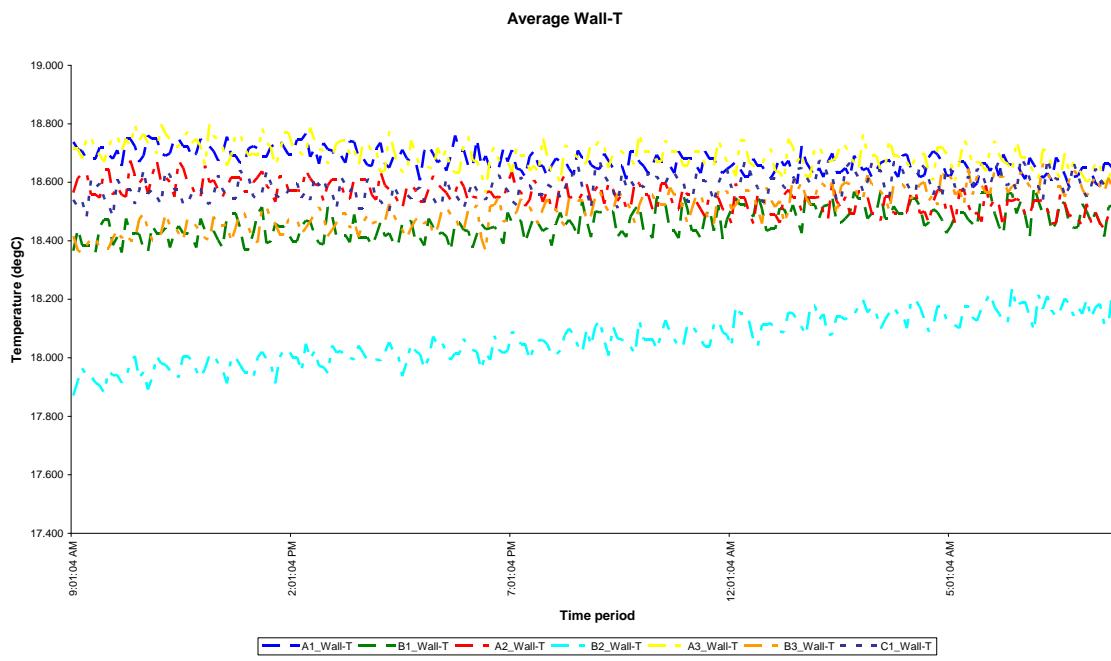


Figure B-120: Average wall temperature of C1-Alt6

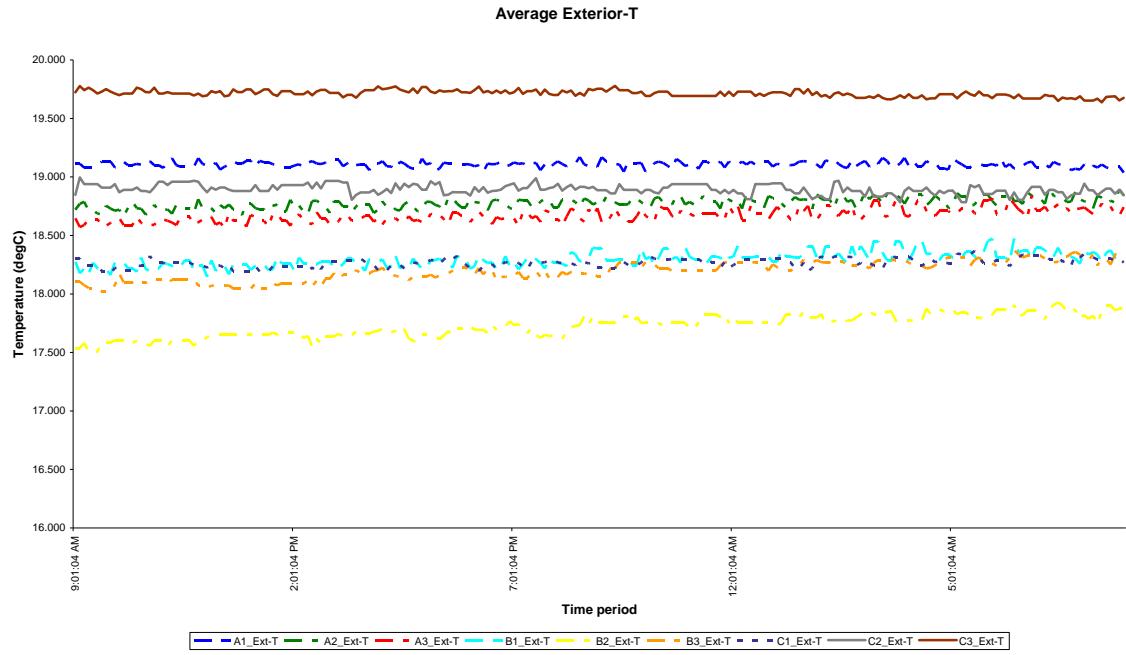


Figure B-121: Average exterior temperature of C1-Alt6

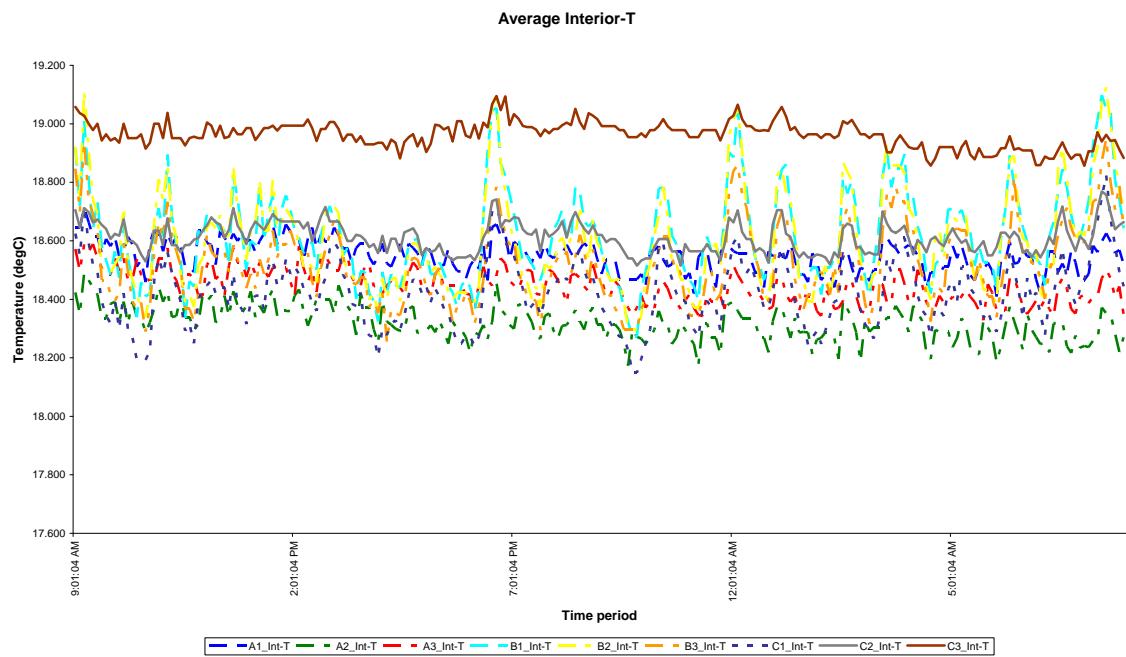


Figure B-122: Average interior temperature of C1-Alt6

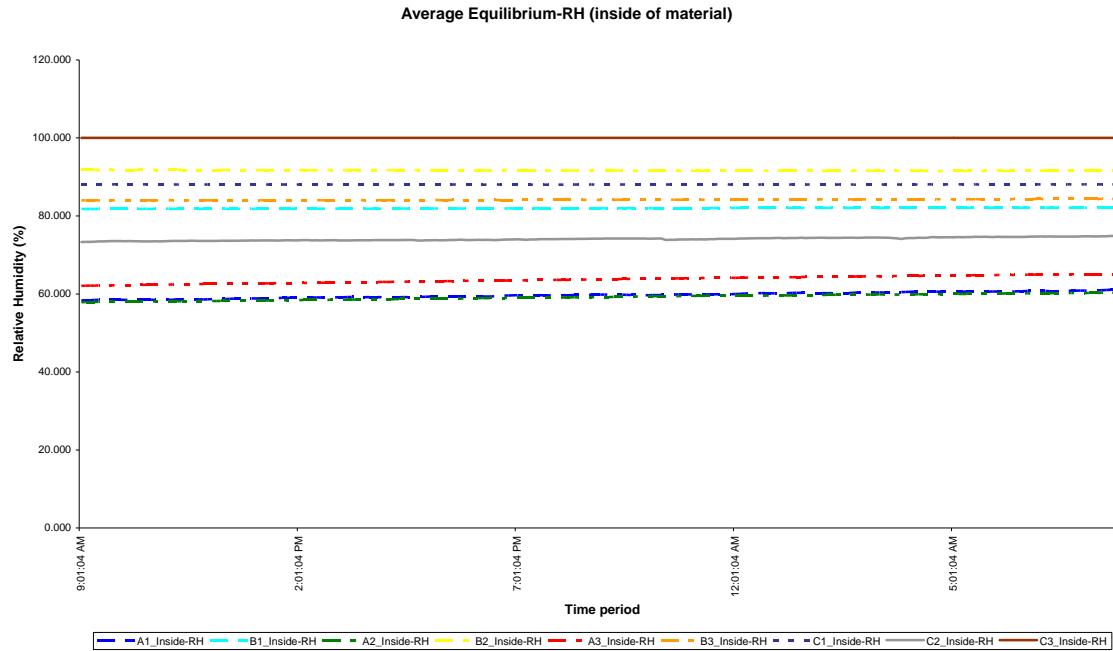


Figure B-123: Average equilibrium of relative humidity in a cavity of C1-Alt6

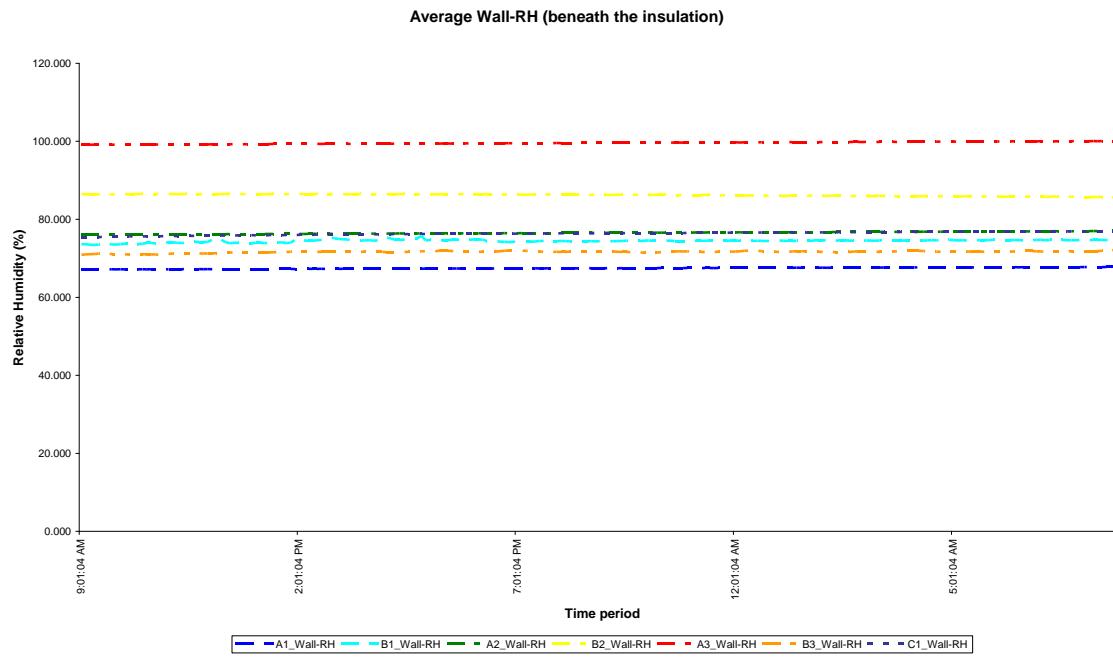


Figure B-124: Average wall relative humidity beneath the insulation of C1-Alt6

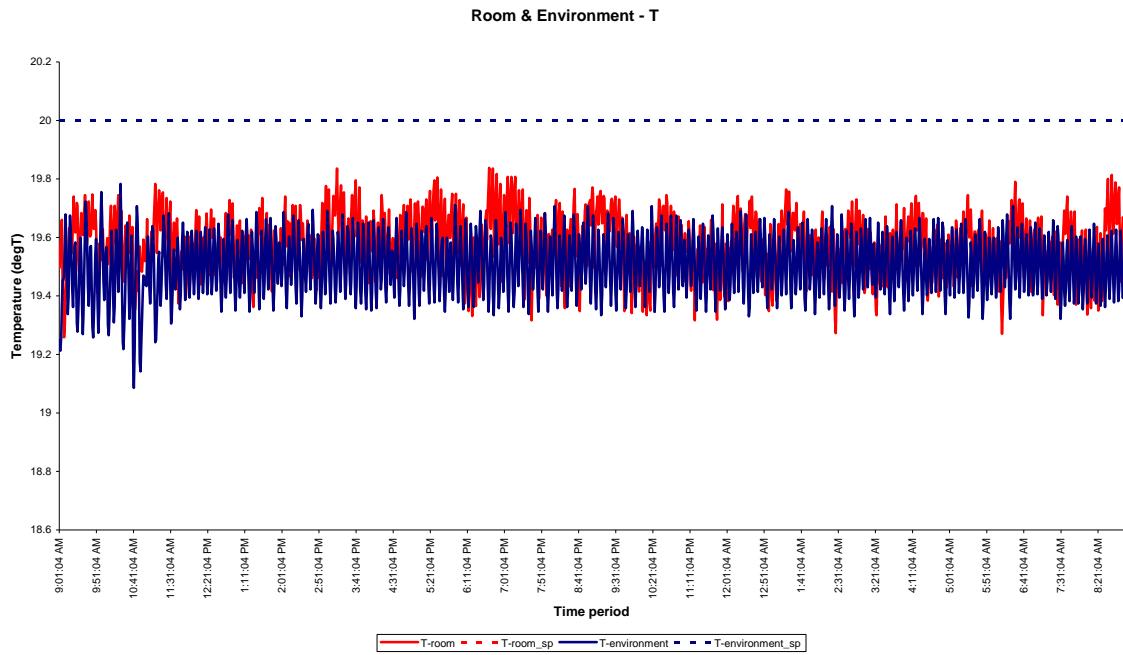


Figure B-125: Temperature of the room and environmental side during C1-Alt6

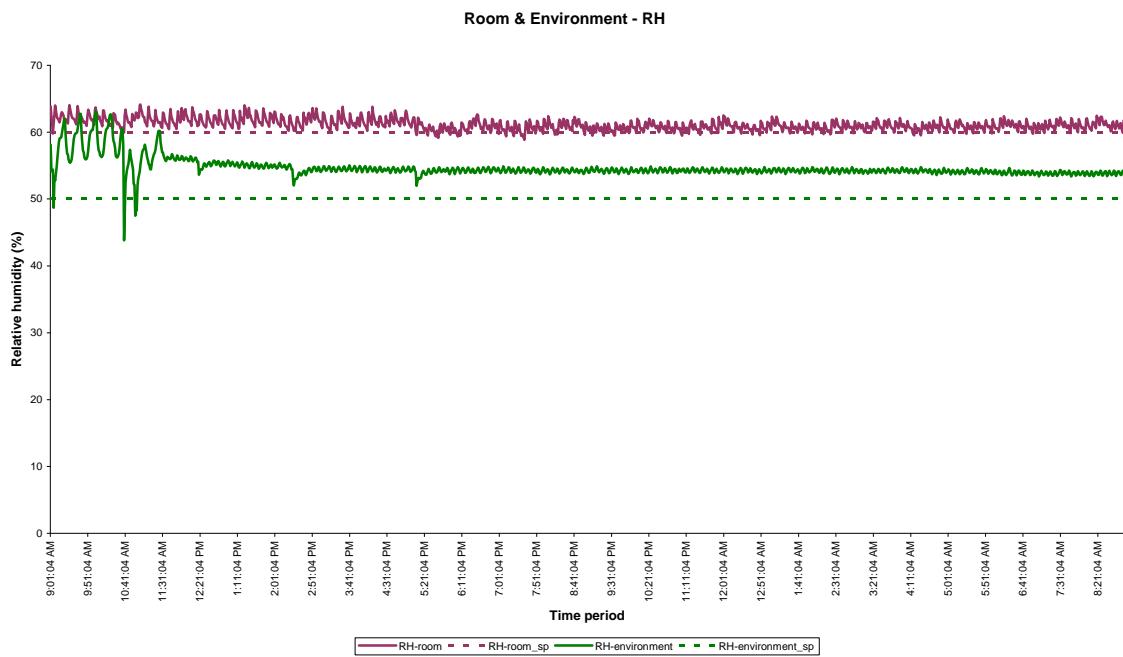


Figure B-126: Relative humidity of the room and environmental side during C1-Alt6

Test cycle: C1 – Alt7

Table B-15: Average data during the last 24 hours for each specimen of C1-Alt7

| Specimen Measurement Data | | | | | Control Loop Data | |
|---------------------------|--------------|-------------|--------------|-------------|-------------------|--------------|
| B-G | A | | B | | C | |
| 1 | A1_Soil-T | 19.312 degC | B1_Soil-T | 19.761 degC | C1_Soil-T | 19.947 degC |
| | A1_Soil-RH | 100.000 % | B1_Soil-RH | 100.000 % | C1_Soil-RH | 100.000 % |
| | A1_Wall-T | 18.462 degC | B1_Wall-T | 18.974 degC | C1_Wall-T | 19.644 degC |
| | A1_Ext-T | 19.629 degC | B1_Ext-T | 19.000 degC | C1_Ext-T | 19.474 degC |
| | A1_Int-T | 18.046 degC | B1_Int-T | 17.503 degC | C1_Int-T | 18.032 degC |
| | A1_Inside-RH | 70.444 % | B1_Inside-RH | 83.449 % | C1_Inside-RH | 88.968 % |
| 2 | A2_Soil-T | 19.442 degC | B2_Soil-T | 19.448 degC | C2_Soil-T | 20.695 degC |
| | A2_Soil-RH | 100.000 % | B2_Soil-RH | 100.000 % | C2_Soil-RH | 100.000 % |
| | A2_Wall-T | 18.051 degC | B2_Wall-T | 18.600 degC | C2_Ext-T | 19.258 degC |
| | A2_Ext-T | 19.245 degC | B2_Ext-T | 18.405 degC | C2_Int-T | 18.130 degC |
| | A2_Int-T | 17.430 degC | B2_Int-T | 17.025 degC | C2_Inside-RH | 77.265 degC |
| | A2_Inside-RH | 64.404 % | B2_Inside-RH | 91.924 % | | |
| 3 | A3_Soil-T | 19.575 degC | B3_Soil-T | 19.692 degC | C3_Soil-T | 23.452 degC |
| | A3_Soil-RH | 100.000 % | B3_Soil-RH | 100.000 % | C3_Soil-RH | 100.000 % |
| | A3_Wall-T | 18.165 degC | B3_Wall-T | 18.949 degC | C3_Ext-T | 20.057 degC |
| | A3_Ext-T | 18.997 degC | B3_Ext-T | 18.785 degC | C3_Int-T | 18.735 degC |
| | A3_Int-T | 17.528 degC | B3_Int-T | 17.463 degC | C3_Inside-RH | 100.000 degC |
| | A3_Inside-RH | 69.353 % | B3_Inside-RH | 85.393 % | | |
| No | A3_Wall-RH | 100.000 % | B3_Wall-RH | 75.340 % | | |
| | | | | | *Pressure diff. | 80.437 Pa |
| A | | B | | C | | Alt7 |

* Measured pressure difference between Room Side & Environmental Side

Remarks

Type: B-G
 Soil type: Clay
 Damproofing: No
 Alternative: Alt7

Legend

T - Temperature (degC)
 RH - Relative Humidity (%)
 SP - Setpoint (either T or RH)

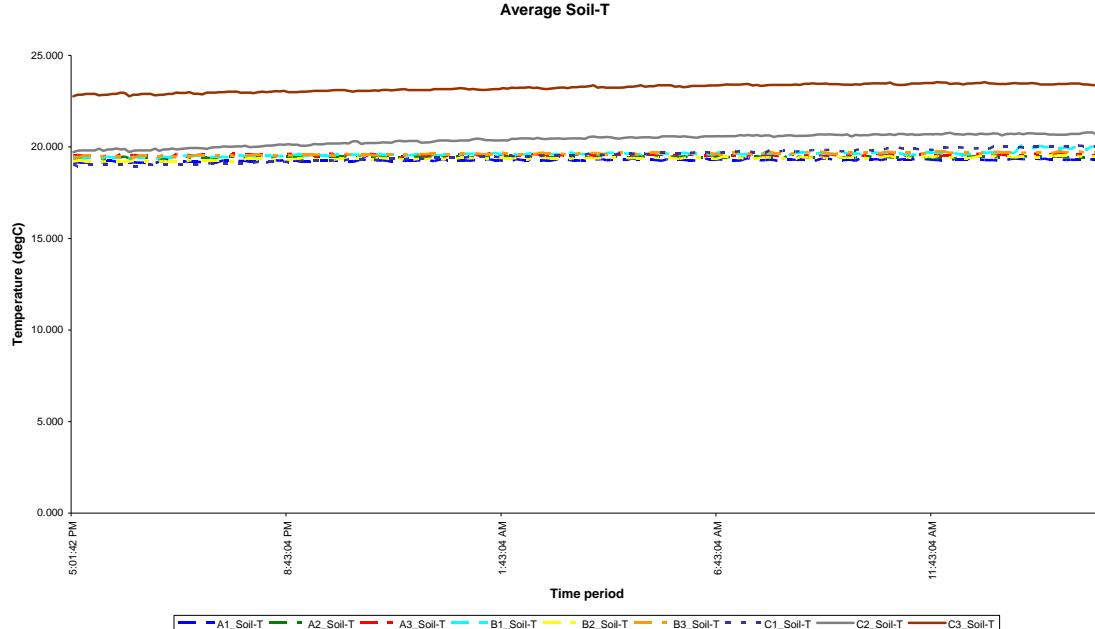


Figure B-127: Average soil temperature of C1-Alt7

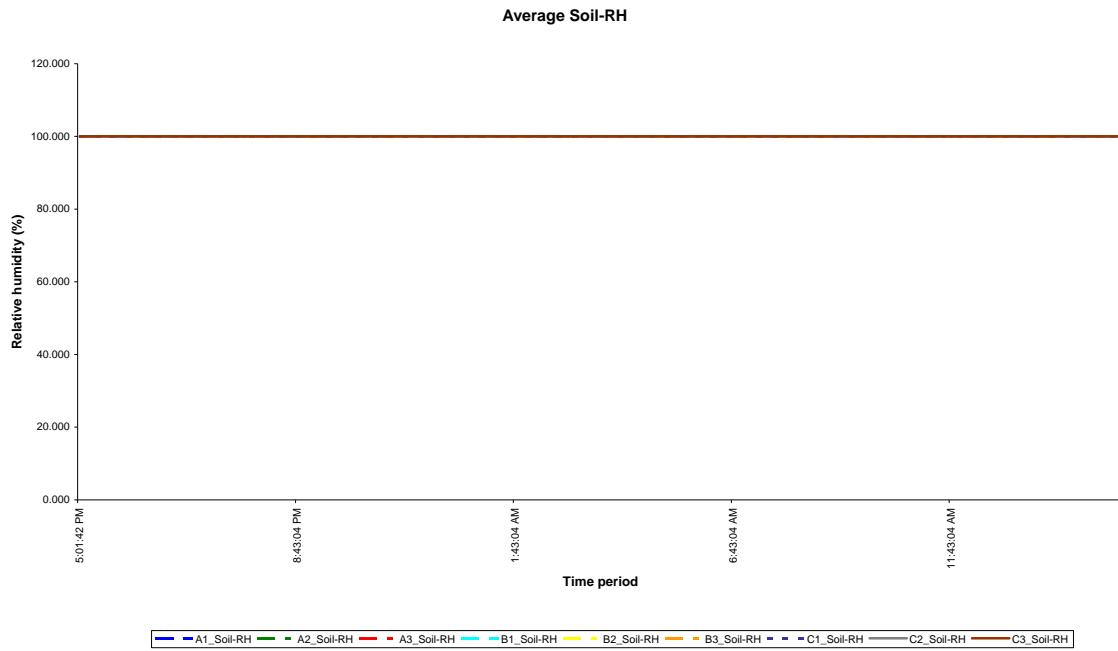


Figure B-128: Average soil relative humidity of C1-Alt7

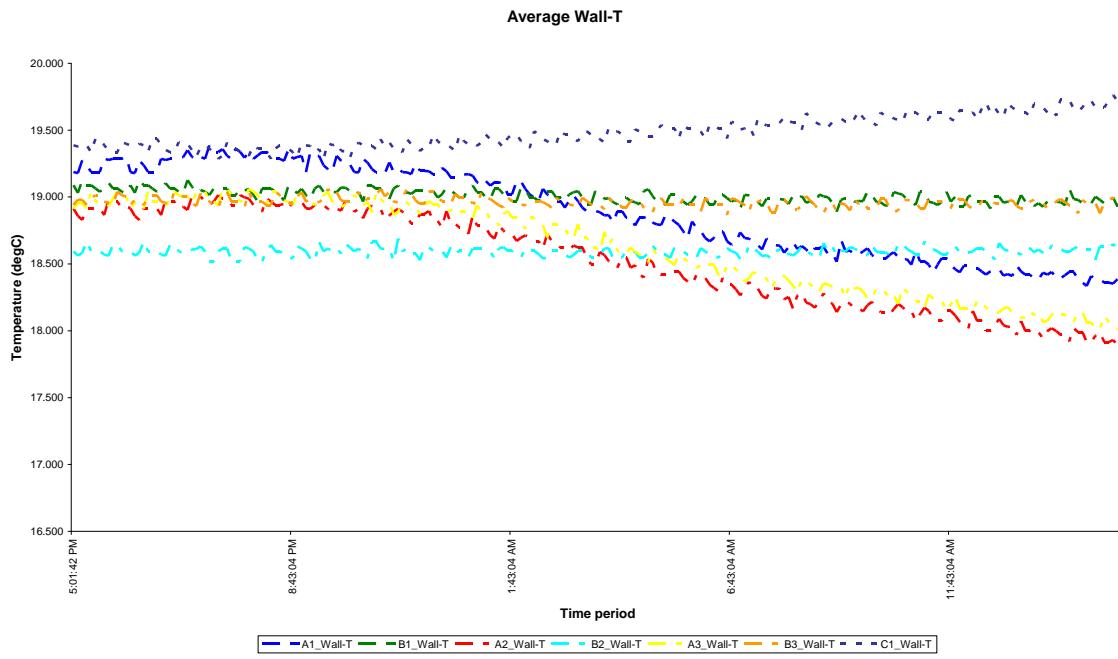


Figure B-129: Average wall temperature of C1-Alt7

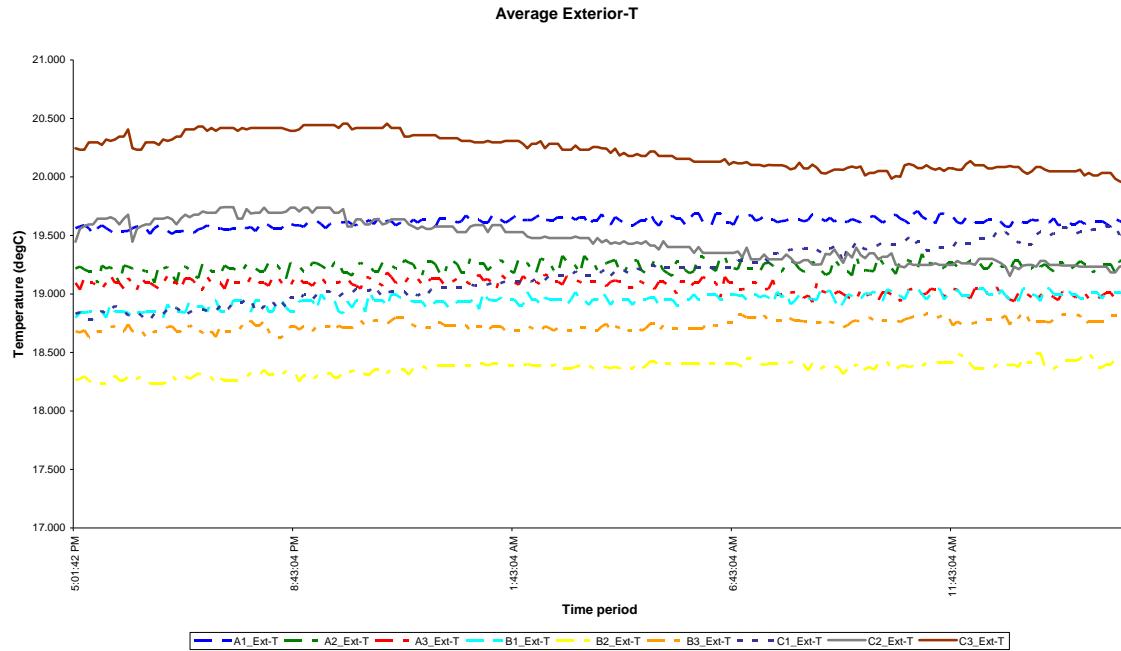


Figure B-130: Average exterior temperature of C1-Alt7

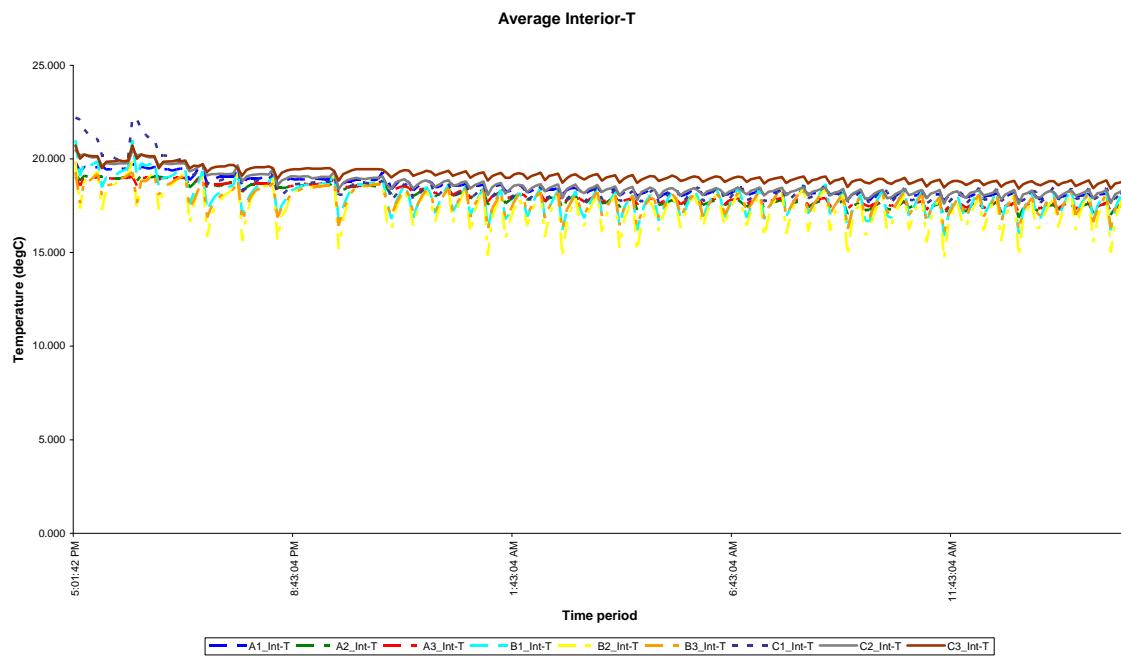


Figure B-131: Average interior temperature of C1-Alt7

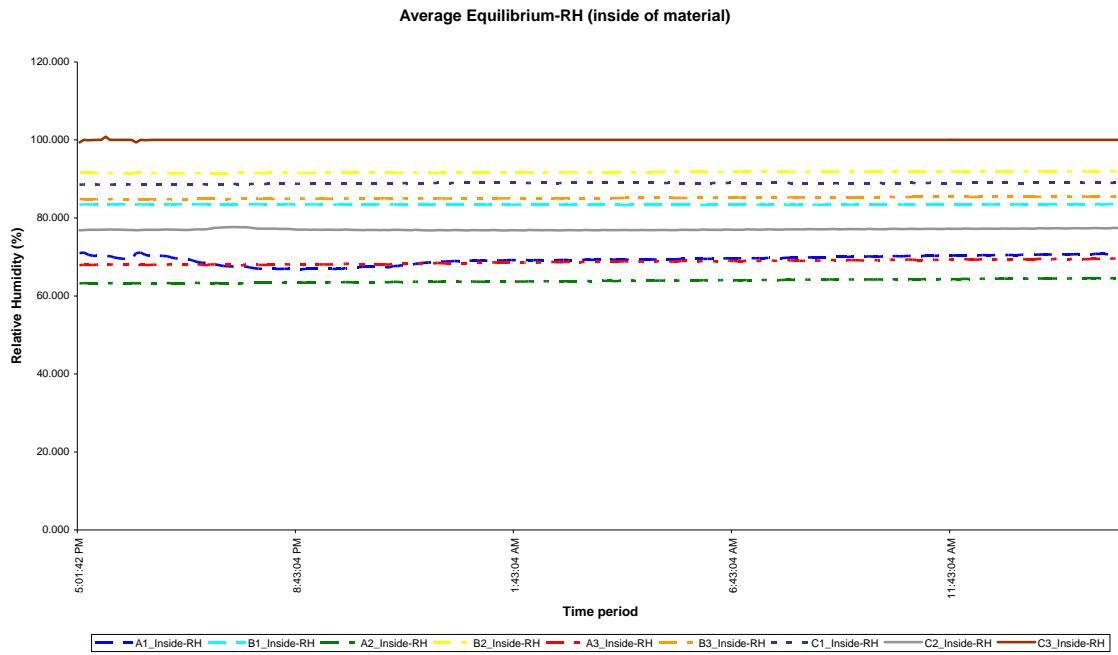


Figure B-132: Average equilibrium of relative humidity in a cavity of C1-Alt7

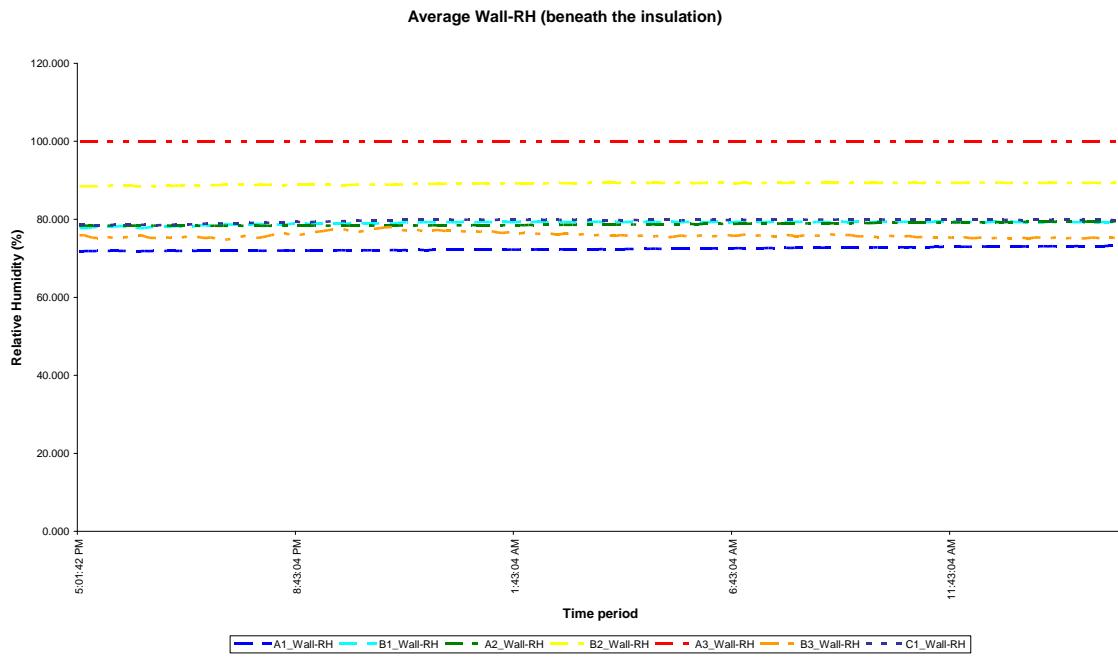


Figure B-133: Average wall relative humidity beneath the insulation of C1-Alt7

Insulated Concrete Masonry Below-grade Walls

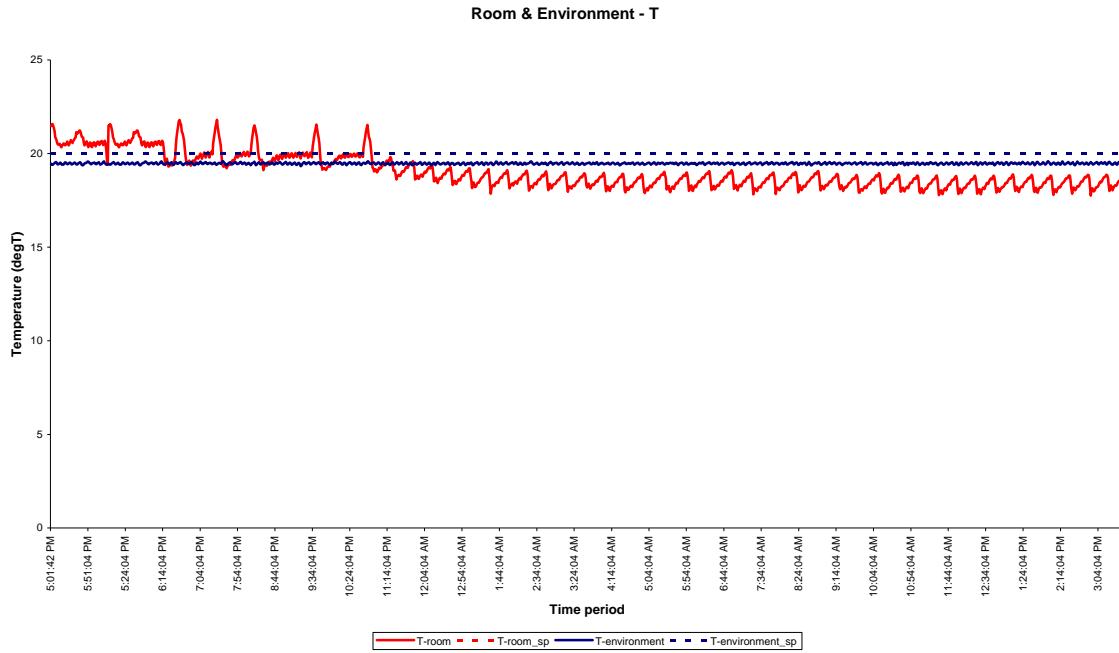


Figure B-134: Temperature of the room and environmental side during C1-Alt7

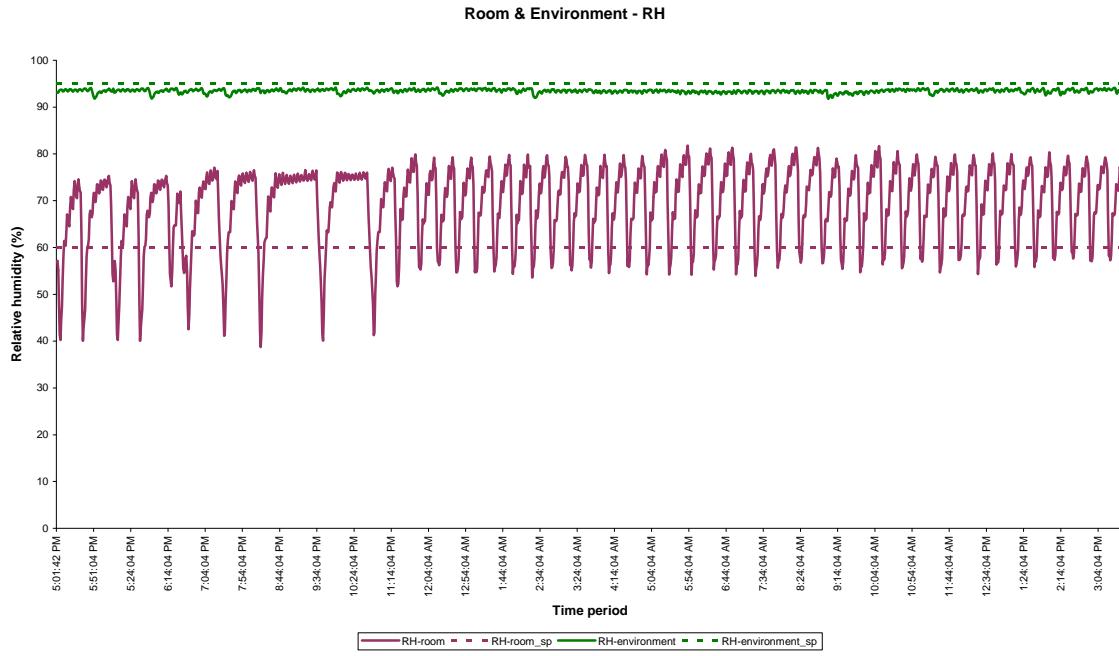


Figure B-135: Relative humidity of the room and environmental side during C1-Alt7

Test cycle: C1 – Alt8

Table B-16: Average data during the last 24 hours for each specimen of C1-Alt8

| Specimen Measurement Data | | | | | Control Loop Data | |
|---------------------------|--------------|-------------|--------------|-------------|---------------------------|--------------|
| B-G | A | | B | | C | |
| 1 | A1_Soil-T | 19.150 degC | B1_Soil-T | 19.574 degC | C1_Soil-T | 20.983 degC |
| | A1_Soil-RH | 100.000 % | B1_Soil-RH | 100.000 % | C1_Soil-RH | 100.000 % |
| | A1_Wall-T | 18.724 degC | B1_Wall-T | 19.290 degC | C1_Wall-T | 20.690 degC |
| | A1_Ext-T | 19.415 degC | B1_Ext-T | 19.252 degC | C1_Ext-T | 20.630 degC |
| | A1_Int-T | 18.604 degC | B1_Int-T | 18.684 degC | C1_Int-T | 18.783 degC |
| | A1_Inside-RH | 66.613 % | B1_Inside-RH | 85.274 % | C1_Inside-RH | 89.156 % |
| 2 | A1_Wall-RH | 76.176 % | B1_Wall-RH | 75.279 % | C1_Wall-RH | 68.122 % |
| | A2_Soil-T | 19.251 degC | B2_Soil-T | 19.544 degC | C2_Soil-T | 21.079 degC |
| | A2_Soil-RH | 100.000 % | B2_Soil-RH | 100.000 % | C2_Soil-RH | 100.000 % |
| | A2_Wall-T | 18.460 degC | B2_Wall-T | 19.206 degC | C2_Ext-T | 19.784 degC |
| | A2_Ext-T | 19.143 degC | B2_Ext-T | 18.963 degC | C2_Int-T | 18.930 degC |
| | A2_Int-T | 18.269 degC | B2_Int-T | 18.754 degC | C2_Inside-RH | 76.246 degC |
| 3 | A2_Inside-RH | 62.424 % | B2_Inside-RH | 91.825 % | C2_Wall-RH | 86.865 % |
| | A2_Wall-RH | 80.730 % | B2_Wall-RH | 86.865 % | C3_Soil-T | 23.711 degC |
| | A3_Soil-T | 19.408 degC | B3_Soil-T | 19.723 degC | C3_Soil-RH | 100.000 % |
| | A3_Soil-RH | 100.000 % | B3_Soil-RH | 100.000 % | C3_Ext-T | 20.445 degC |
| | A3_Wall-T | 18.575 degC | B3_Wall-T | 19.074 degC | C3_Int-T | 19.192 degC |
| | A3_Ext-T | 18.972 degC | B3_Ext-T | 18.867 degC | C3_Inside-RH | 100.000 degC |
| No | A3_Int-T | 18.297 degC | B3_Int-T | 18.475 degC | *Pressure diff. 15.696 Pa | |
| | A3_Inside-RH | 67.374 % | B3_Inside-RH | 82.745 % | | |
| | A3_Wall-RH | 100.000 % | B3_Wall-RH | 44.971 % | | |
| | A | | B | | C | |
| | | | | | Alt8 | |

* Measured pressure difference between Room Side & Environmental Side

| Environmental / Room Side | |
|---------------------------|-------------|
| T-room | 19.432 degC |
| RH-room | 32.782 % |
| T-room_sp | 20.000 degC |
| RH-room_sp | 30.000 % |
| T-environment | 19.464 degC |
| RH-environment | 91.533 % |
| T-environment_sp | 20.000 degC |
| RH-environment_sp | 95.000 % |

| Remarks | |
|--------------|------|
| Type: | B-G |
| Soil type: | Clay |
| Damproofing: | No |
| Alternative: | Alt8 |

| Legend | |
|--------------------------------|--|
| T - Temperature (degC) | |
| RH - Relative Humidity (%) | |
| SP - Setpoint (either T or RH) | |

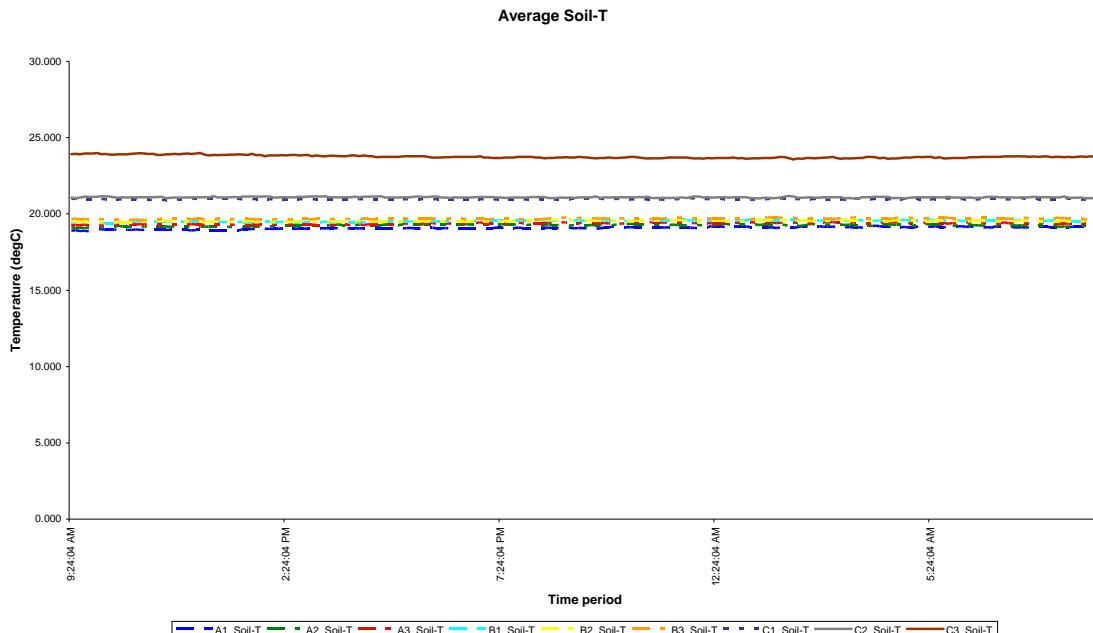


Figure B-136: Average soil temperature of C1-Alt8

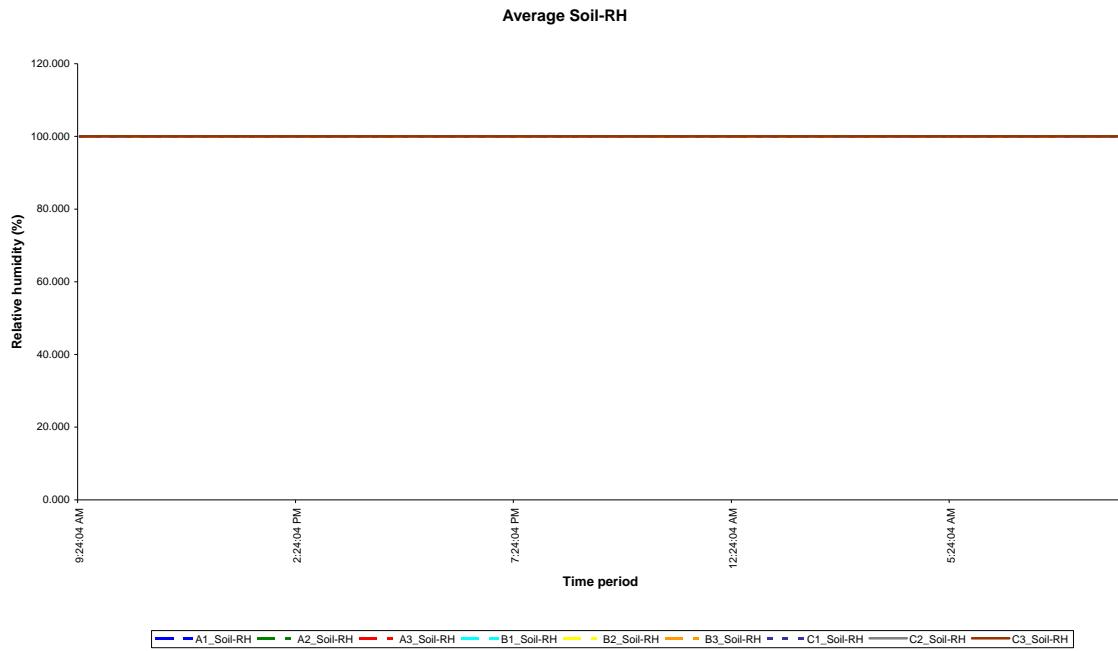


Figure B-137: Average soil relative humidity of C1-Alt8

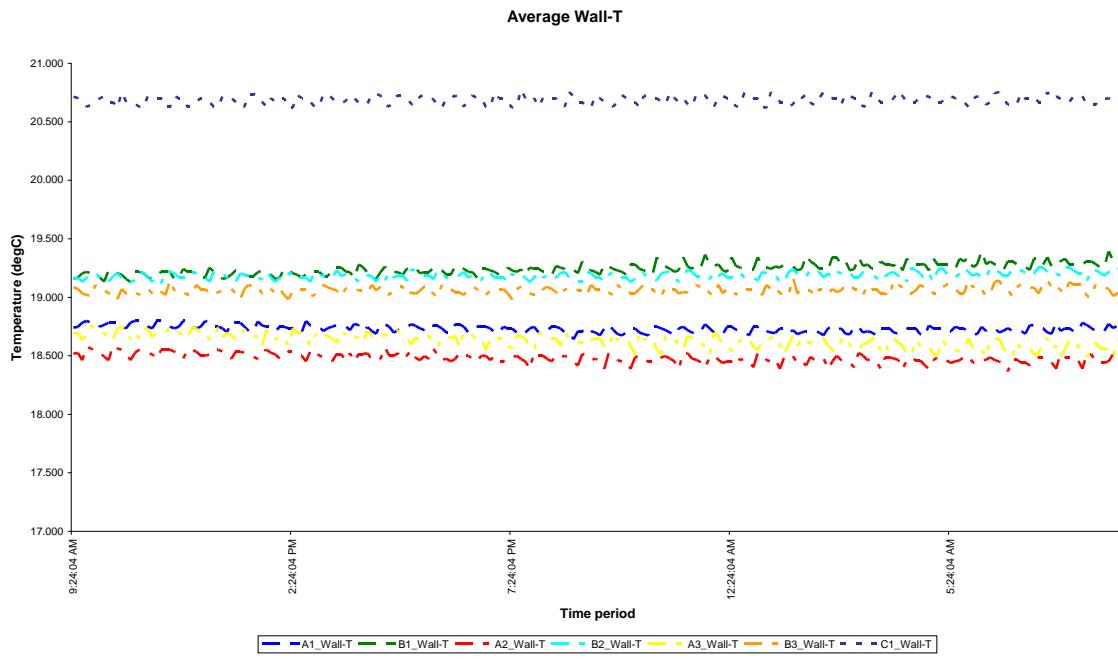


Figure B-138: Average wall temperature of C1-Alt8

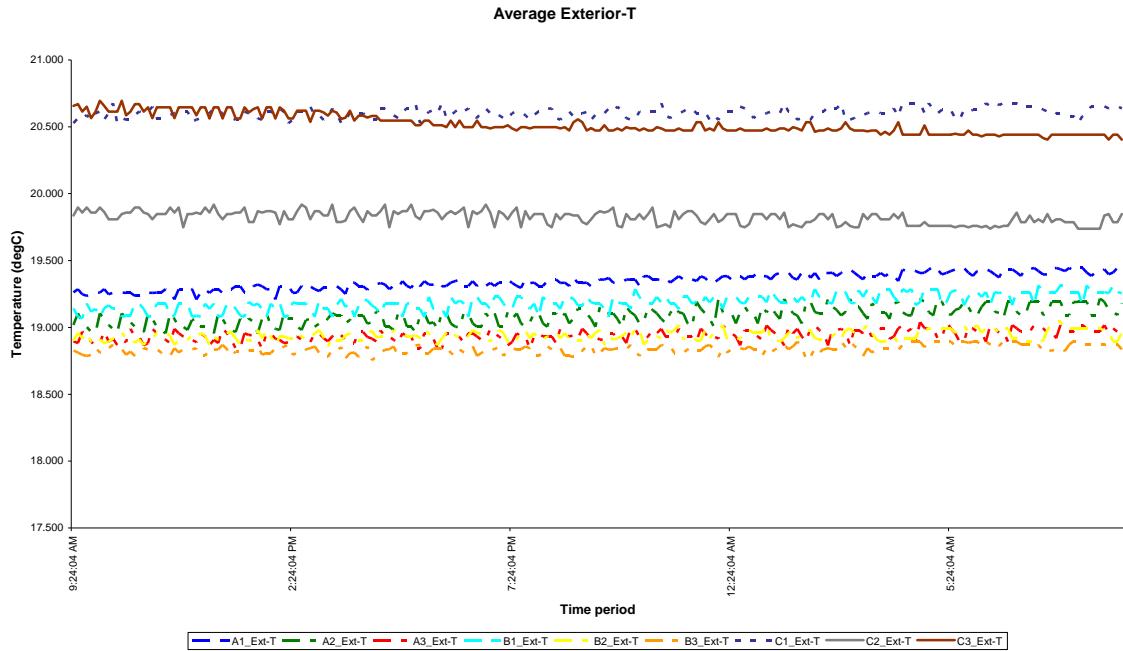


Figure B-139: Average exterior temperature of C1-Alt8

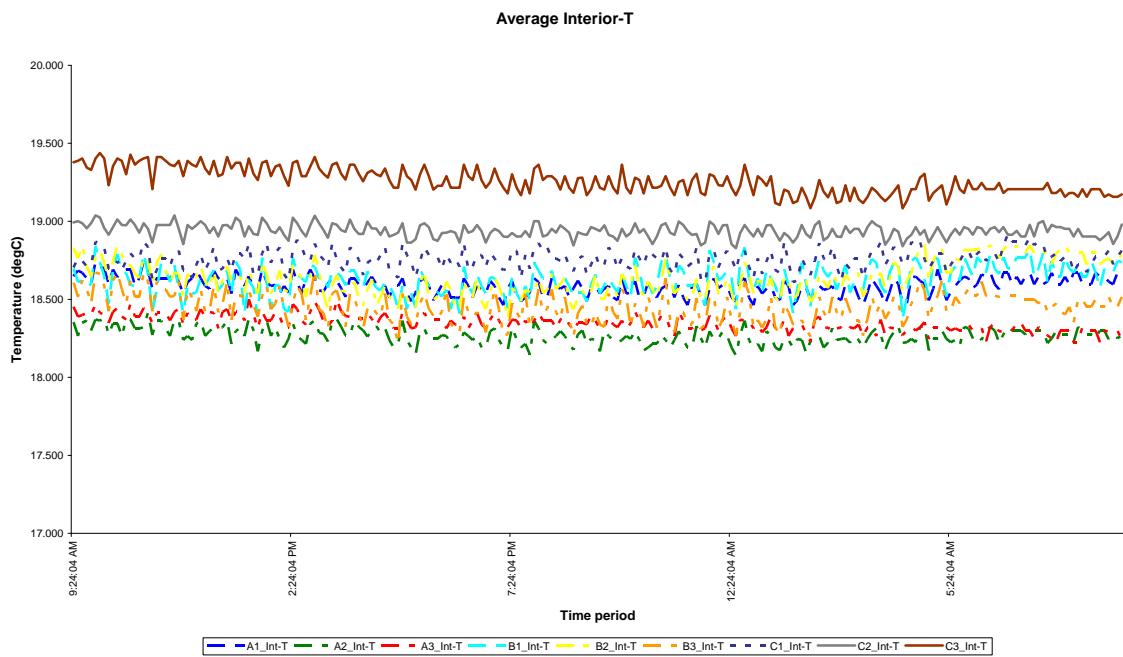


Figure B-140: Average interior temperature of C1-Alt8

Insulated Concrete Masonry Below-grade Walls

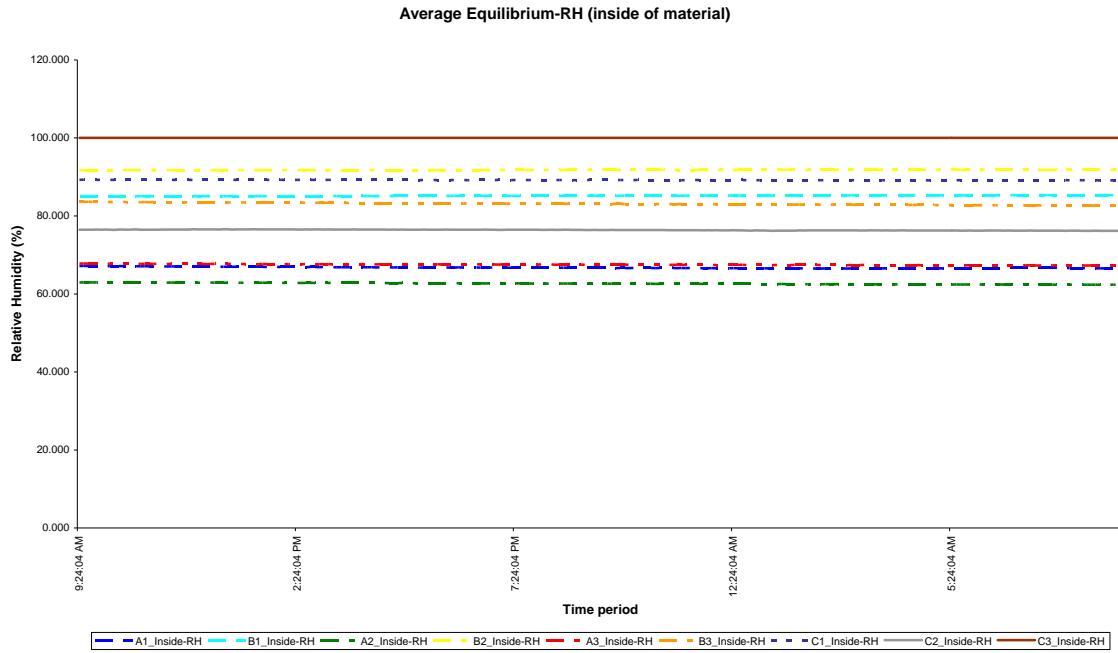


Figure B-141: Average equilibrium of relative humidity in a cavity of C1-Alt8

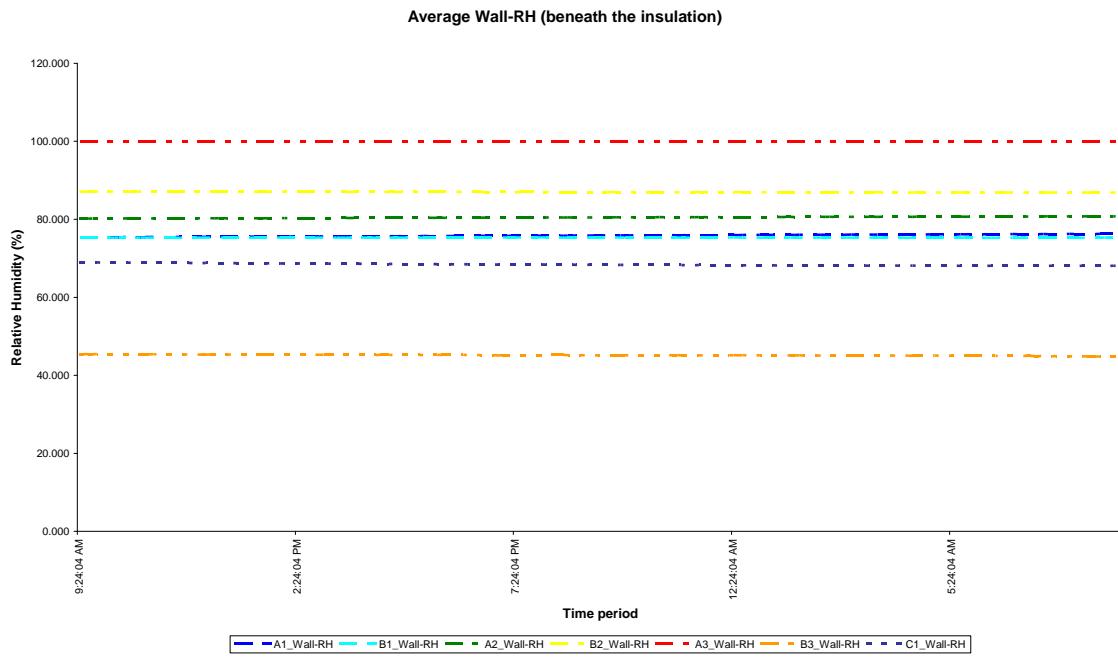


Figure B-142: Average wall relative humidity beneath the insulation of C1-Alt8

Insulated Concrete Masonry Below-grade Walls

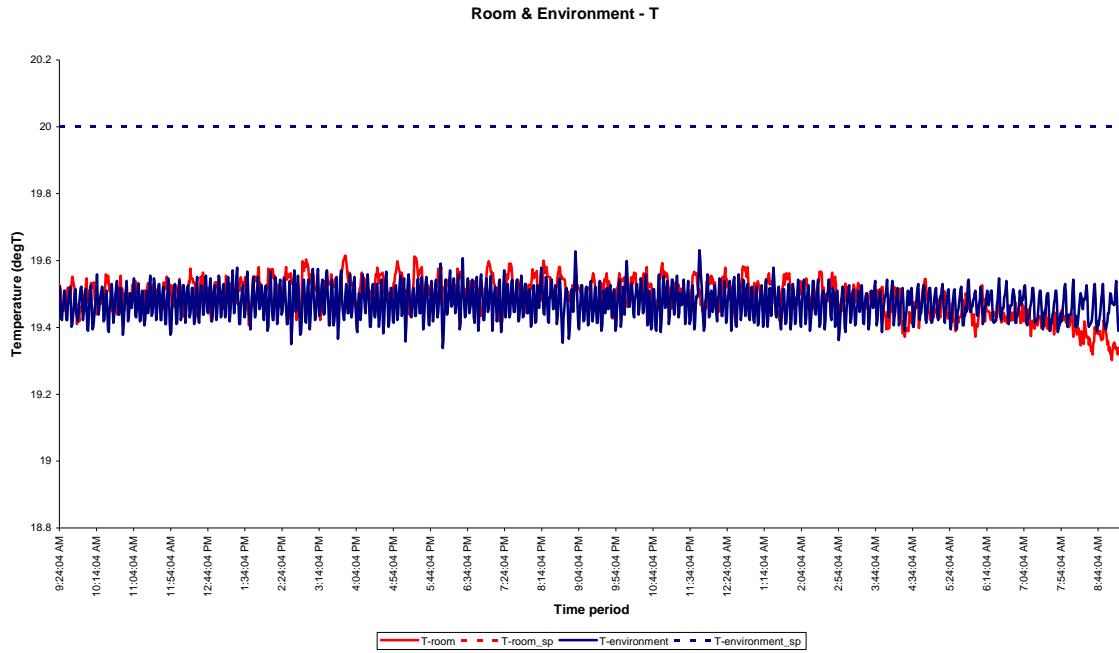


Figure B-143: Temperature of the room and environmental side during C1-Alt8

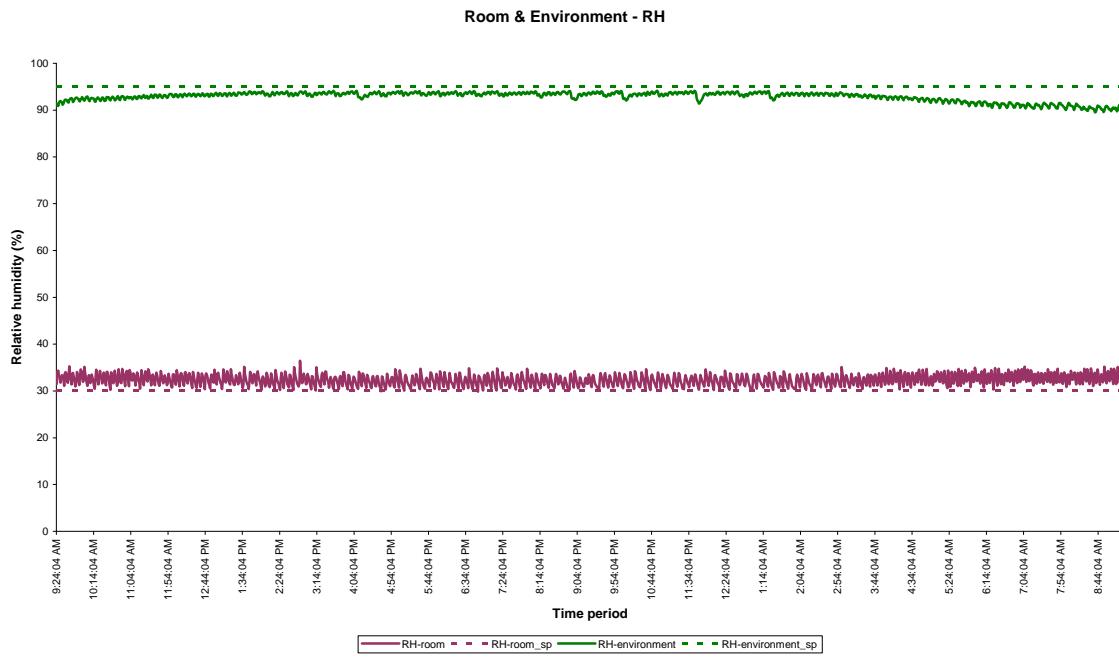


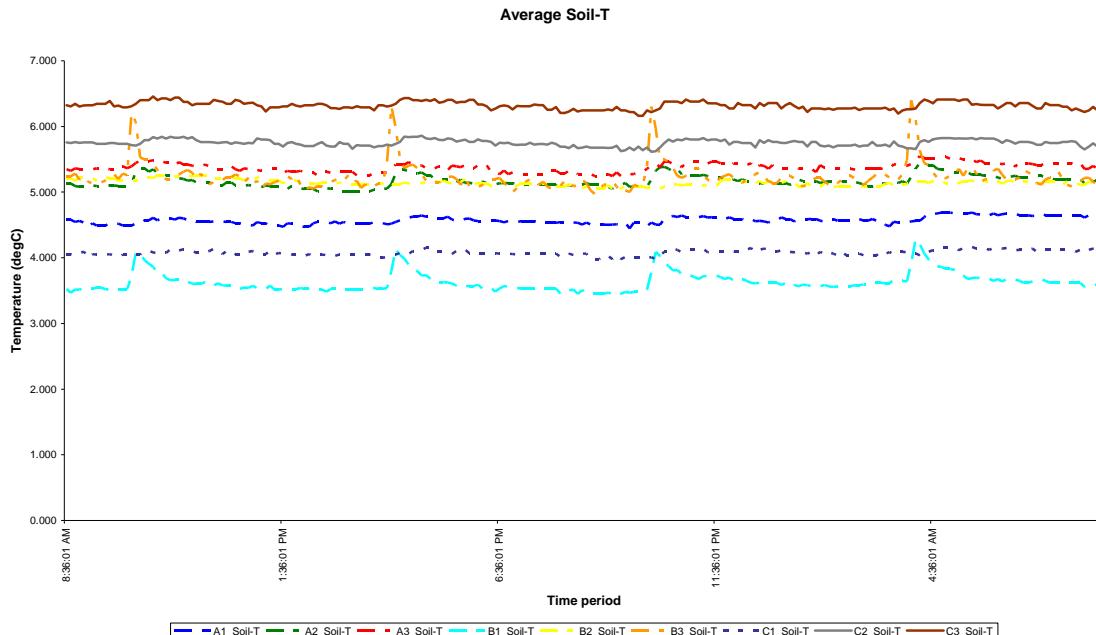
Figure B-144: Relative humidity of the room and environmental side during C1-Alt8

Measurement series: **S2 (Sand; with dampproofing)**

 Test cycle: **S2 – Alt1**
Table B-17: Average data during the last 24 hours for each specimen of S2-Alt1

| Specimen Measurement Data | | | | | Control Loop Data | |
|---------------------------|--|---|---|------|--|---|
| B-G | A | B | C | Sand | Environmental / Room Side | Remarks |
| 1 | A1_Soil-T 4.624 degC A1_Soil-RH 100.000 % A1_Wall-T 14.698 degC A1_Ext-T 5.780 degC A1_Int-T 17.245 degC A1_Inside-RH 49.556 % A1_Wall-RH 48.712 % | B1_Soil-T 3.692 degC B1_Soil-RH 100.000 % B1_Wall-T 5.918 degC B1_Ext-T 4.838 degC B1_Int-T 16.395 degC B1_Inside-RH 79.851 % B1_Wall-RH 72.559 % | C1_Soil-T 4.107 degC C1_Soil-RH 100.000 % C1_Wall-T 6.578 degC C1_Ext-T 4.597 degC C1_Int-T 17.452 degC C1_Inside-RH 81.054 % C1_Wall-RH 71.804 % | 1 | T-room 19.569 degC RH-room 28.890 % T-room_sp 20.000 degC RH-room_sp 30.000 % T-environment 3.786 degC RH-environment 79.528 % T-environment_sp 3.000 degC RH-environment_sp 90.000 % | Type: B-G Soil type: Sand Damproofing: Yes Alternative: Alt1 |
| 2 | A2_Soil-T 5.224 degC A2_Soil-RH 100.000 % A2_Wall-T 16.008 degC A2_Ext-T 6.793 degC A2_Int-T 17.021 degC A2_Inside-RH 51.112 % A2_Wall-RH 58.570 % | B2_Soil-T 5.138 degC B2_Soil-RH 100.000 % B2_Wall-T 7.507 degC B2_Ext-T 6.200 degC B2_Int-T 17.064 degC B2_Inside-RH 90.170 % B2_Wall-RH 85.226 % | C2_Soil-T 5.752 degC C2_Soil-RH 100.000 % C2_Ext-T 10.184 degC C2_Int-T 14.817 degC C2_Inside-RH 66.834 % | 2 | | |
| 3 | A3_Soil-T 5.430 degC A3_Soil-RH 100.000 % A3_Wall-T 15.814 degC A3_Ext-T 6.656 degC A3_Int-T 16.919 degC A3_Inside-RH 53.073 % A3_Wall-RH 66.430 % | B3_Soil-T 5.274 degC B3_Soil-RH 100.000 % B3_Wall-T 8.145 degC B3_Ext-T 6.514 degC B3_Int-T 17.020 degC B3_Inside-RH 81.294 % B3_Wall-RH 68.379 % | C3_Soil-T 6.312 degC C3_Soil-RH 100.000 % C3_Ext-T 11.391 degC C3_Int-T 13.764 degC C3_Inside-RH 98.173 % | 3 | | |
| Yes | A | B | C | Alt1 | | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-145: Average soil temperature of S2-Alt1

Insulated Concrete Masonry Below-grade Walls

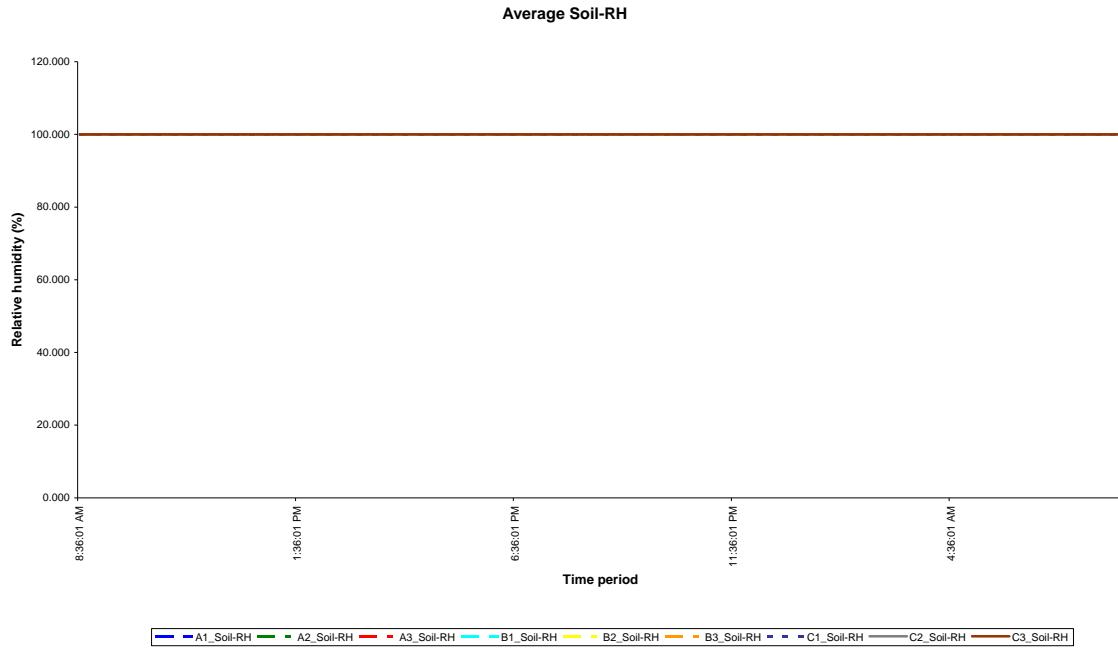


Figure B-146: Average soil relative humidity of S2-Alt1

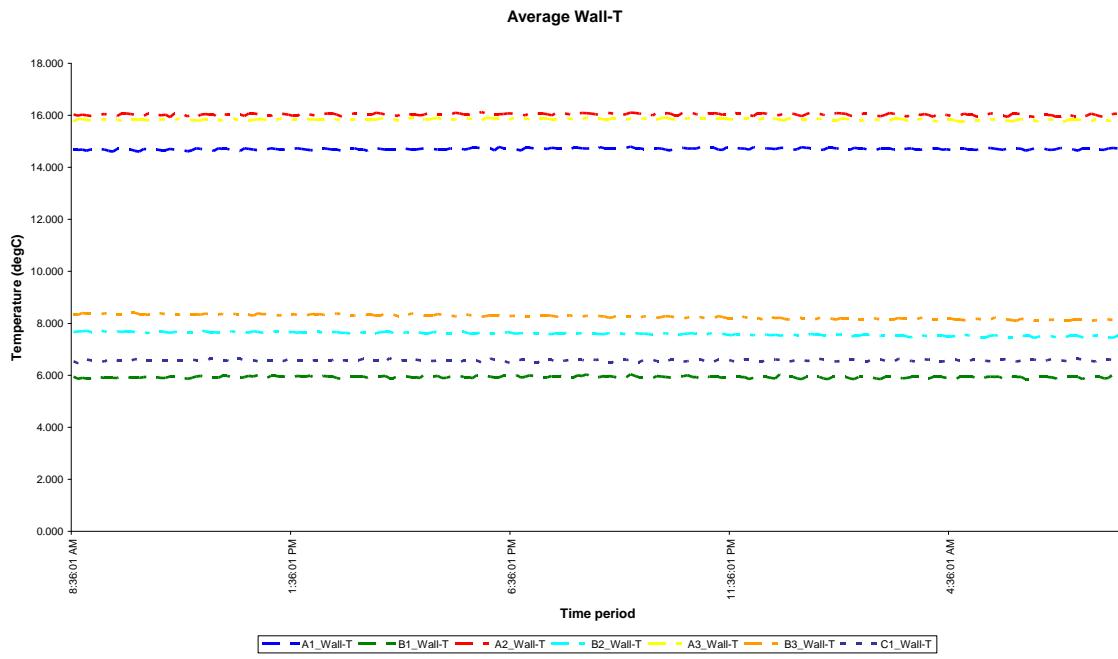


Figure B-147: Average wall temperature of S2-Alt1

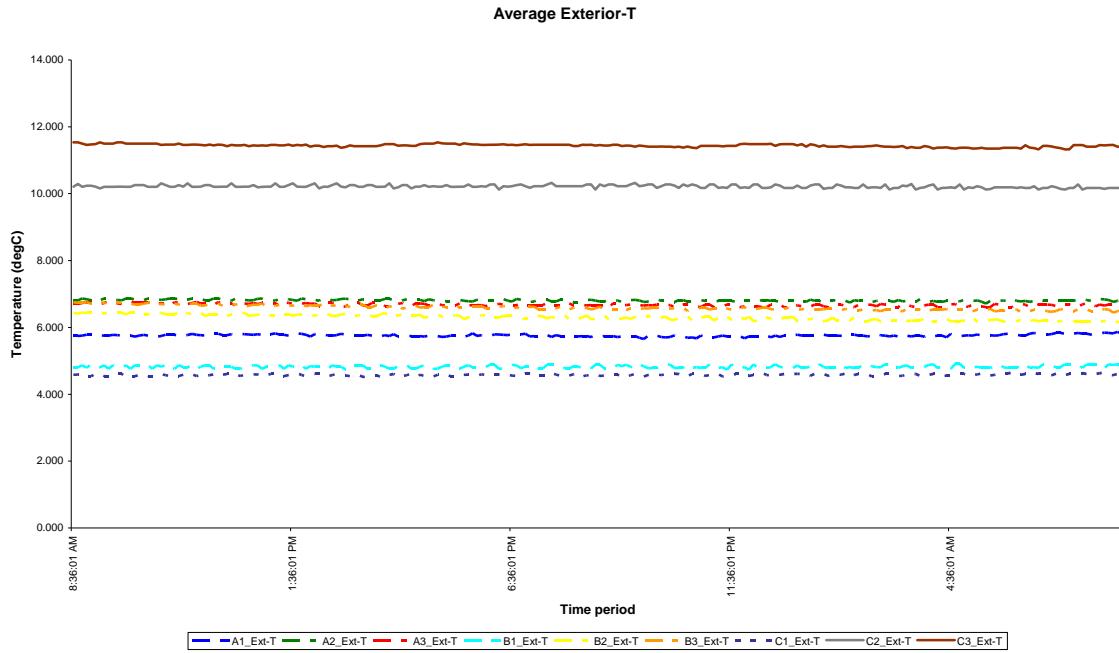


Figure B-148: Average exterior temperature of S2-Alt1

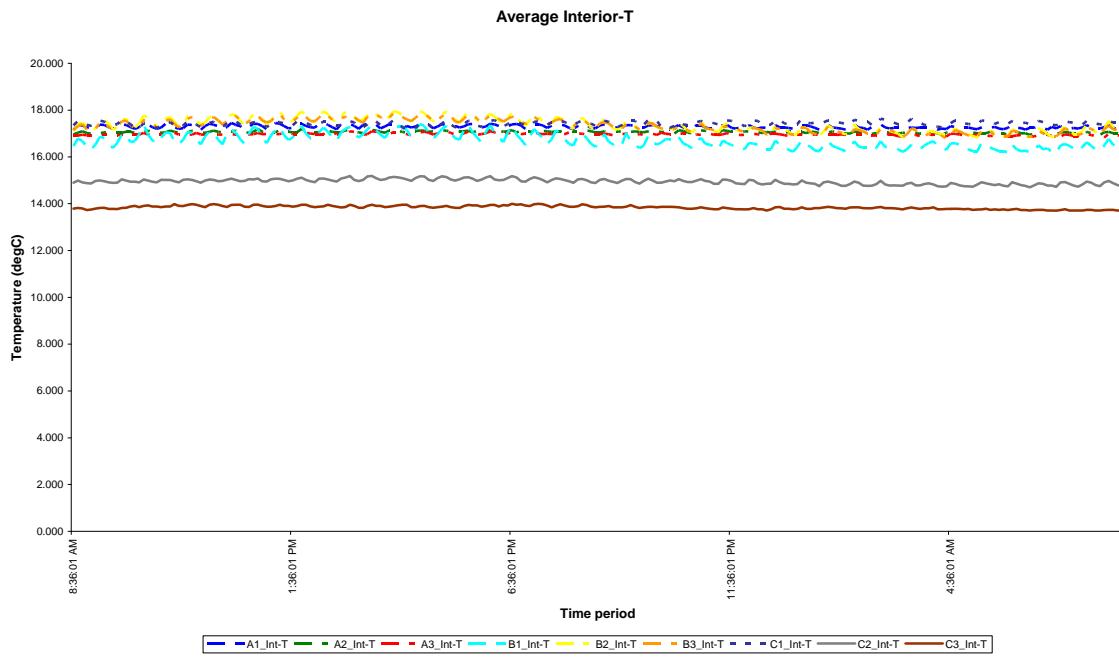


Figure B-149: Average interior temperature of S2-Alt1

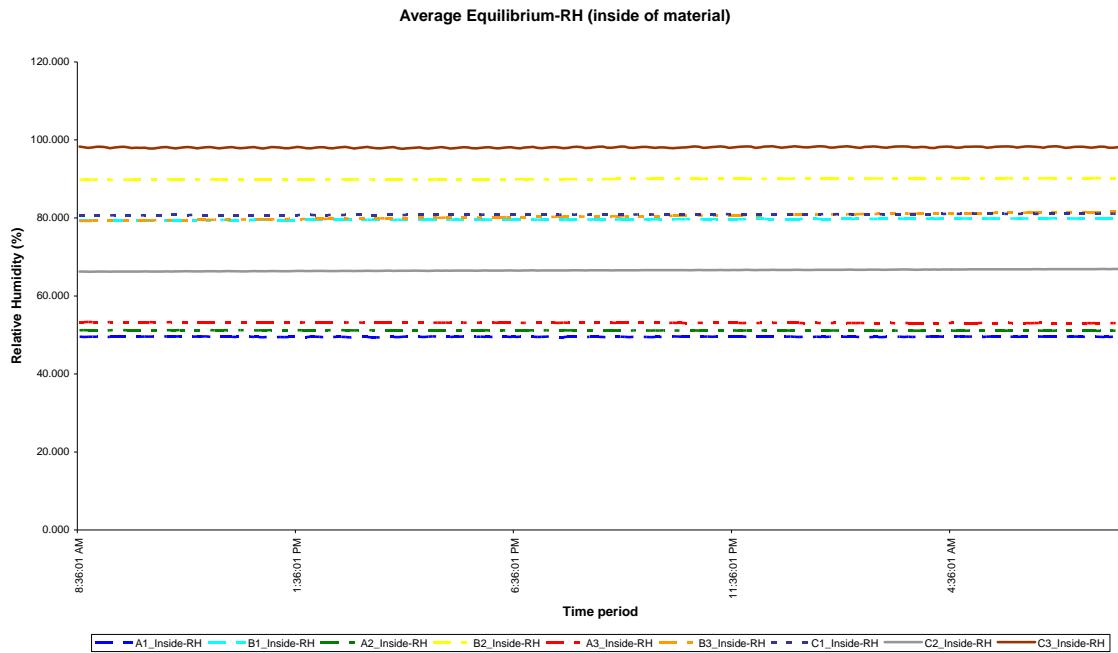


Figure B-150: Average equilibrium of relative humidity in a cavity of S2-Alt1

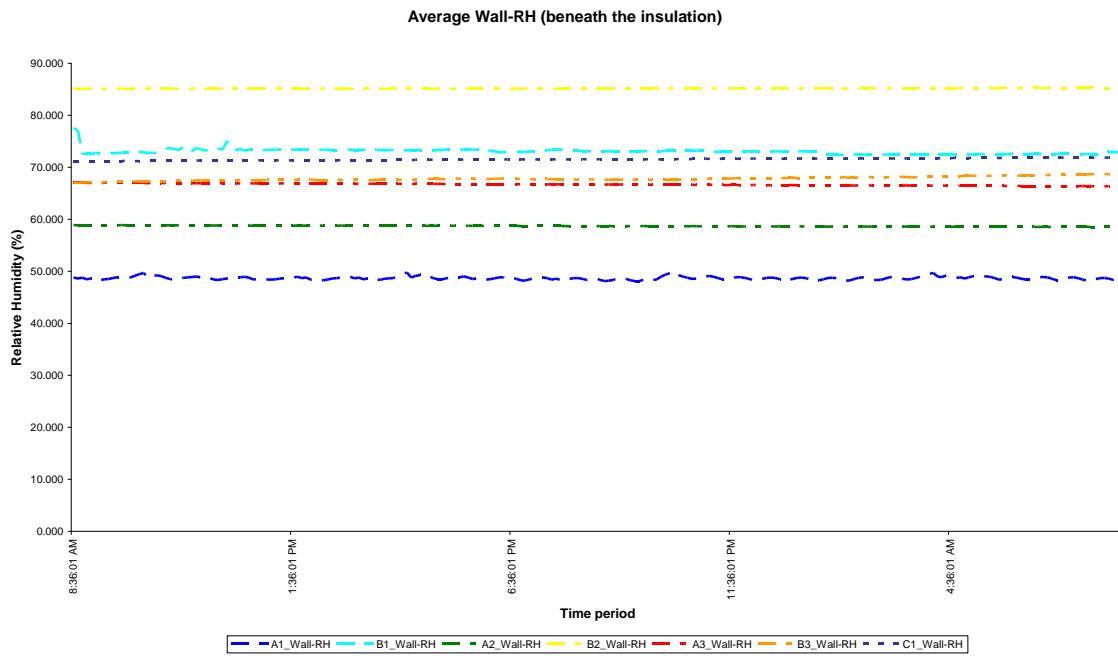


Figure B-151: Average wall relative humidity beneath the insulation of S2-Alt1

Insulated Concrete Masonry Below-grade Walls

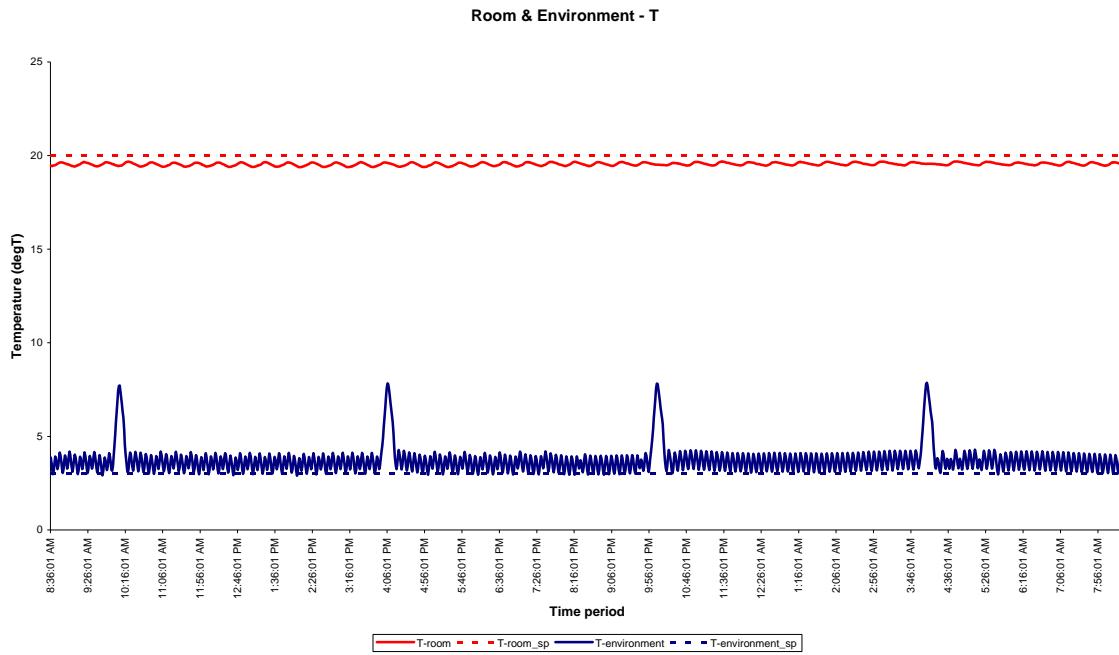


Figure B-152: Temperature of the room and environmental side during S2-Alt1

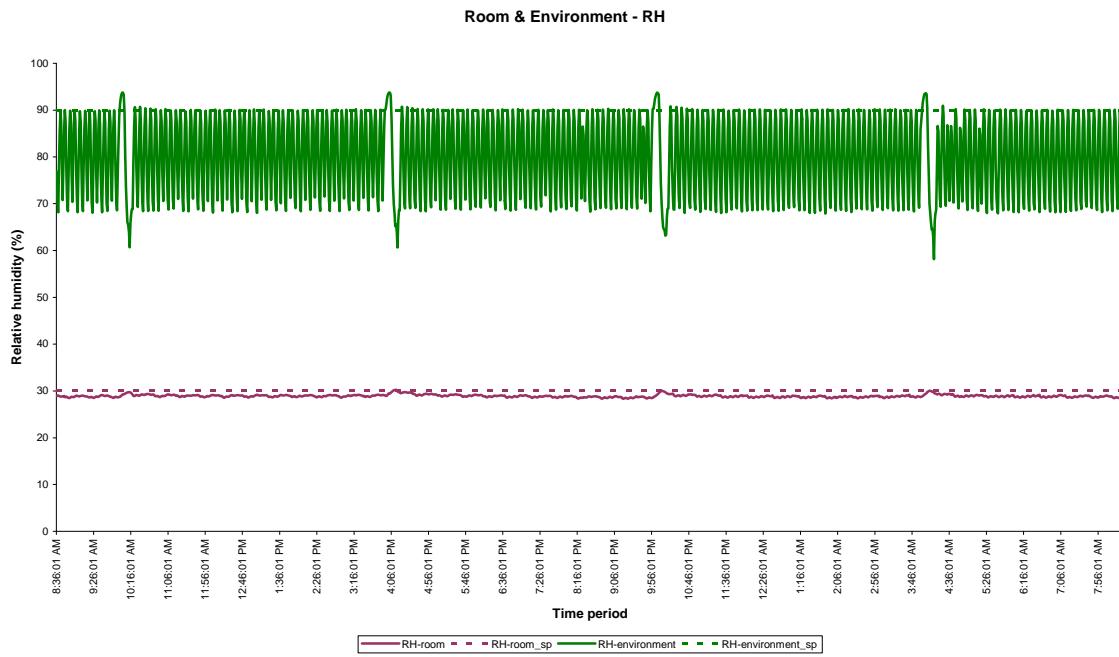


Figure B-153: Relative humidity of the room and environmental side during S2-Alt1

Test cycle: S2 – Alt2

Table B-18: Average data during the last 24 hours for each specimen of S2-Alt2

| Specimen Measurement Data | | | | | Control Loop Data | |
|---------------------------|--|--|---|------|--|--|
| B-G | A | B | C | Sand | Environmental / Room Side | Remarks |
| 1 | A1_Soil-T 4.765 degC A1_Soil-RH 100.000 % A1_Wall-T 14.741 degC A1_Ext-T 5.950 degC A1_Int-T 17.220 degC A1_Inside-RH 66.580 % A1_Wall-RH 50.208 % | B1_Soil-T 3.832 degC B1_Soil-RH 100.000 % B1_Wall-T 6.202 degC B1_Ext-T 5.010 degC B1_Int-T 17.327 degC B1_Inside-RH 83.023 % B1_Wall-RH 79.084 % | C1_Soil-T 4.267 degC C1_Soil-RH 100.000 % C1_Wall-T 6.819 degC C1_Ext-T 4.799 degC C1_Int-T 17.703 degC C1_Inside-RH 86.288 % C1_Wall-RH 90.991 % | 1 | T-room 19.510 degC RH-room 59.191 % T-room_sp 20.000 degC RH-room_sp 60.000 % T-environment 3.798 degC RH-environment 80.614 % T-environment_sp 3.000 degC RH-environment_sp 90.000 % | Type: B-G Soil type: Sand Damp proofing: Yes Alternative: Alt2 |
| 2 | A2_Soil-T 5.280 degC A2_Soil-RH 100.000 % A2_Wall-T 16.202 degC A2_Ext-T 6.883 degC A2_Int-T 17.225 degC A2_Inside-RH 61.167 % A2_Wall-RH 61.282 % | B2_Soil-T 5.092 degC B2_Soil-RH 100.000 % B2_Wall-T 7.484 degC B2_Ext-T 6.118 degC B2_Int-T 17.804 degC B2_Inside-RH 92.068 % B2_Wall-RH 91.457 % | C2_Soil-T 5.731 degC C2_Soil-RH 100.000 % C2_Ext-T 10.110 degC C2_Int-T 15.235 degC C2_Inside-RH 77.877 % | 2 | | |
| 3 | A3_Soil-T 5.498 degC A3_Soil-RH 100.000 % A3_Wall-T 16.148 degC A3_Ext-T 6.721 degC A3_Int-T 17.301 degC A3_Inside-RH 63.457 % A3_Wall-RH 74.187 % | B3_Soil-T 5.088 degC B3_Soil-RH 100.000 % B3_Wall-T 8.106 degC B3_Ext-T 6.279 degC B3_Int-T 17.755 degC B3_Inside-RH 93.317 % B3_Wall-RH 100.000 % | C3_Soil-T 6.094 degC C3_Soil-RH 100.000 % C3_Ext-T 11.273 degC C3_Int-T 13.990 degC C3_Inside-RH 98.150 % | 3 | | |
| Yes | A | B | C | | | Legend |
| | | | | Alt2 | | T - Temperature (degC) RH - Relative Humidity (%) SP - Setpoint (either T or RH) |

* Measured pressure difference between Room Side & Environmental Side

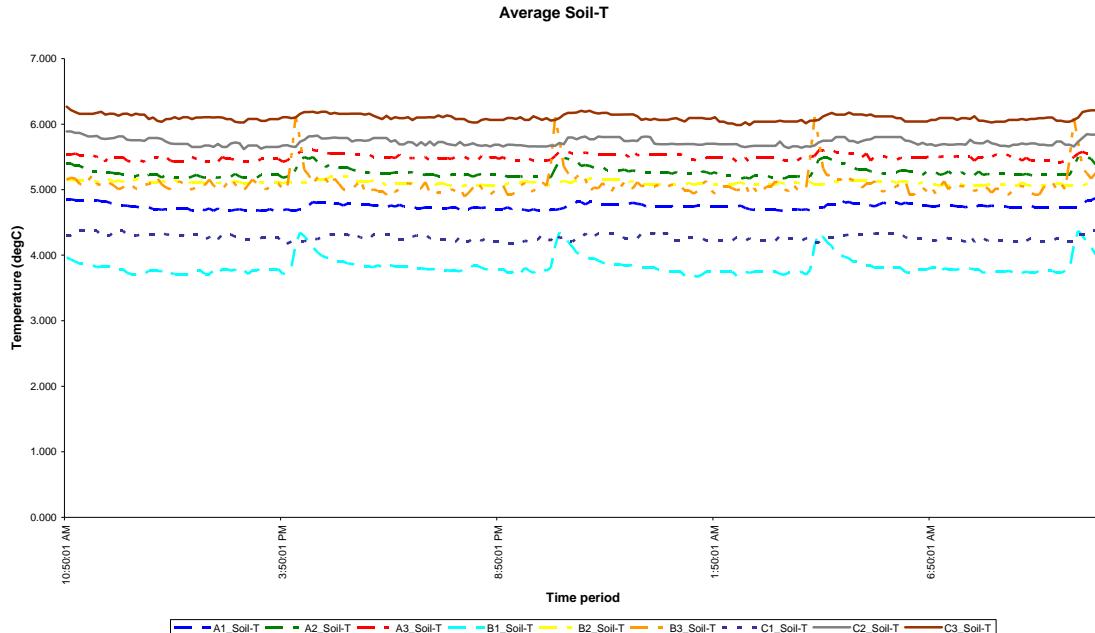


Figure B-154: Average soil temperature of S2-Alt2

Insulated Concrete Masonry Below-grade Walls

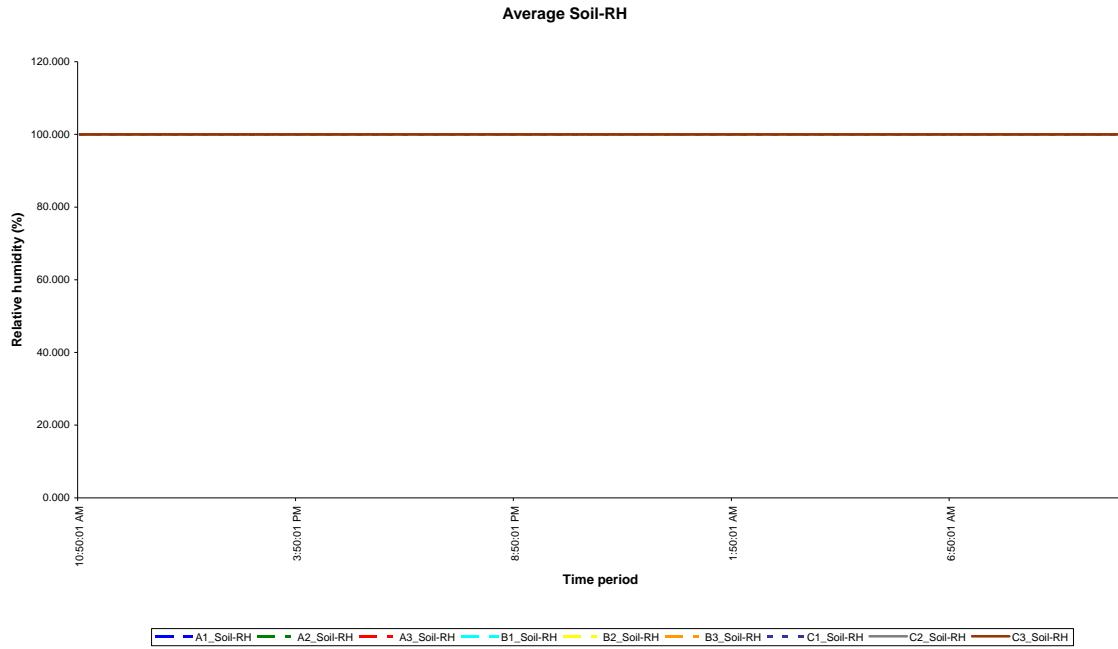


Figure B-155: Average soil relative humidity of S2-Alt2

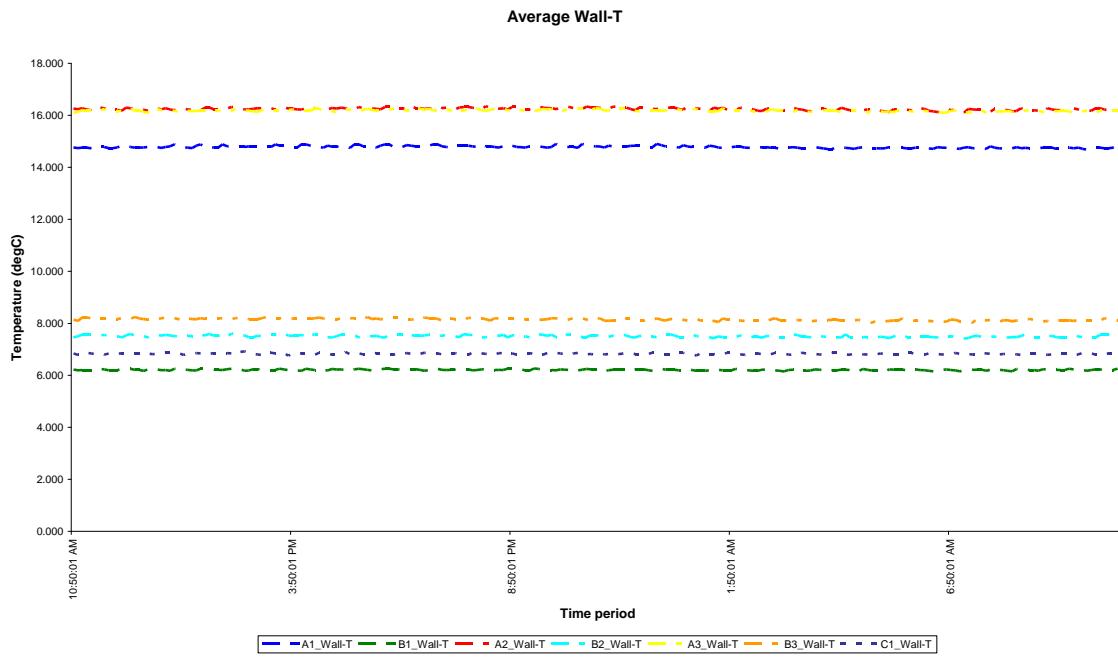


Figure B-156: Average wall temperature of S2-Alt2

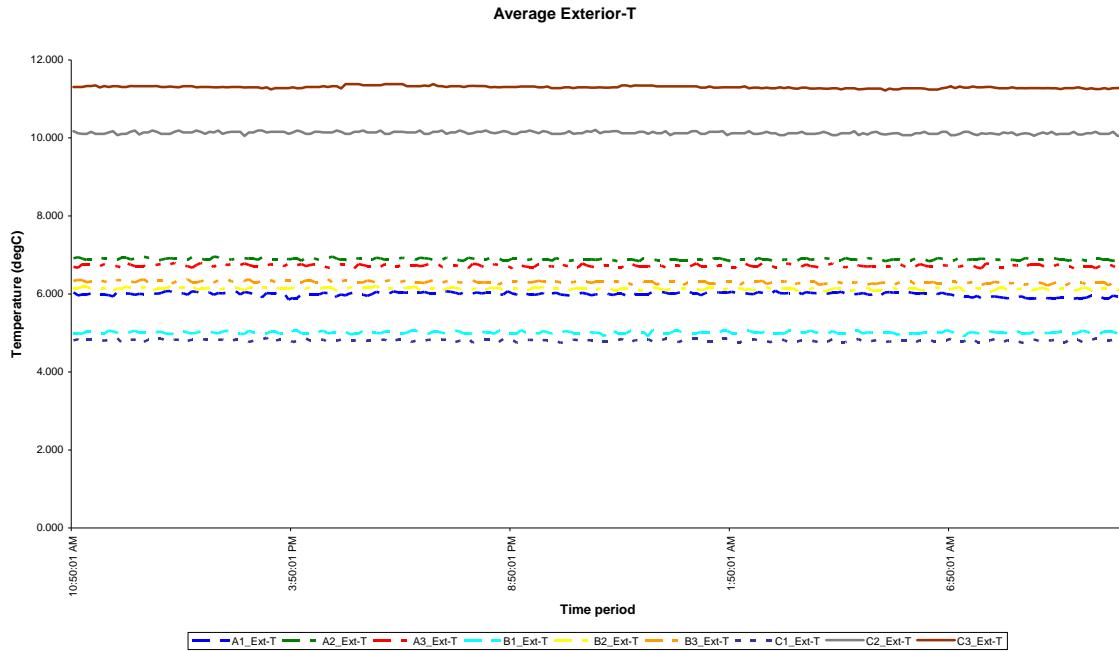


Figure B-157: Average exterior temperature of S2-Alt2

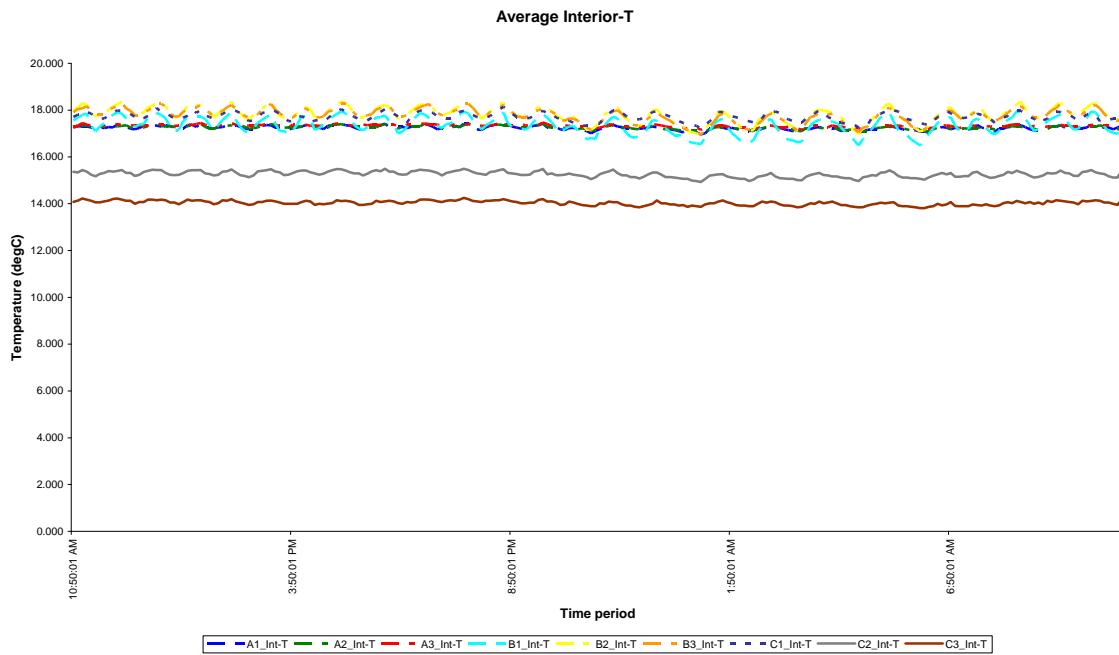


Figure B-158: Average interior temperature of S2-Alt2

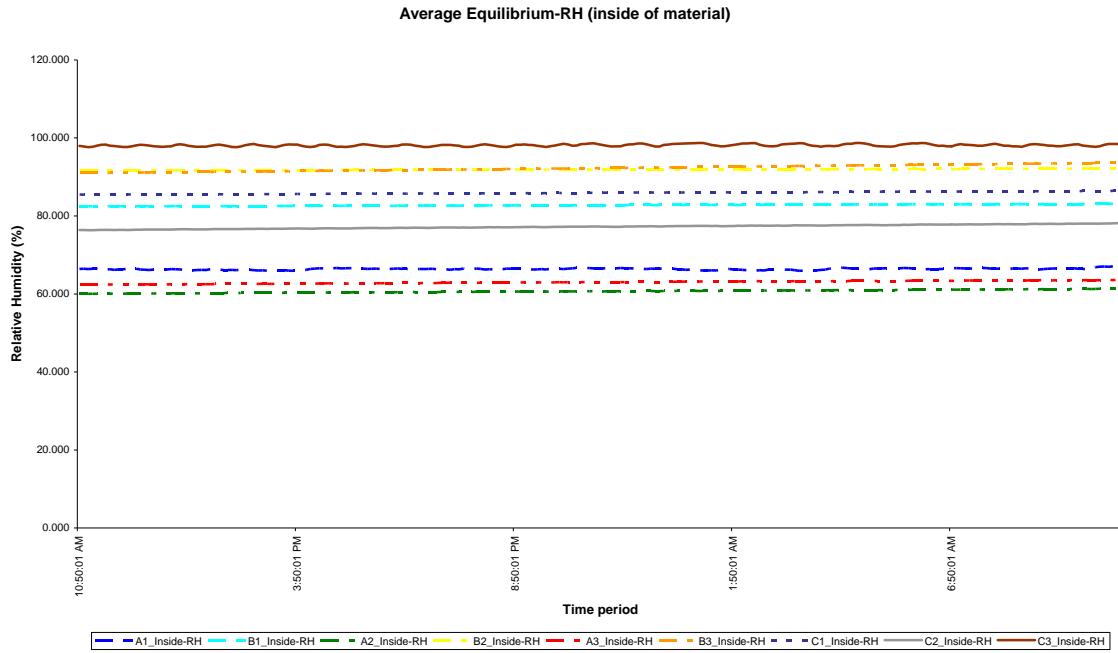


Figure B-159: Average equilibrium of relative humidity in a cavity of S2-Alt2

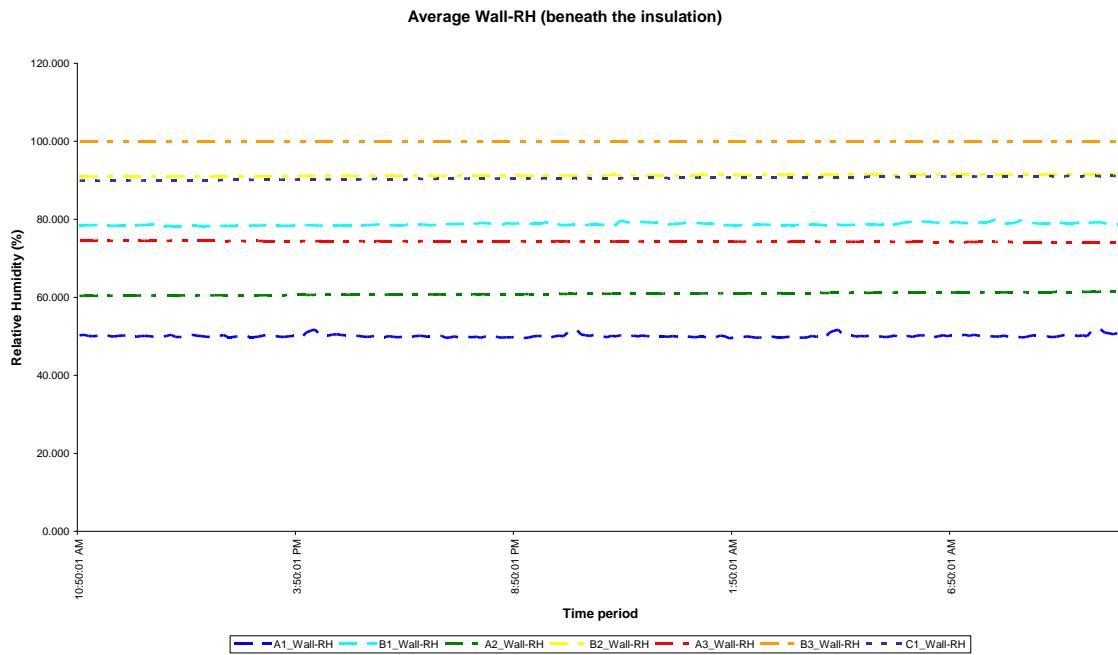


Figure B-160: Average wall relative humidity beneath the insulation of S2-Alt2

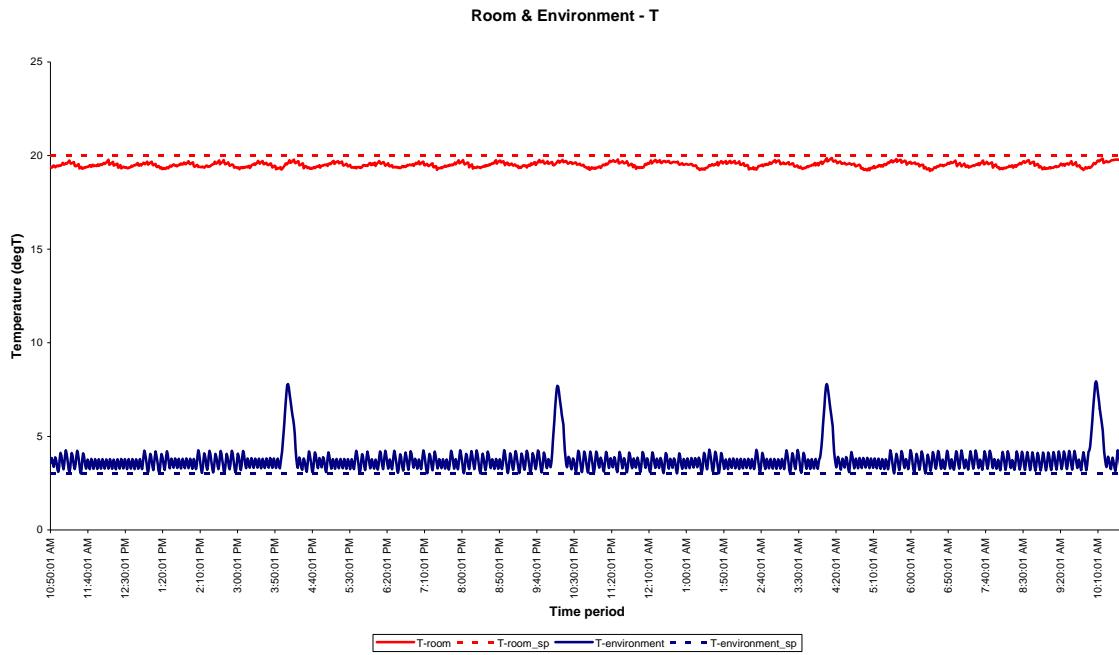


Figure B-161: Temperature of the room and environmental side during S2-Alt2

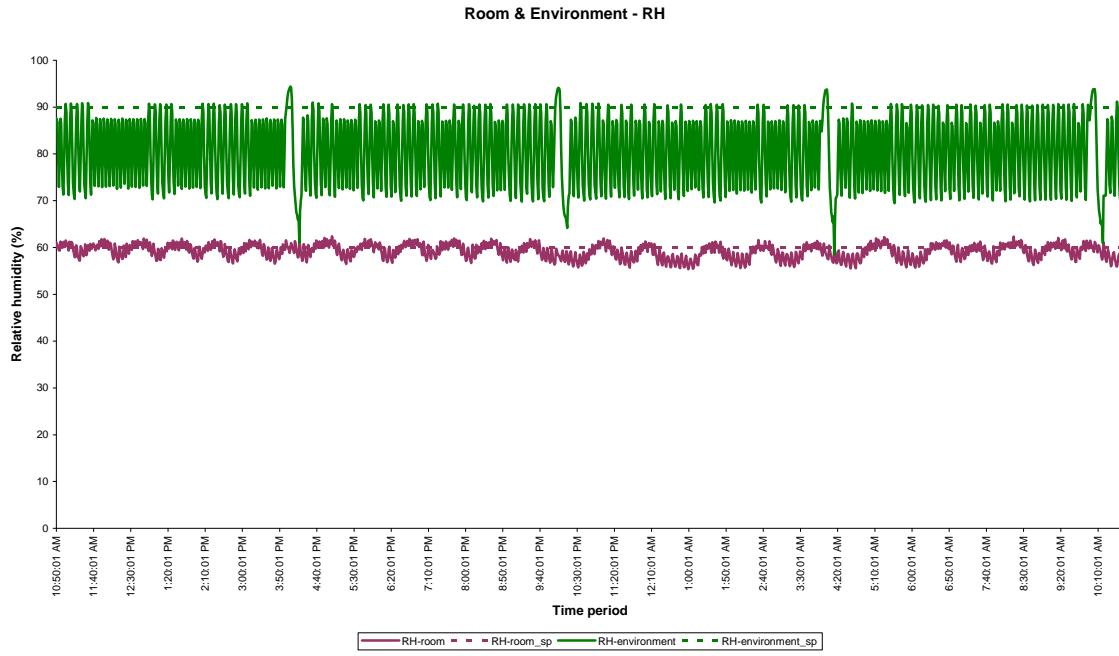


Figure B-162: Relative humidity of the room and environmental side during S2-Alt2

Test cycle: S2 – Alt3

Table B-19: Average data during the last 24 hours for each specimen of S2-Alt3

| Specimen Measurement Data | | | | | Control Loop Data | | |
|---------------------------|--------------|-------------|--------------|-------------|-------------------|-------------|--|
| B-G | A | | B | | C | | |
| 1 | A1_Soil-T | 18.696 degC | B1_Soil-T | 19.487 degC | C1_Soil-T | 20.638 degC | |
| | A1_Soil-RH | 100.000 % | B1_Soil-RH | 100.000 % | C1_Soil-RH | 100.000 % | |
| | A1_Wall-T | 18.300 degC | B1_Wall-T | 18.974 degC | C1_Wall-T | 20.394 degC | |
| | A1_Ext-T | 19.146 degC | B1_Ext-T | 18.969 degC | C1_Ext-T | 20.324 degC | |
| | A1_Int-T | 18.289 degC | B1_Int-T | 17.679 degC | C1_Int-T | 18.744 degC | |
| | A1_Inside-RH | 71.486 % | B1_Inside-RH | 87.392 % | C1_Inside-RH | 88.885 % | |
| | A1_Wall-RH | 70.892 % | B1_Wall-RH | 79.519 % | C1_Wall-RH | 77.804 % | |
| | A2_Soil-T | 18.582 degC | B2_Soil-T | 19.010 degC | C2_Soil-T | 20.313 degC | |
| | A2_Soil-RH | 100.000 % | B2_Soil-RH | 100.000 % | C2_Soil-RH | 100.000 % | |
| | A2_Wall-T | 17.737 degC | B2_Wall-T | 18.519 degC | C2_Ext-T | 19.524 degC | |
| 2 | A2_Ext-T | 18.872 degC | B2_Ext-T | 18.352 degC | C2_Int-T | 18.500 degC | |
| | A2_Int-T | 17.447 degC | B2_Int-T | 16.911 degC | C2_Inside-RH | 83.064 % | |
| | A2_Inside-RH | 64.096 % | B2_Inside-RH | 92.856 % | | | |
| | A2_Wall-RH | 65.407 % | B2_Wall-RH | 90.822 % | | | |
| | A3_Soil-T | 18.590 degC | B3_Soil-T | 19.140 degC | C3_Soil-T | 19.997 degC | |
| | A3_Soil-RH | 100.000 % | B3_Soil-RH | 100.000 % | C3_Soil-RH | 100.000 % | |
| | A3_Wall-T | 17.755 degC | B3_Wall-T | 18.512 degC | C3_Ext-T | 20.283 degC | |
| | A3_Ext-T | 18.614 degC | B3_Ext-T | 18.376 degC | C3_Int-T | 18.621 degC | |
| | A3_Int-T | 17.517 degC | B3_Int-T | 17.418 degC | C3_Inside-RH | 100.000 % | |
| | A3_Inside-RH | 66.171 % | B3_Inside-RH | 99.827 % | | | |
| 3 | A3_Wall-RH | 70.759 % | B3_Wall-RH | 75.377 % | | | |
| | Yes | A | | B | | C | |

* Measured pressure difference between Room Side & Environmental Side

| Environmental / Room Side | |
|---------------------------|-------------|
| T-room | 18.616 degC |
| RH-room | 63.371 % |
| T-room_sp | 20.000 degC |
| RH-room_sp | 60.000 % |
| T-environment | 19.553 degC |
| RH-environment | 83.426 % |
| T-environment_sp | 20.000 degC |
| RH-environment_sp | 90.000 % |

| Remarks | |
|--------------|------|
| Type: | B-G |
| Soil type: | Sand |
| Damproofing: | Yes |
| Alternative: | Alt3 |

| Legend | |
|--------------------------------|--|
| T - Temperature (degC) | |
| RH - Relative Humidity (%) | |
| SP - Setpoint (either T or RH) | |

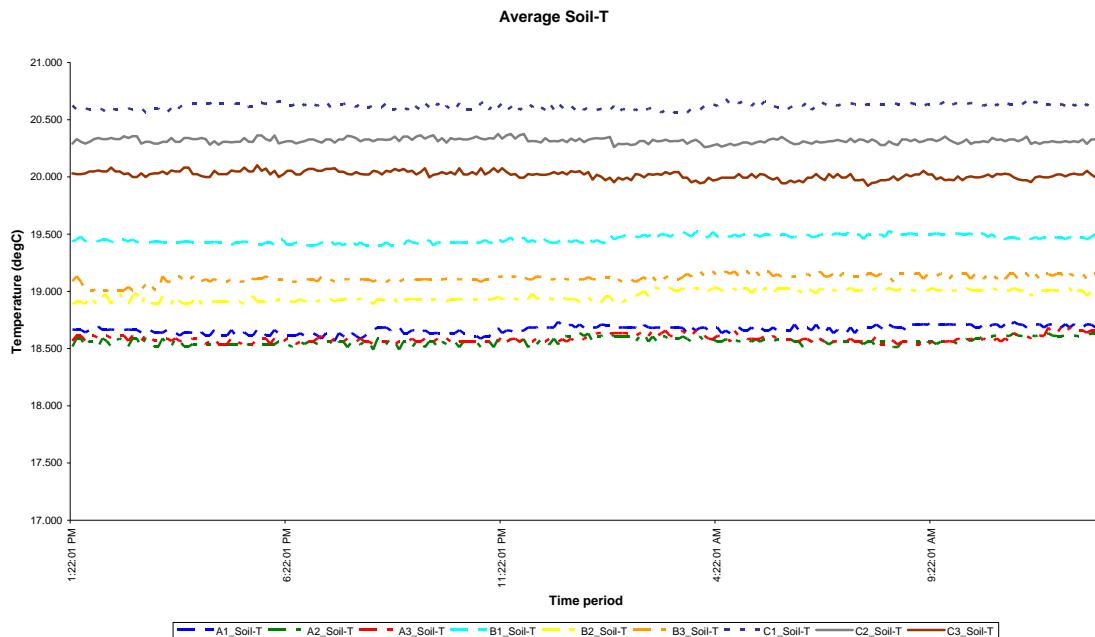


Figure B-163: Average soil temperature of S2-Alt3

Insulated Concrete Masonry Below-grade Walls

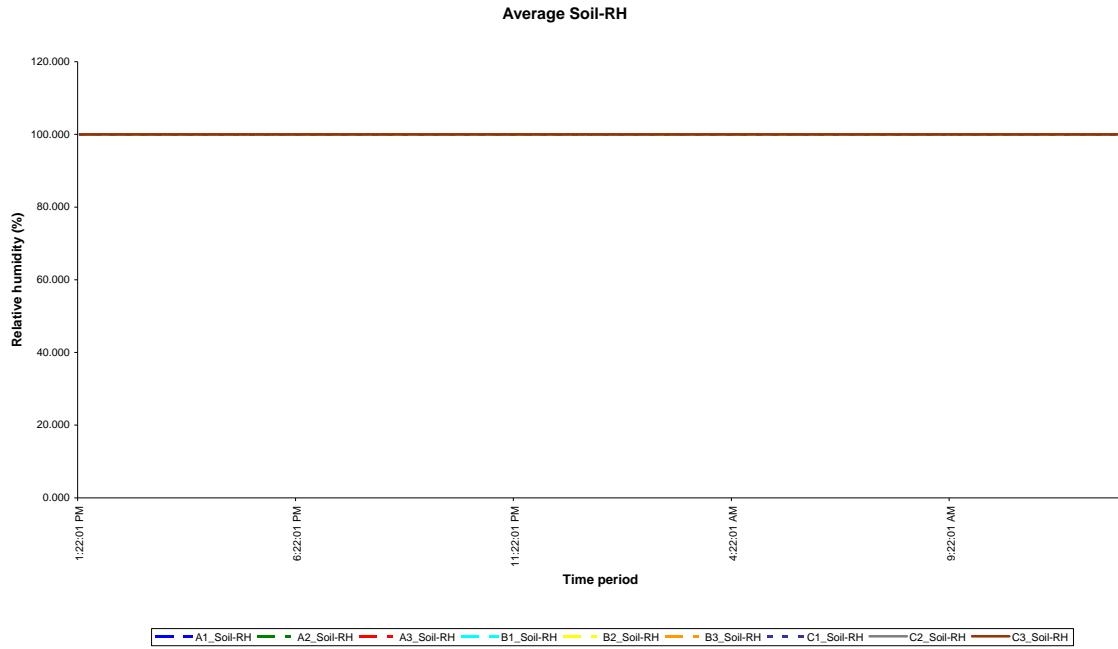


Figure B-164: Average soil relative humidity of S2-Alt3

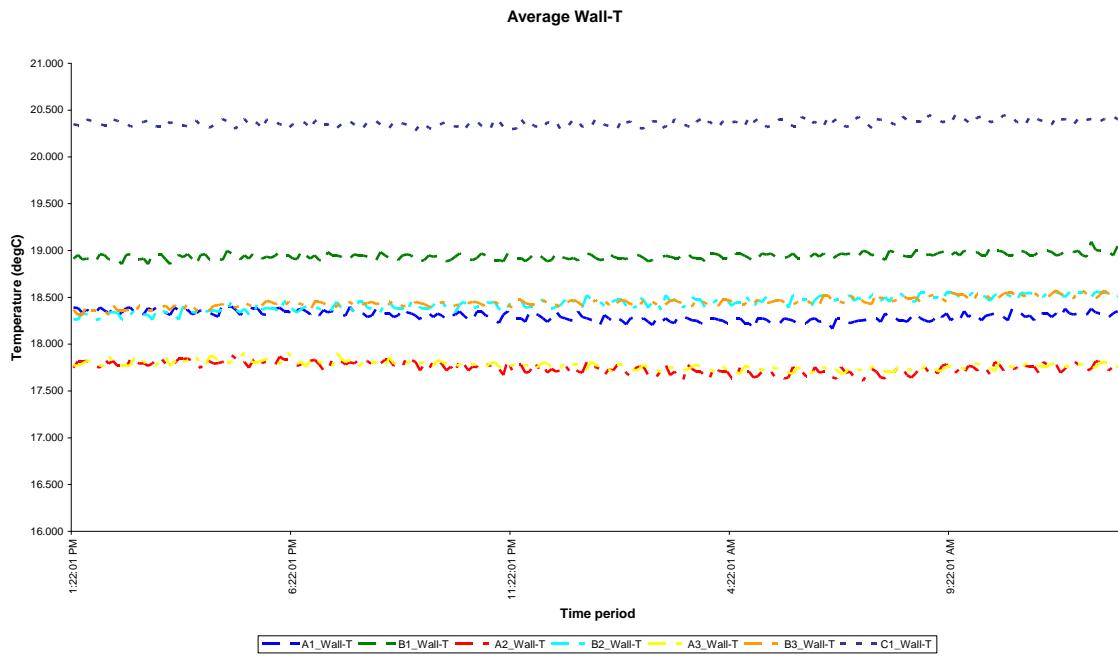


Figure B-165: Average wall temperature of S2-Alt3

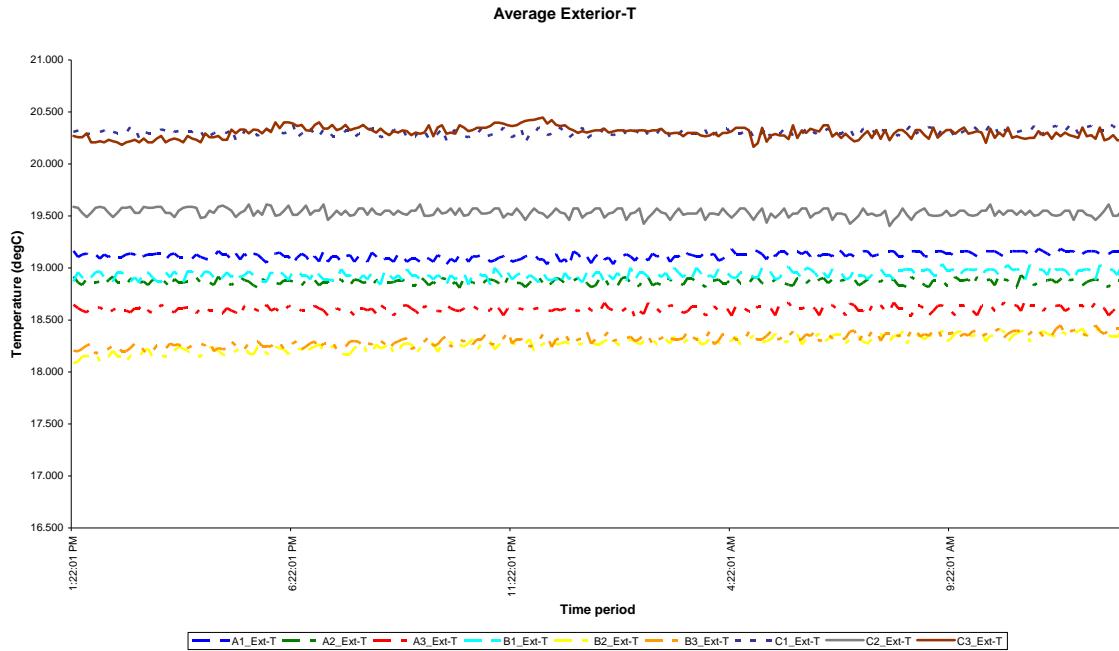


Figure B-166: Average exterior temperature of S2-Alt3

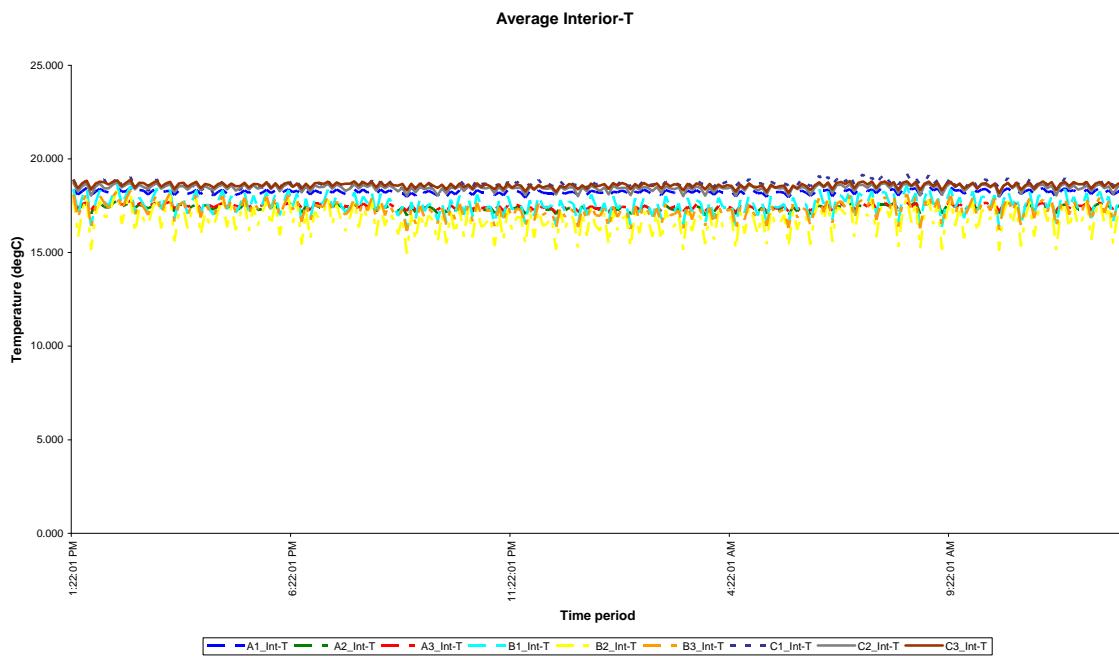


Figure B-167: Average interior temperature of S2-Alt3

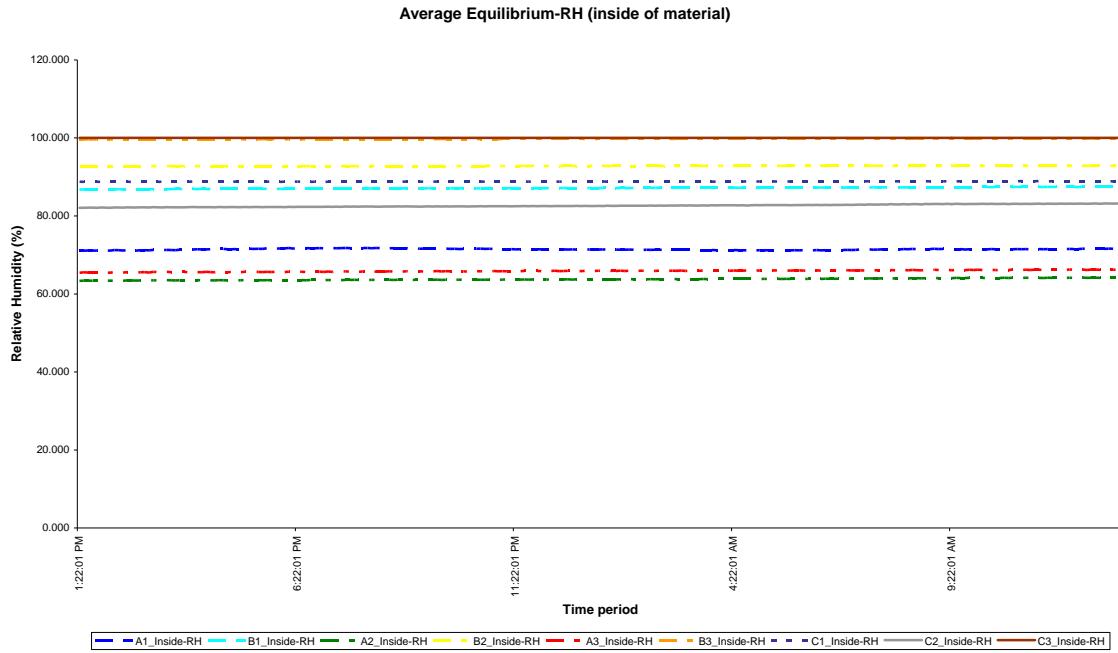


Figure B-168: Average equilibrium of relative humidity in a cavity of S2-Alt3

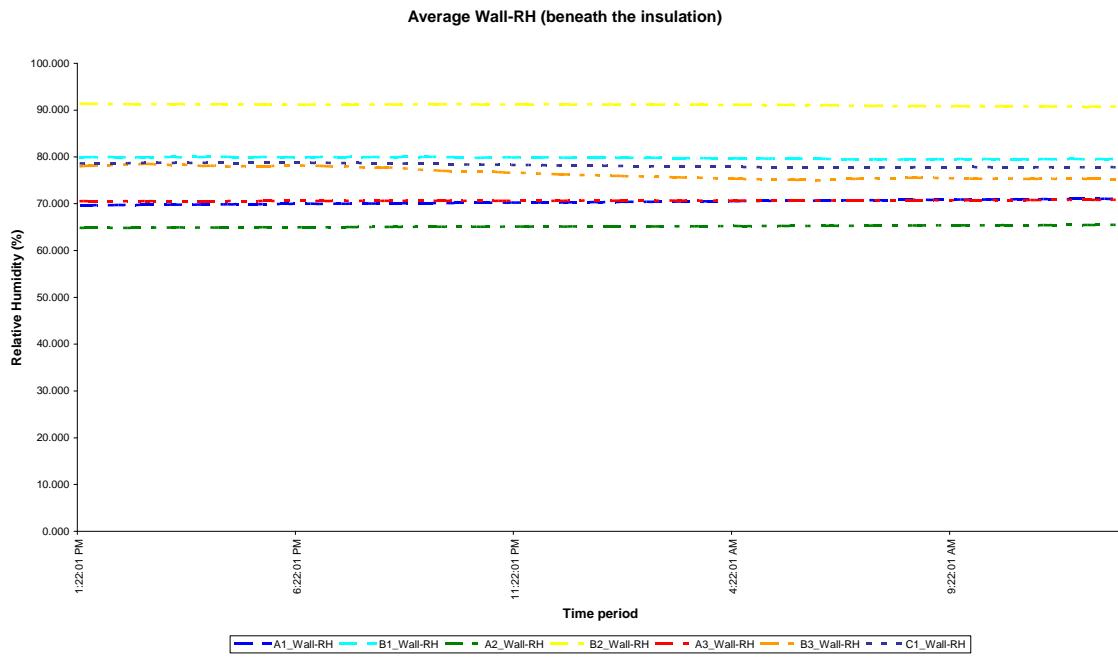


Figure B-169: Average wall relative humidity beneath the insulation of S2-Alt3

Insulated Concrete Masonry Below-grade Walls

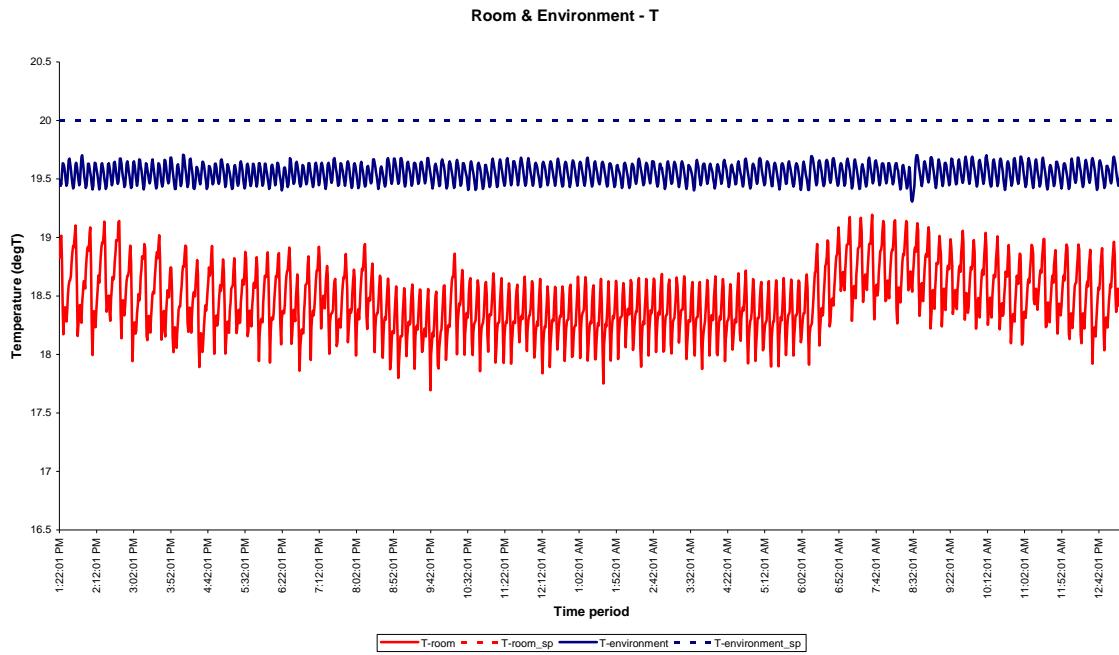


Figure B-170: Temperature of the room and environmental side during S2-Alt3

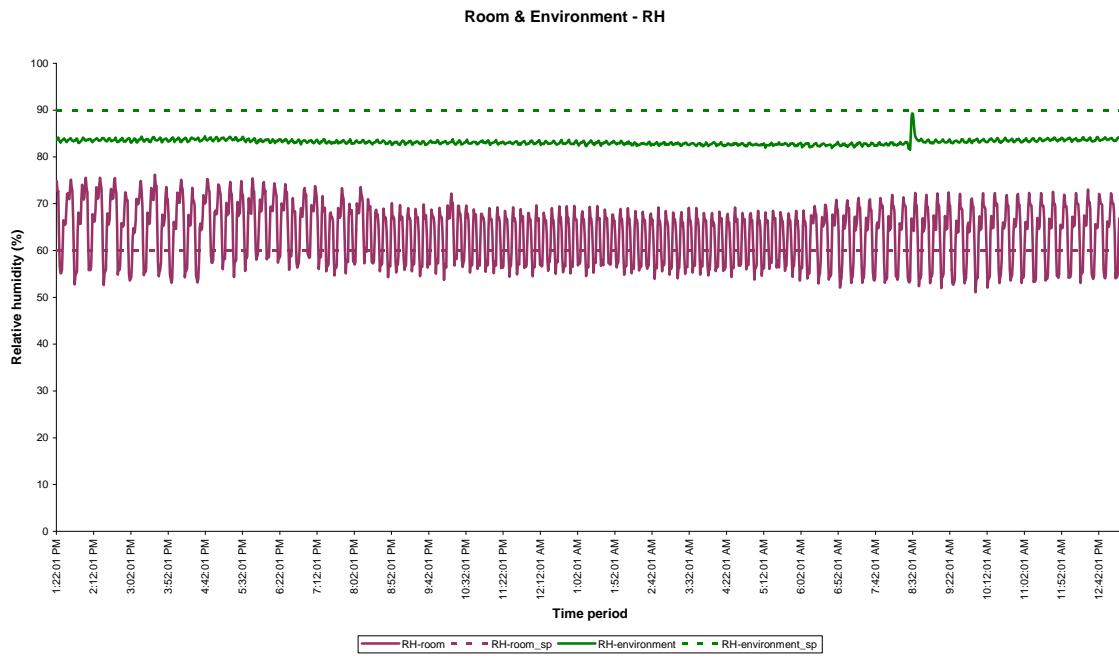


Figure B-171: Relative humidity of the room and environmental side during S2-Alt3

Test cycle: S2 – Alt4

Table B-20: Average data during the last 24 hours for each specimen of S2-Alt4

| Specimen Measurement Data | | | | | Control Loop Data | | | |
|---------------------------|--------------|-------------|--------------|-------------|--------------------------|-------------|------|--|
| B-G | A | | B | | C | | Sand | |
| 1 | A1_Soil-T | 19.030 degC | B1_Soil-T | 19.592 degC | C1_Soil-T | 20.706 degC | 1 | |
| | A1_Soil-RH | 100.000 % | B1_Soil-RH | 100.000 % | C1_Soil-RH | 100.000 % | | |
| | A1_Wall-T | 18.657 degC | B1_Wall-T | 19.278 degC | C1_Wall-T | 20.512 degC | | |
| | A1_Ext-T | 19.905 degC | B1_Ext-T | 19.248 degC | C1_Ext-T | 20.302 degC | | |
| | A1_Int-T | 18.532 degC | B1_Int-T | 18.099 degC | C1_Int-T | 19.630 degC | | |
| | A1_Inside-RH | 62.646 % | B1_Inside-RH | 91.426 % | C1_Inside-RH | 89.279 % | | |
| 2 | A1_Wall-RH | 72.436 % | B1_Wall-RH | 77.081 % | C1_Wall-RH | 69.444 % | 2 | |
| | A2_Soil-T | 18.950 degC | B2_Soil-T | 19.196 degC | C2_Soil-T | 20.305 degC | | |
| | A2_Soil-RH | 100.000 % | B2_Soil-RH | 100.000 % | C2_Soil-RH | 100.000 % | | |
| | A2_Wall-T | 17.947 degC | B2_Wall-T | 18.852 degC | C2_Ext-T | 19.869 degC | | |
| | A2_Ext-T | 19.183 degC | B2_Ext-T | 18.645 degC | C2_Int-T | 19.231 degC | | |
| | A2_Int-T | 17.611 degC | B2_Int-T | 16.999 degC | C2_Inside-RH | 83.716 % | | |
| 3 | A2_Inside-RH | 61.128 % | B2_Inside-RH | 93.231 % | C2_Wall-RH | 83.030 % | 3 | |
| | A2_Wall-RH | 66.902 % | B3_Soil-T | 19.287 degC | C3_Soil-T | 19.823 degC | | |
| | A3_Soil-T | 18.896 degC | B3_Soil-RH | 100.000 % | C3_Soil-RH | 100.000 % | | |
| | A3_Soil-RH | 100.000 % | B3_Wall-T | 18.631 degC | C3_Ext-T | 20.720 degC | | |
| | A3_Wall-T | 17.655 degC | B3_Ext-T | 18.500 degC | C3_Int-T | 18.634 degC | | |
| | A3_Ext-T | 18.766 degC | B3_Int-T | 16.795 degC | C3_Inside-RH | 99.956 % | | |
| Yes | A3_Int-T | 17.304 degC | B3_Inside-RH | 101.520 % | *Pressure diff. 7.757 Pa | | Alt4 | |
| | A3_Inside-RH | 61.710 % | B3_Wall-RH | 56.702 % | | | | |
| | A3_Wall-RH | 70.373 % | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |

* Measured pressure difference between Room Side & Environmental Side

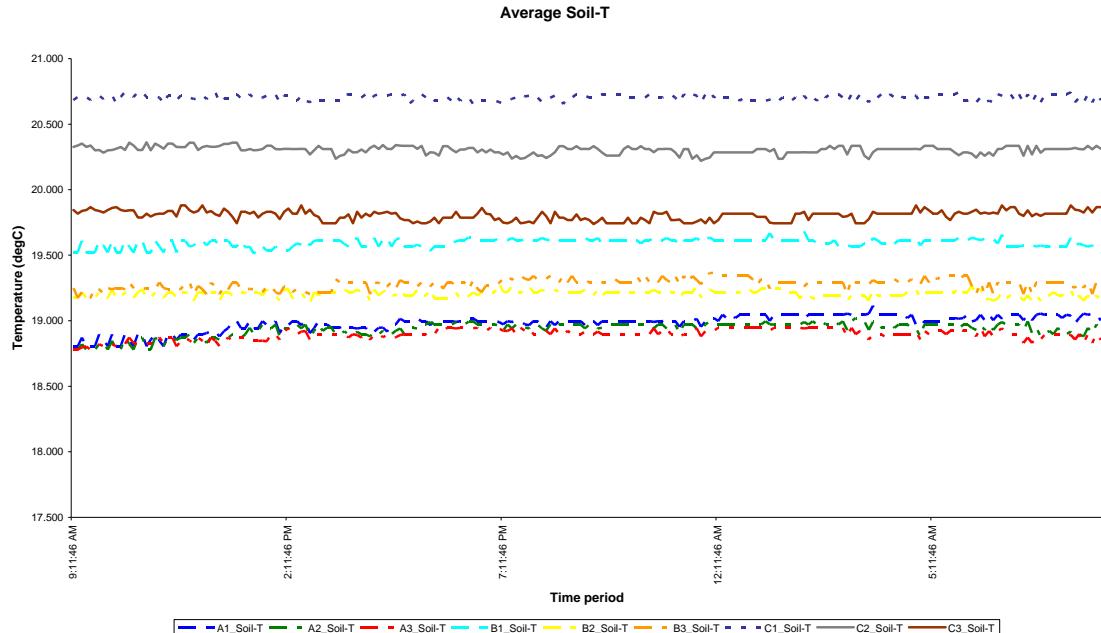


Figure B-172: Average soil temperature of S2-Alt4

Insulated Concrete Masonry Below-grade Walls

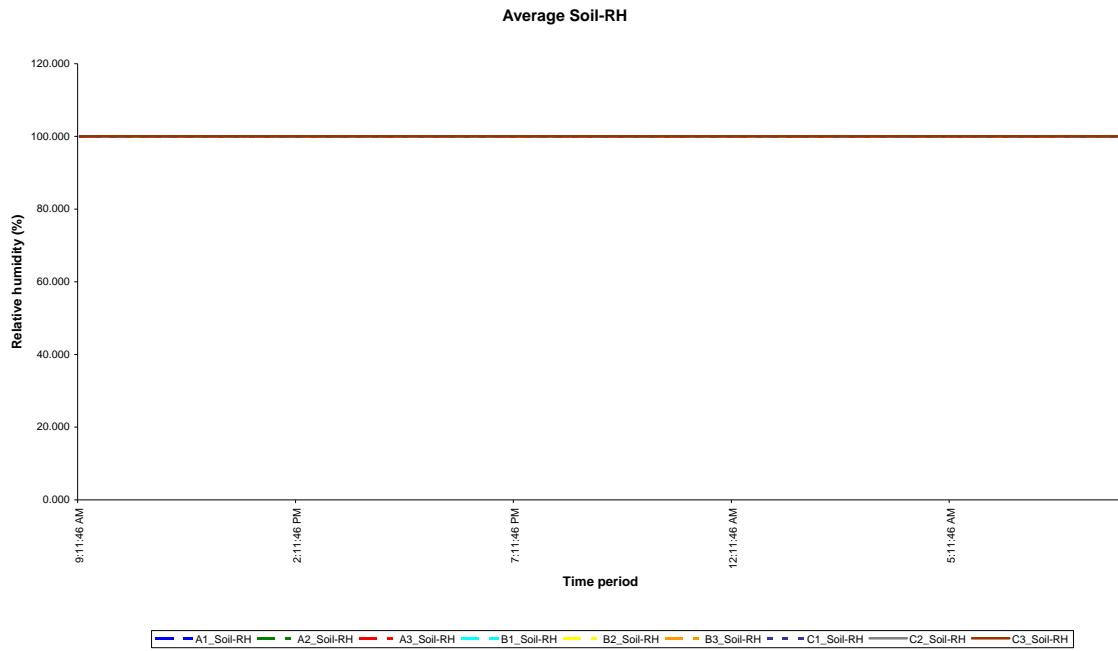


Figure B-173: Average soil relative humidity of S2-Alt4

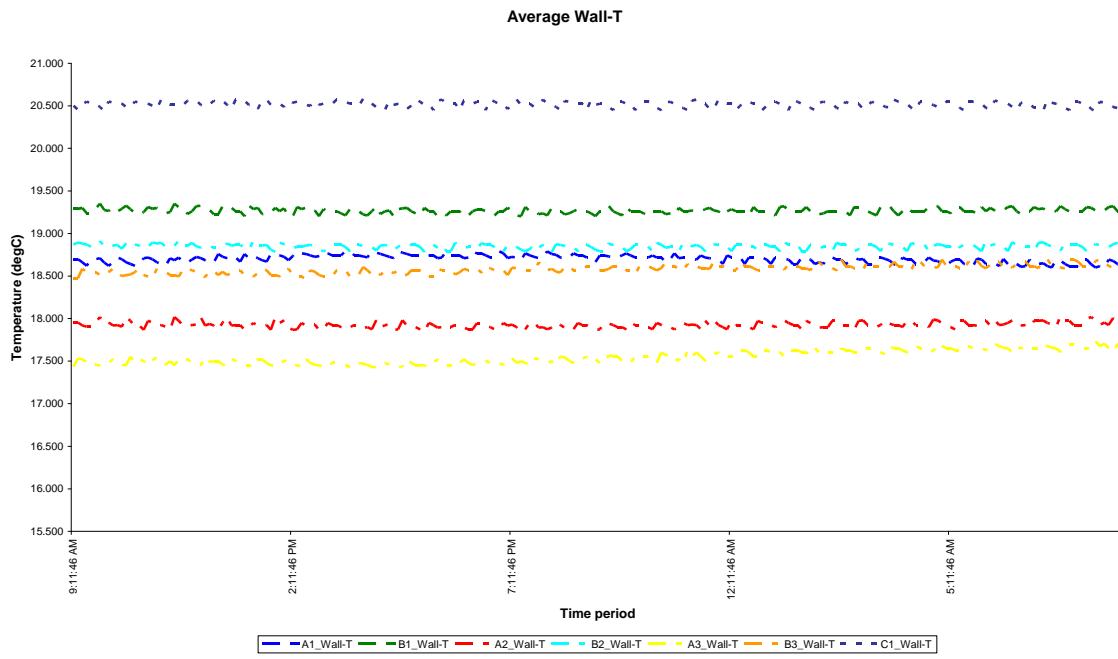


Figure B-174: Average wall temperature of S2-Alt4

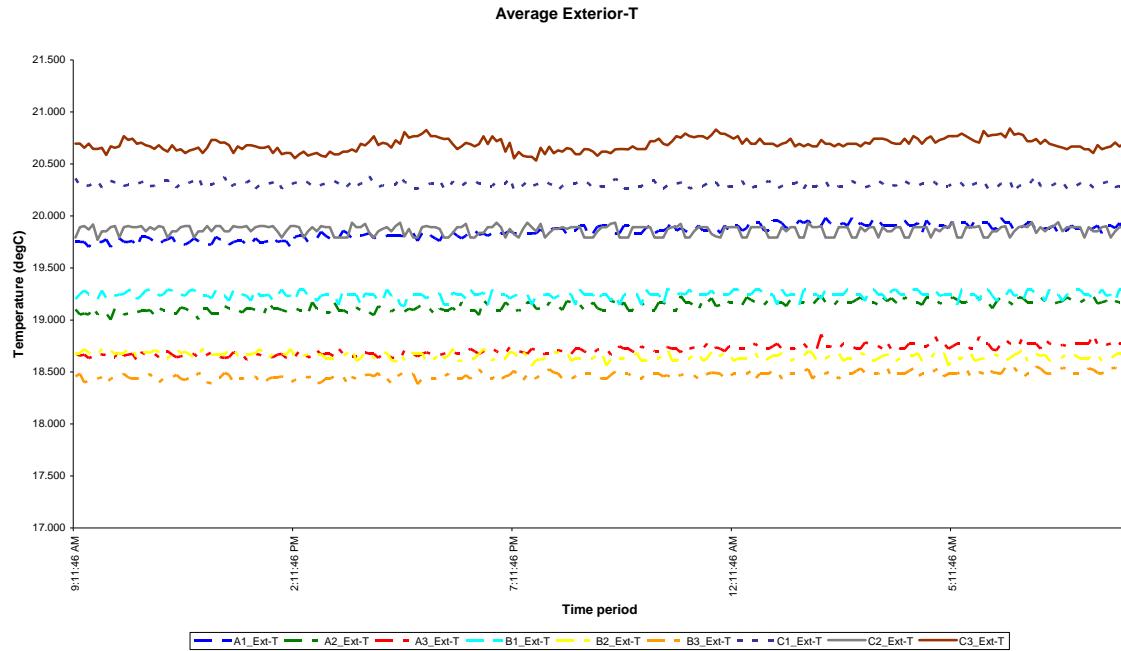


Figure B-175: Average exterior temperature of S2-Alt4

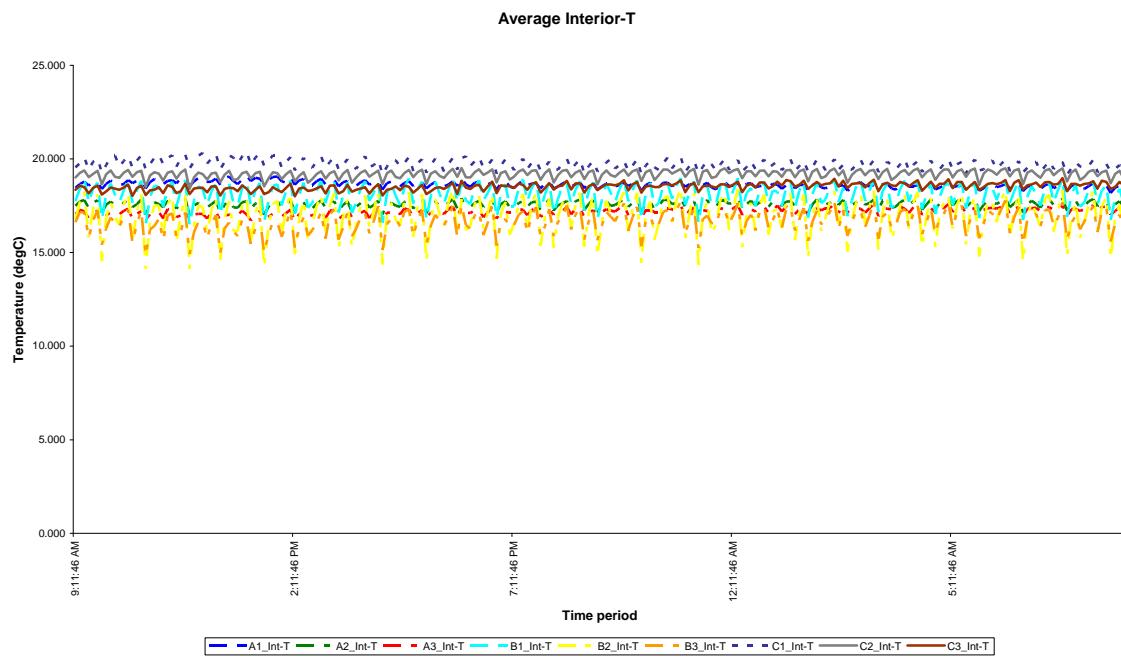


Figure B-176: Average interior temperature of S2-Alt4

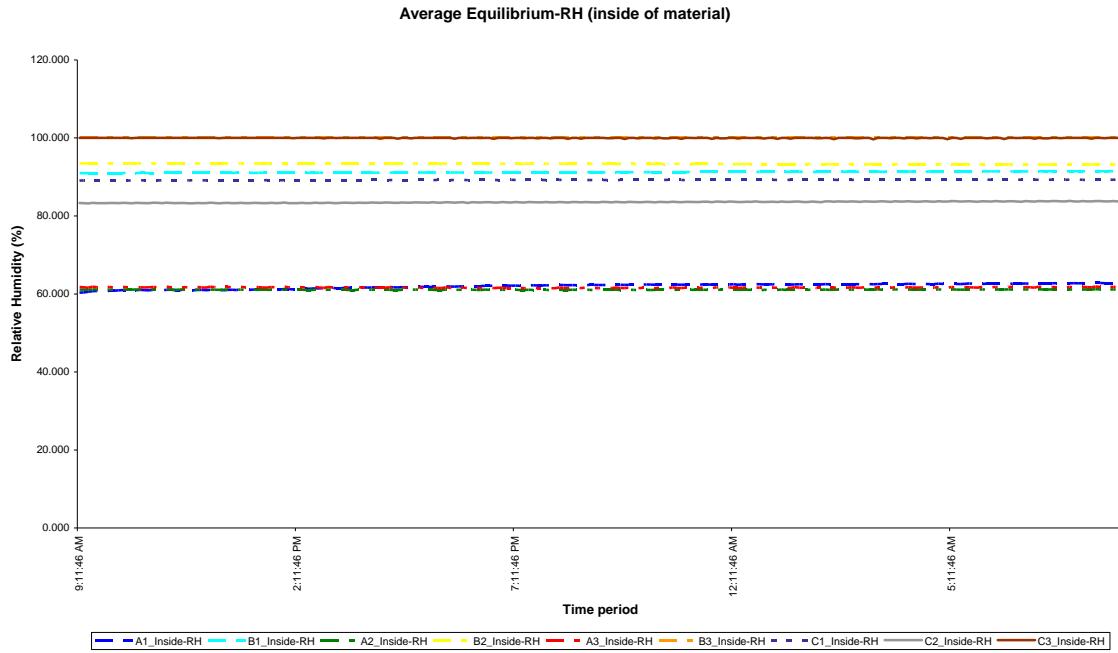


Figure B-177: Average equilibrium of relative humidity in a cavity of S2-Alt4

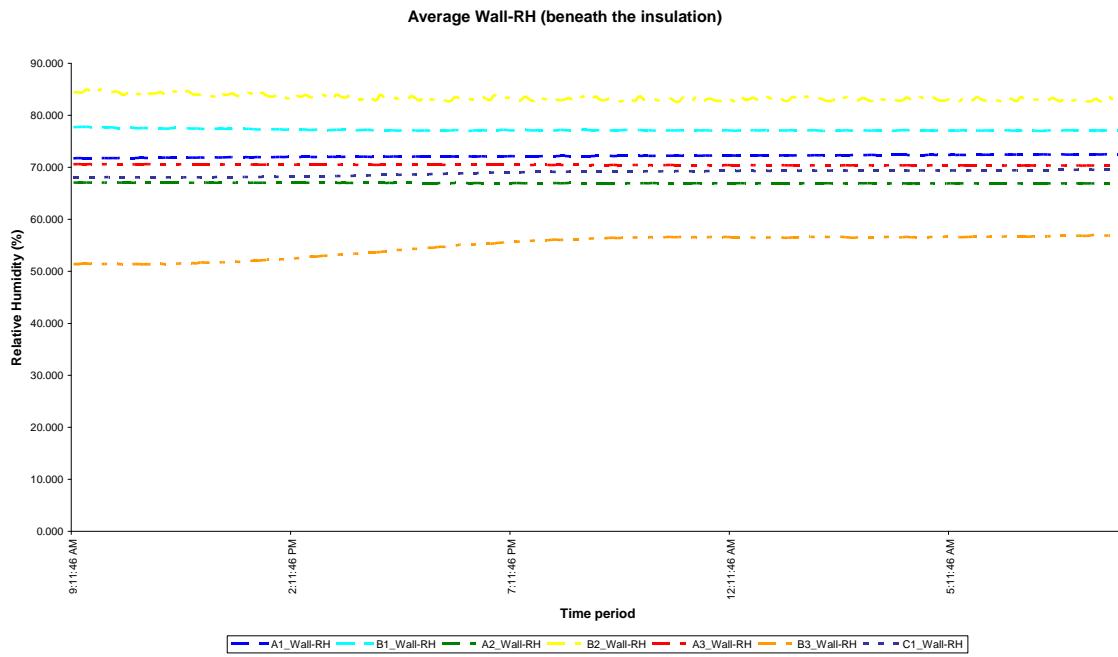


Figure B-178: Average wall relative humidity beneath the insulation of S2-Alt4

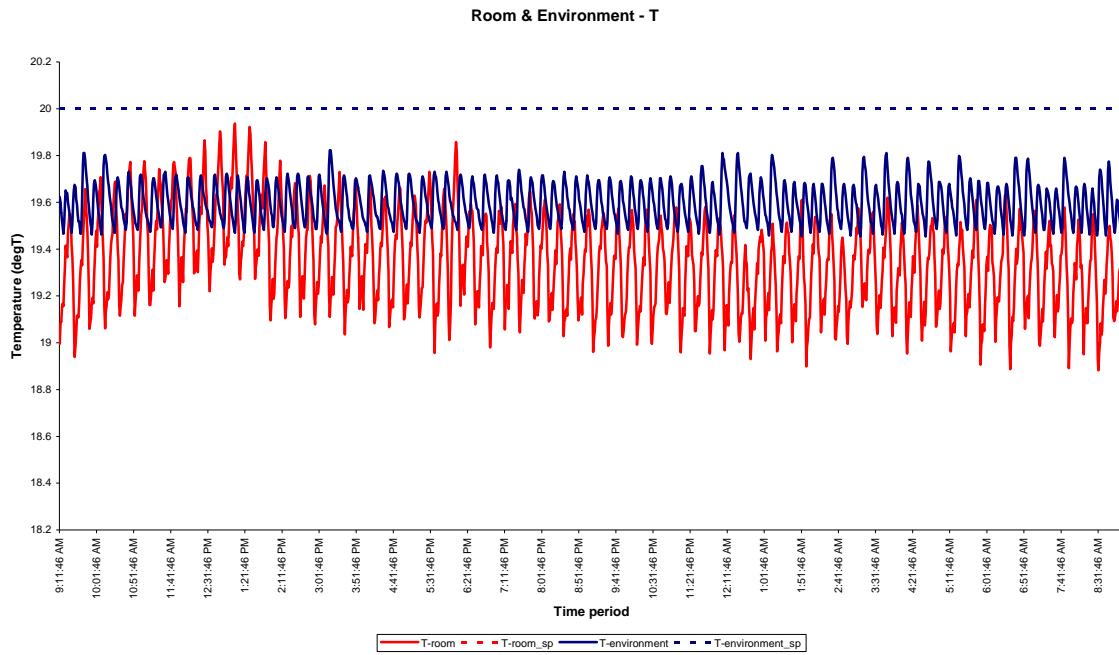


Figure B-179: Temperature of the room and environmental side during S2-Alt4

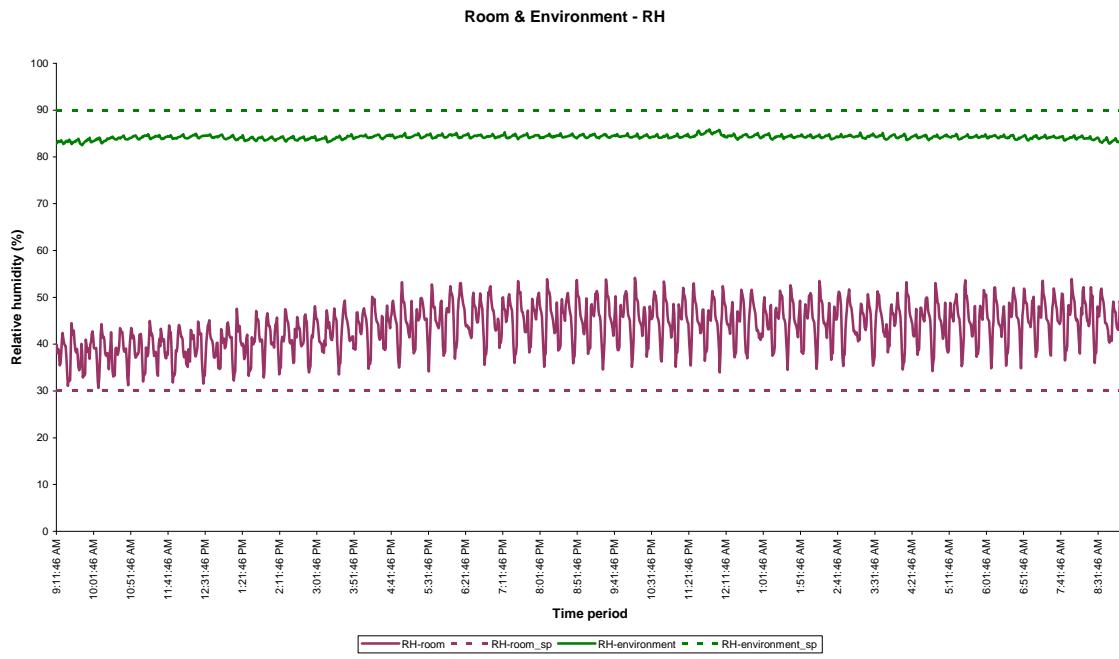


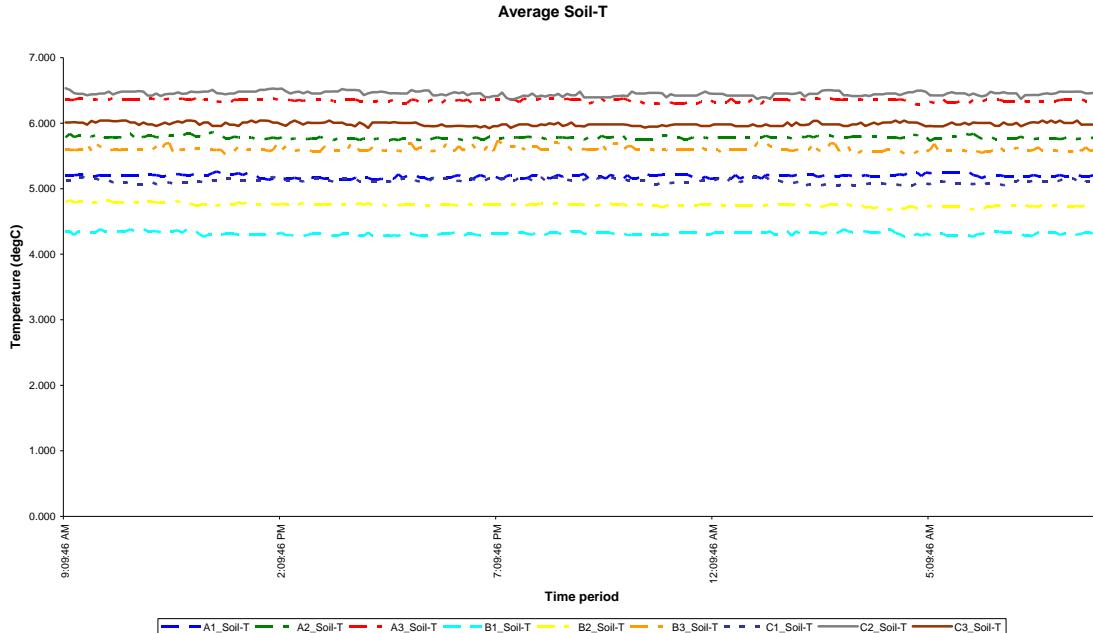
Figure B-180: Relative humidity of the room and environmental side during S2-Alt4

Measurement series: **C2 (Clay; with dampproofing)**

 Test cycle: **C2 – Alt1**
Table B-21: Average data during the last 24 hours for each specimen of C2-Alt1

| Specimen Measurement Data | | | | | Control Loop Data | | |
|---------------------------|--|--|--|------|--|---------|--|
| B-G | A | B | C | Clay | Environmental / Room Side | | |
| 1 | A1_Soil-T 5.209 degC A1_Soil-RH 100.000 % A1_Wall-T 14.955 degC A1_Ext-T 6.822 degC A1_Int-T 17.418 degC A1_Inside-RH 53.491 % A1_Wall-RH 60.712 % | B1_Soil-T 4.316 degC B1_Soil-RH 100.000 % B1_Wall-T 6.745 degC B1_Ext-T 5.351 degC B1_Int-T 18.285 degC B1_Inside-RH 100.000 % B1_Wall-RH 85.460 % | C1_Soil-T 5.091 degC C1_Soil-RH 100.000 % C1_Wall-T 7.560 degC C1_Ext-T 5.583 degC C1_Int-T 18.149 degC C1_Inside-RH 100.000 % C1_Wall-RH 81.092 % | 1 | T-room 19.588 degC RH-room 32.094 % T-room_sp 20.000 degC RH-room_sp 30.000 % T-environment 3.459 degC RH-environment 86.494 % T-environment_sp 3.000 degC RH-environment_sp 90.000 % | Remarks | |
| | A2_Soil-T 5.781 degC A2_Soil-RH 100.000 % A2_Wall-T 16.761 degC A2_Ext-T 7.775 degC A2_Int-T 17.790 degC A2_Inside-RH 52.818 % A2_Wall-RH 58.421 % | B2_Soil-T 4.728 degC B2_Soil-RH 100.000 % B2_Wall-T 8.497 degC B2_Ext-T 7.168 degC B2_Int-T 18.379 degC B2_Inside-RH 93.428 % B2_Wall-RH 83.832 % | C2_Soil-T 6.448 degC C2_Soil-RH 100.000 % C2_Wall-T 12.387 degC C2_Ext-T 16.527 degC C2_Int-T 97.572 % | | Type: B-G Soil type: Clay Damproofing: Yes Alternative: Alt1 | | |
| | A3_Soil-T 6.341 degC A3_Soil-RH 100.000 % A3_Wall-T 16.737 degC A3_Ext-T 7.807 degC A3_Int-T 17.879 degC A3_Inside-RH 53.477 % A3_Wall-RH 63.552 % | B3_Soil-T 5.581 degC B3_Soil-RH 100.000 % B3_Wall-T 8.627 degC B3_Ext-T 6.898 degC B3_Int-T 18.106 degC B3_Inside-RH 98.456 % B3_Wall-RH 76.989 % | C3_Soil-T 5.994 degC C3_Soil-RH 100.000 % C3_Wall-T 16.606 degC C3_Ext-T 15.714 degC C3_Int-T 97.365 % | | *Pressure diff. 7.836 Pa | | |
| Yes | A | B | C | | Legend | | |
| | | | | | T - Temperature (degC) RH - Relative Humidity (%) SP - Setpoint (either T or RH) | | |
| | | | | | | | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-181: Average soil temperature of C2-Alt1

Insulated Concrete Masonry Below-grade Walls

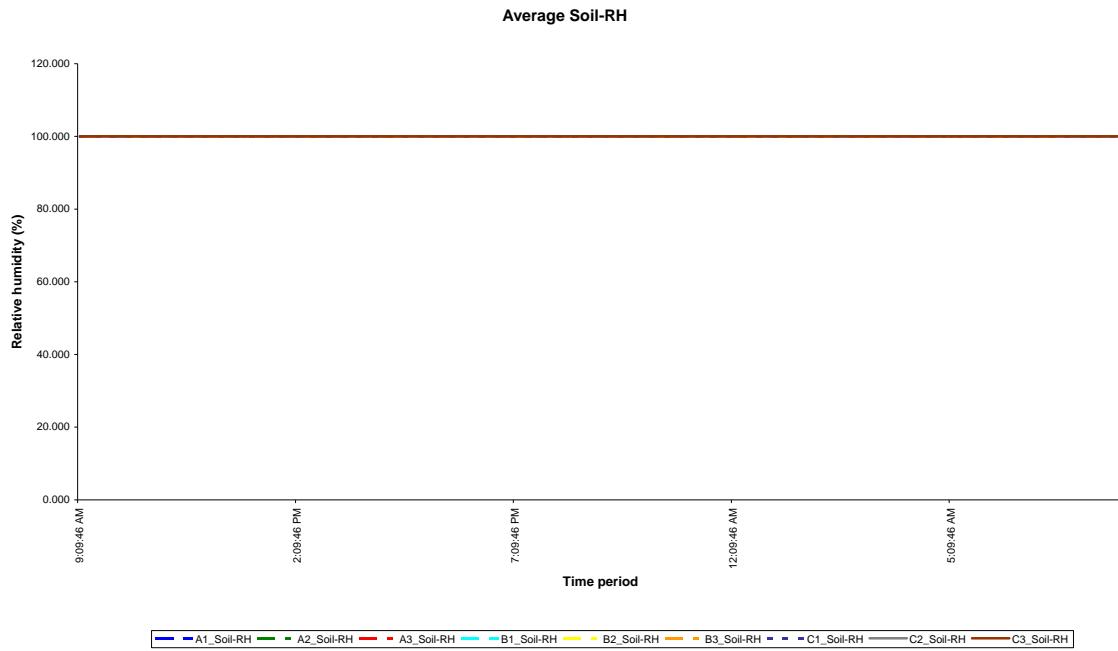


Figure B-182: Average soil relative humidity of C2-Alt1

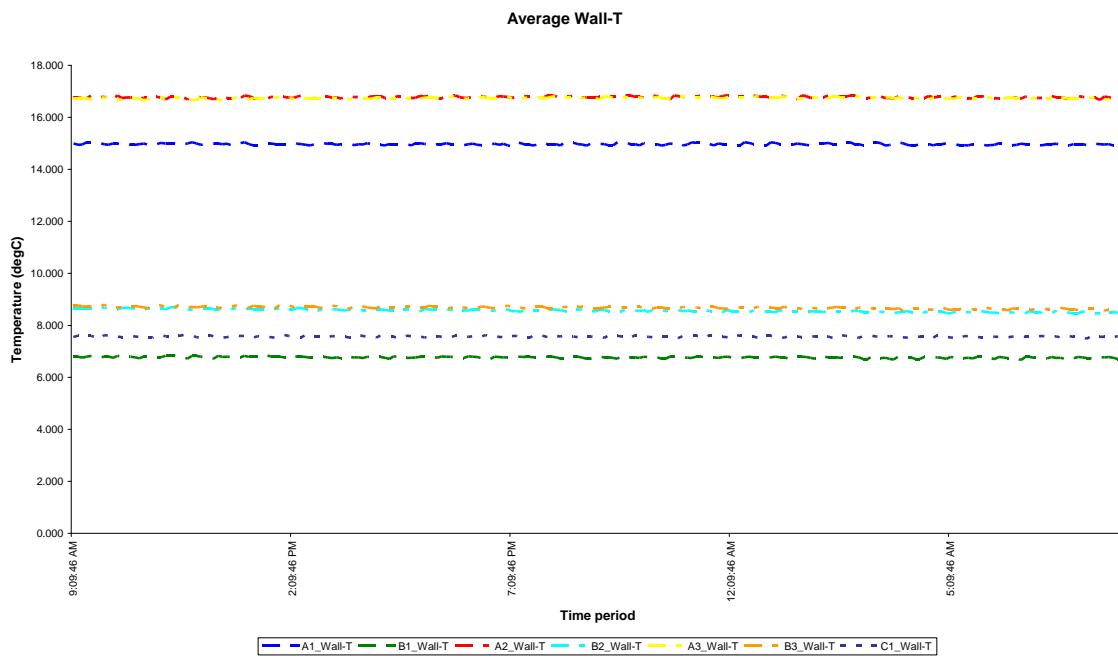


Figure B-183: Average wall temperature of C2-Alt1

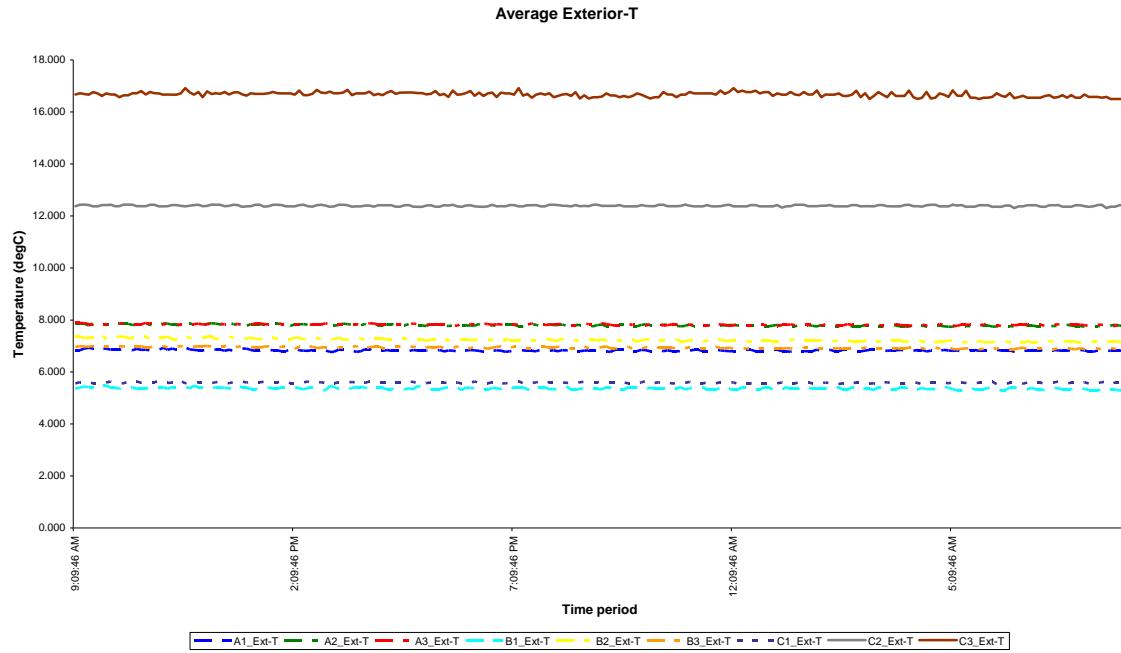


Figure B-184: Average exterior temperature of C2-Alt1

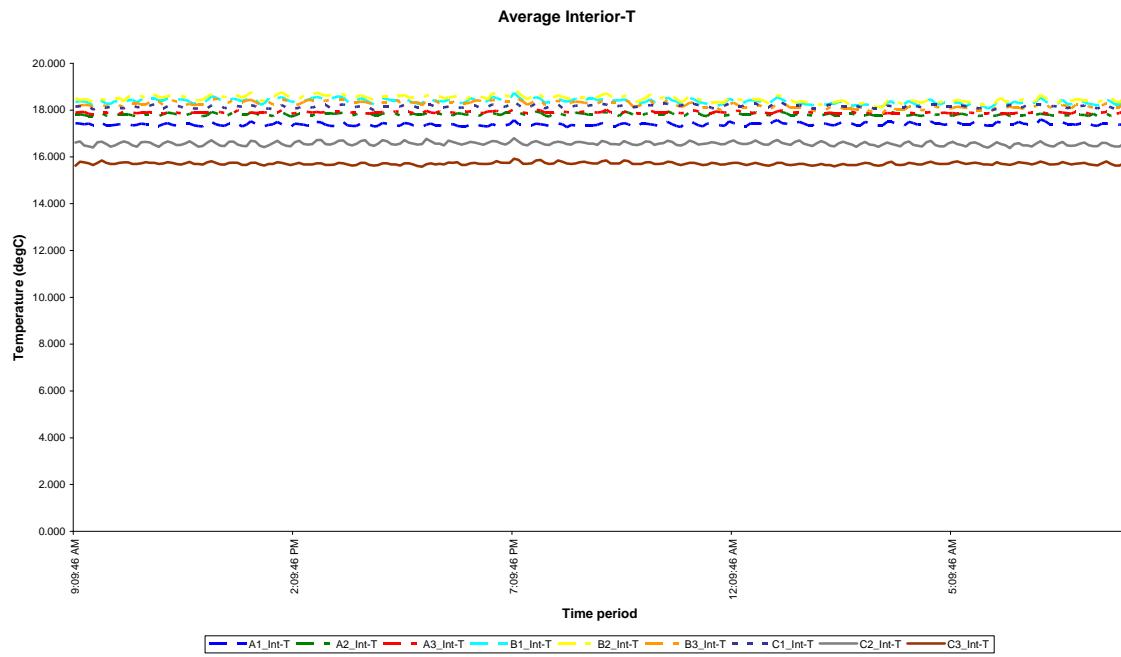


Figure B-185: Average interior temperature of C2-Alt1

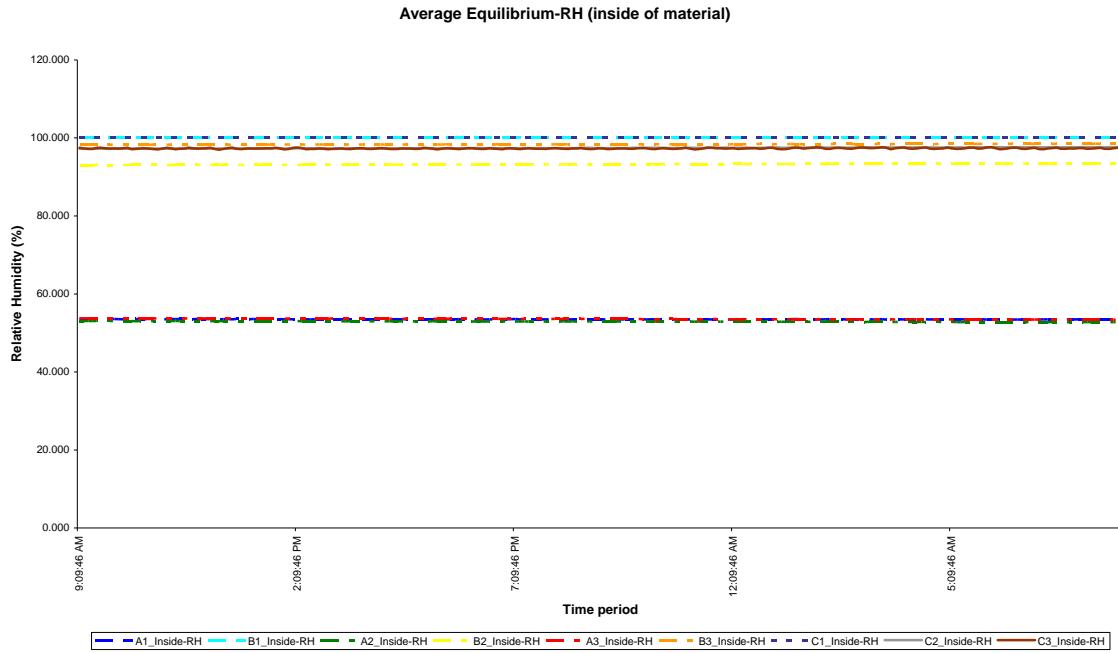


Figure B-186: Average equilibrium of relative humidity in a cavity of C2-Alt1

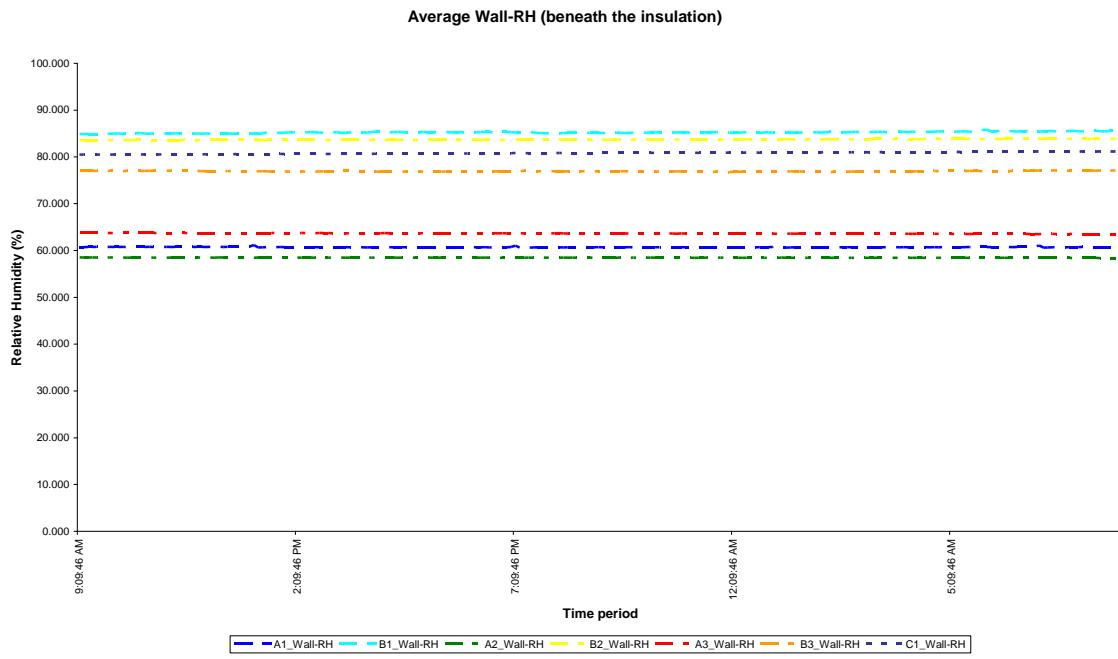


Figure B-187: Average wall relative humidity beneath the insulation of C2-Alt1

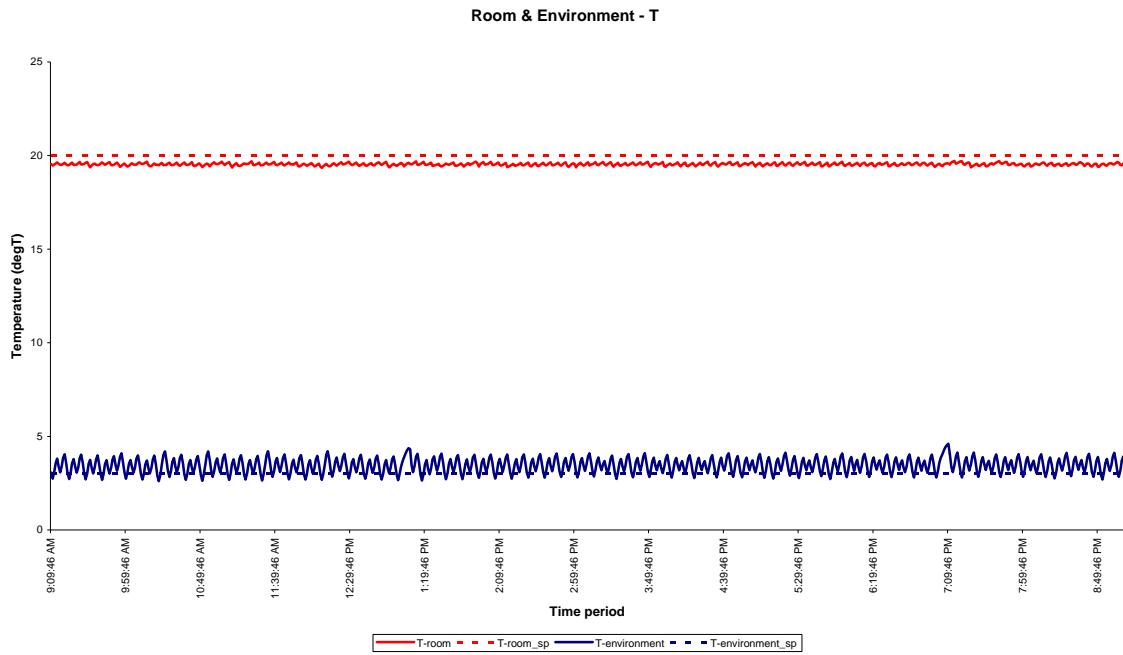


Figure B-188: Temperature of the room and environmental side during C2-Alt1

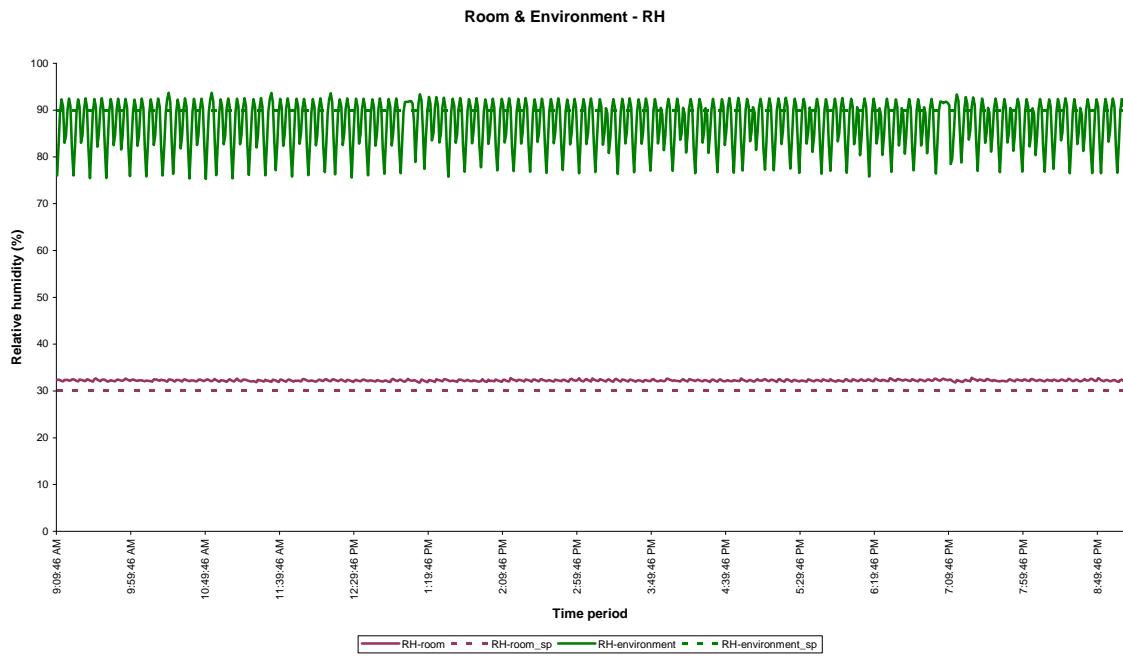


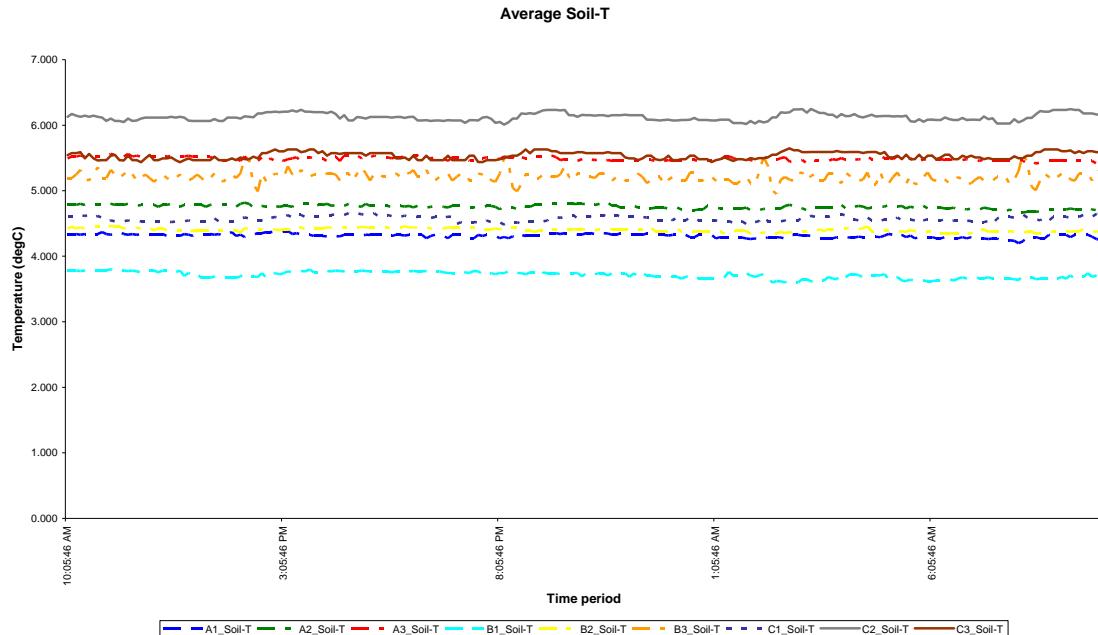
Figure B-189: Relative humidity of the room and environmental side during C2-Alt1

Test cycle: C2 – Alt2

Table B-22: Average data during the last 24 hours for each specimen of C2-Alt2

| Specimen Measurement Data | | | | | Control Loop Data | | |
|---------------------------|--|--|--|------|--|---------|--|
| B-G | A | B | C | Clay | Environmental / Room Side | | |
| 1 | A1_Soil-T 4.286 degC A1_Soil-RH 100.000 % A1_Wall-T 14.858 degC A1_Ext-T 5.527 degC A1_Int-T 17.743 degC A1_Inside-RH 54.006 % A1_Wall-RH 61.168 % | B1_Soil-T 3.668 degC B1_Soil-RH 100.000 % B1_Wall-T 6.132 degC B1_Ext-T 4.708 degC B1_Int-T 18.570 degC B1_Inside-RH 100.000 % B1_Wall-RH 91.850 % | C1_Soil-T 4.573 degC C1_Soil-RH 100.000 % C1_Wall-T 6.979 degC C1_Ext-T 4.894 degC C1_Int-T 18.541 degC C1_Inside-RH 100.000 % C1_Wall-RH 95.907 % | 1 | T-room 19.480 degC RH-room 61.734 % T-room_sp 20.000 degC RH-room_sp 60.000 % T-environment 3.713 degC RH-environment 80.159 % T-environment_sp 3.000 degC RH-environment_sp 90.000 % | Remarks | |
| | A2_Soil-T 4.727 degC A2_Soil-RH 100.000 % A2_Wall-T 16.761 degC A2_Ext-T 6.816 degC A2_Int-T 18.030 degC A2_Inside-RH 62.591 % A2_Wall-RH 60.717 % | B2_Soil-T 4.382 degC B2_Soil-RH 100.000 % B2_Wall-T 8.047 degC B2_Ext-T 6.677 degC B2_Int-T 18.972 degC B2_Inside-RH 95.905 % B2_Wall-RH 95.897 % | C2_Soil-T 6.128 degC C2_Soil-RH 100.000 % C2_Ext-T 12.310 degC C2_Int-T 16.909 degC C2_Inside-RH 99.351 % | | Type: B-G Soil type: Clay Damproofing: Yes Alternative: Alt2 | | |
| | A3_Soil-T 5.466 degC A3_Soil-RH 100.000 % A3_Wall-T 16.985 degC A3_Ext-T 7.265 degC A3_Int-T 18.178 degC A3_Inside-RH 62.948 % A3_Wall-RH 66.282 % | B3_Soil-T 5.194 degC B3_Soil-RH 100.000 % B3_Wall-T 9.102 degC B3_Ext-T 7.093 degC B3_Int-T 18.840 degC B3_Inside-RH 99.500 % B3_Wall-RH 100.000 % | C3_Soil-T 5.547 degC C3_Soil-RH 100.000 % C3_Ext-T 17.493 degC C3_Int-T 16.228 degC C3_Inside-RH 97.875 % | | | | |
| | Yes | A | B | | | | |
| | | | | | | | |
| | | | | | | | |

* Measured pressure difference between Room Side & Environmental Side


Figure B-190: Average soil temperature of C2-Alt2

Insulated Concrete Masonry Below-grade Walls

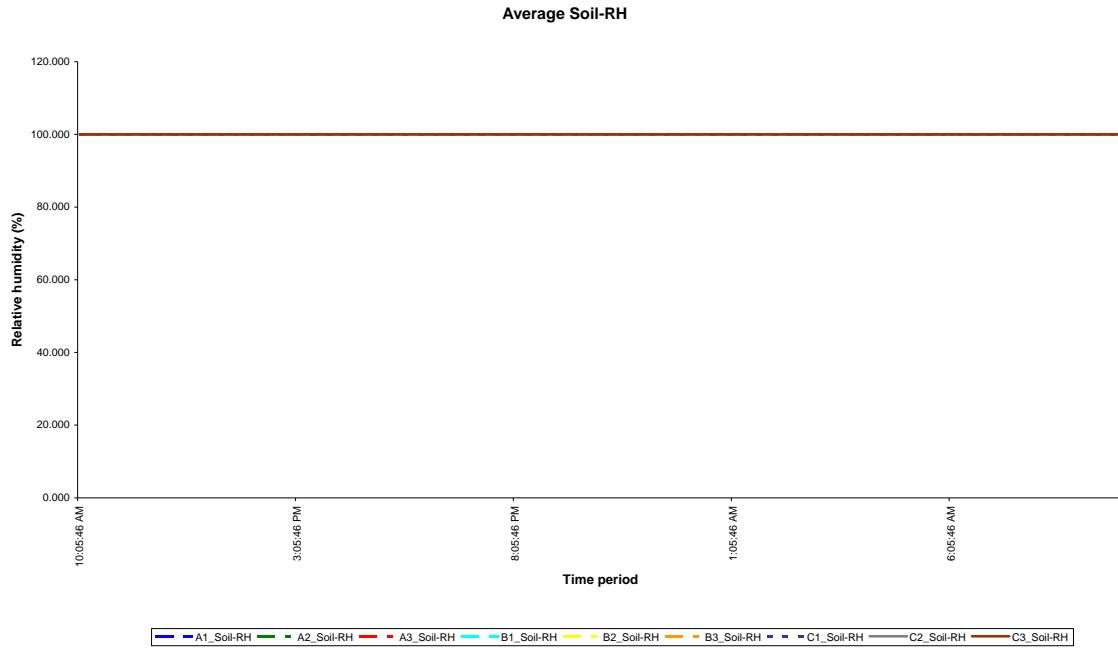


Figure B-191: Average soil relative humidity of C2-Alt2

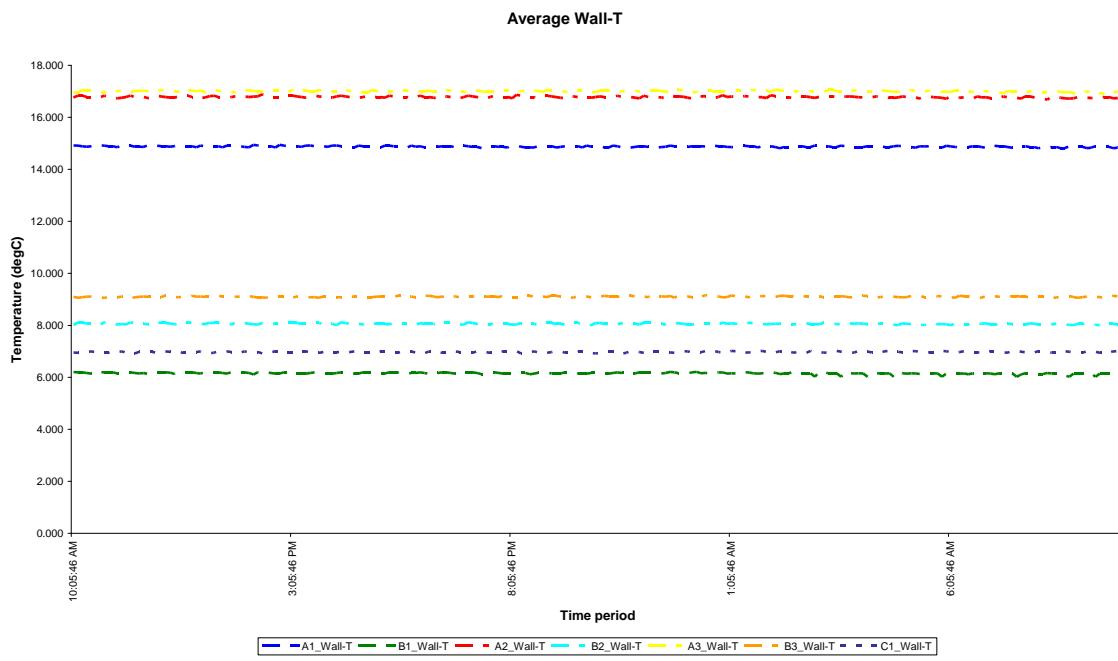


Figure B-192: Average wall temperature of C2-Alt2

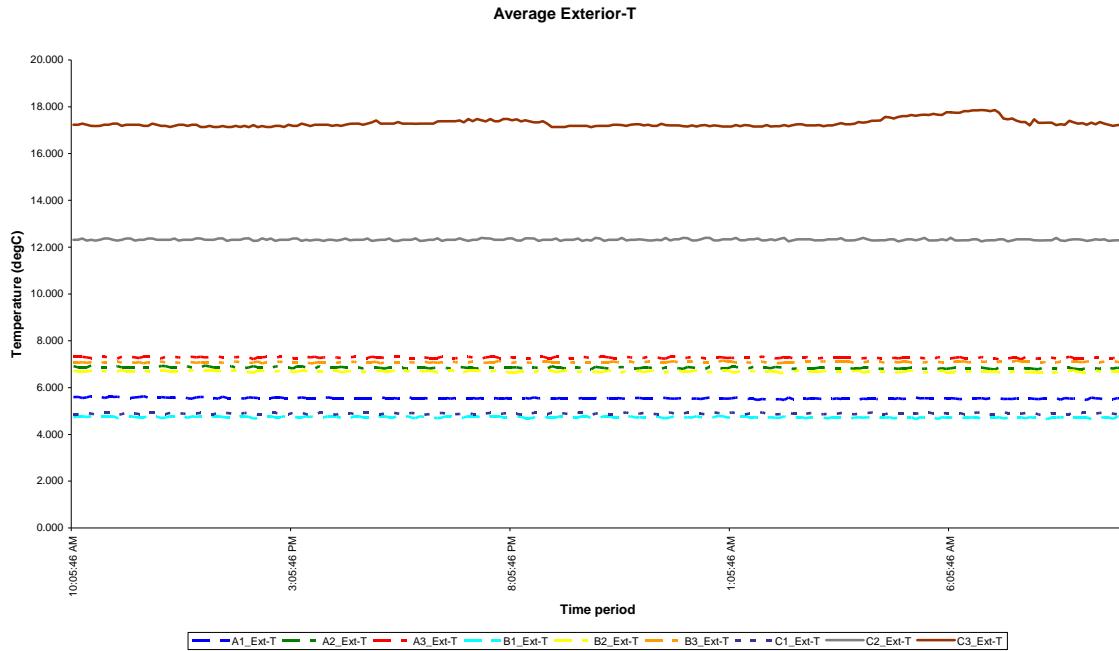


Figure B-193: Average exterior temperature of C2-Alt2

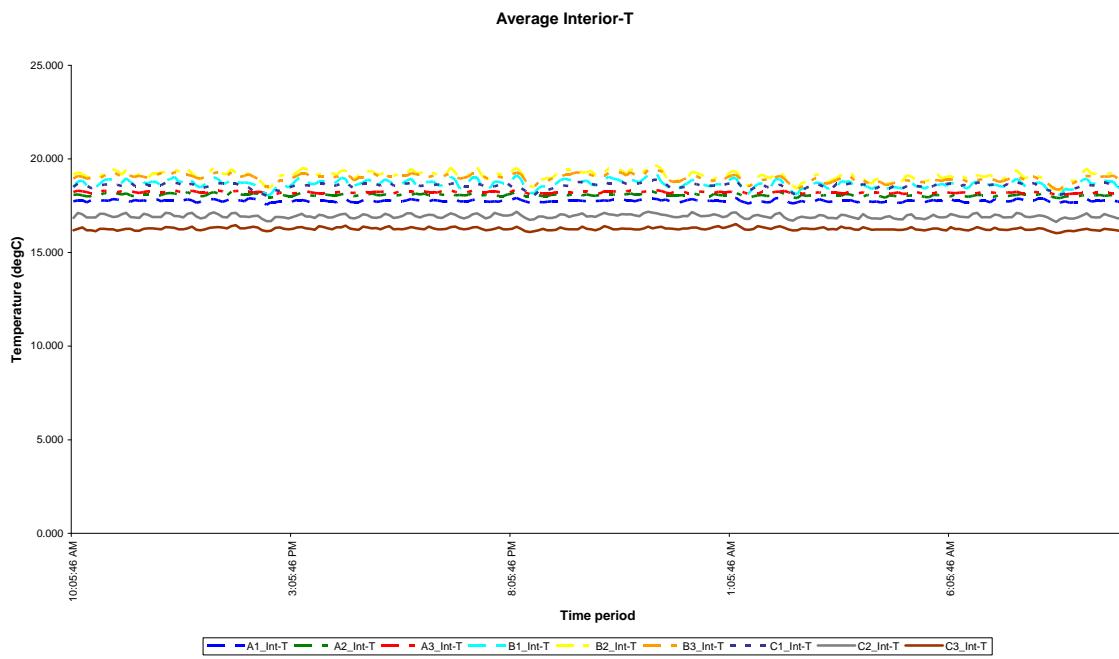


Figure B-194: Average interior temperature of C2-Alt2

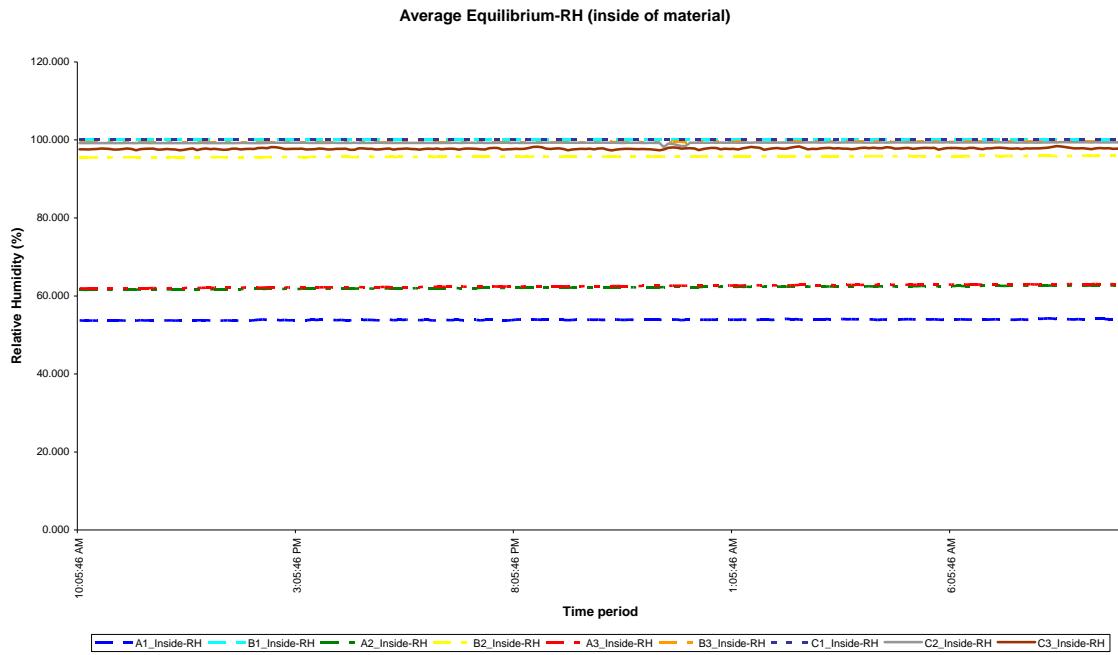


Figure B-195: Average equilibrium of relative humidity in a cavity of C2-Alt2

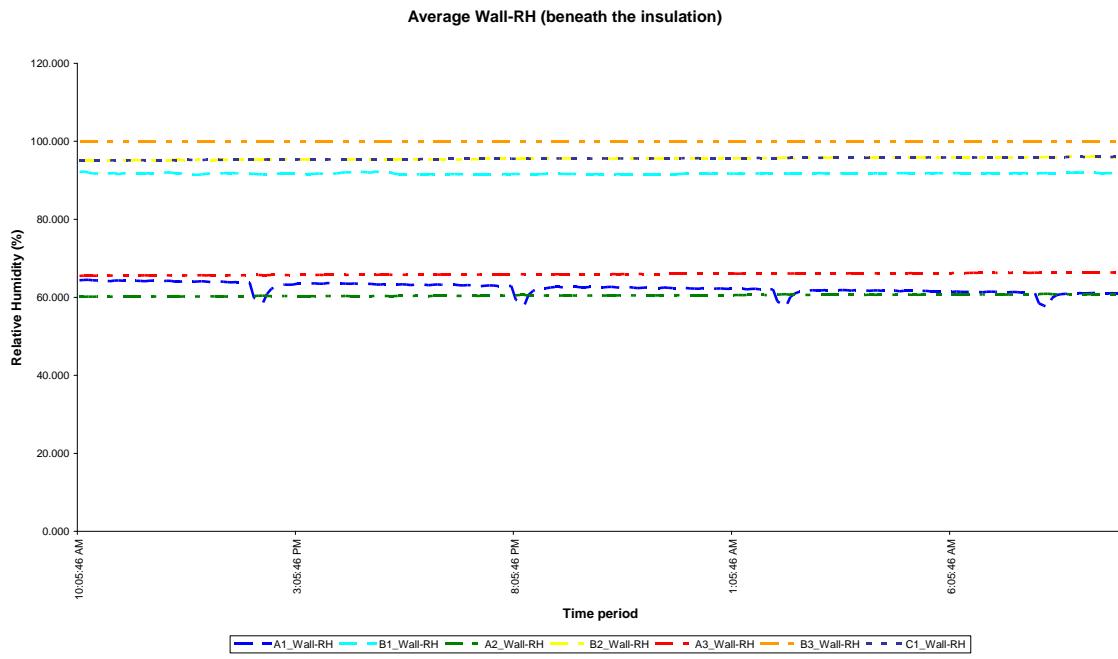


Figure B-196: Average wall relative humidity beneath the insulation of C2-Alt2

Insulated Concrete Masonry Below-grade Walls

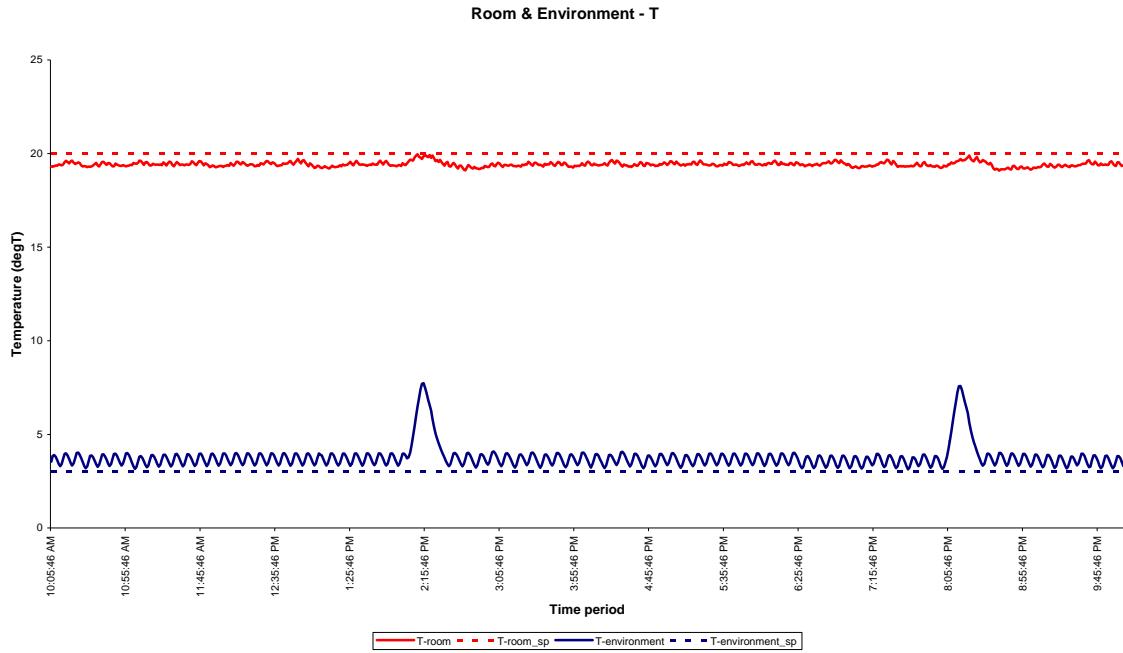


Figure B-197: Temperature of the room and environmental side during C2-Alt2

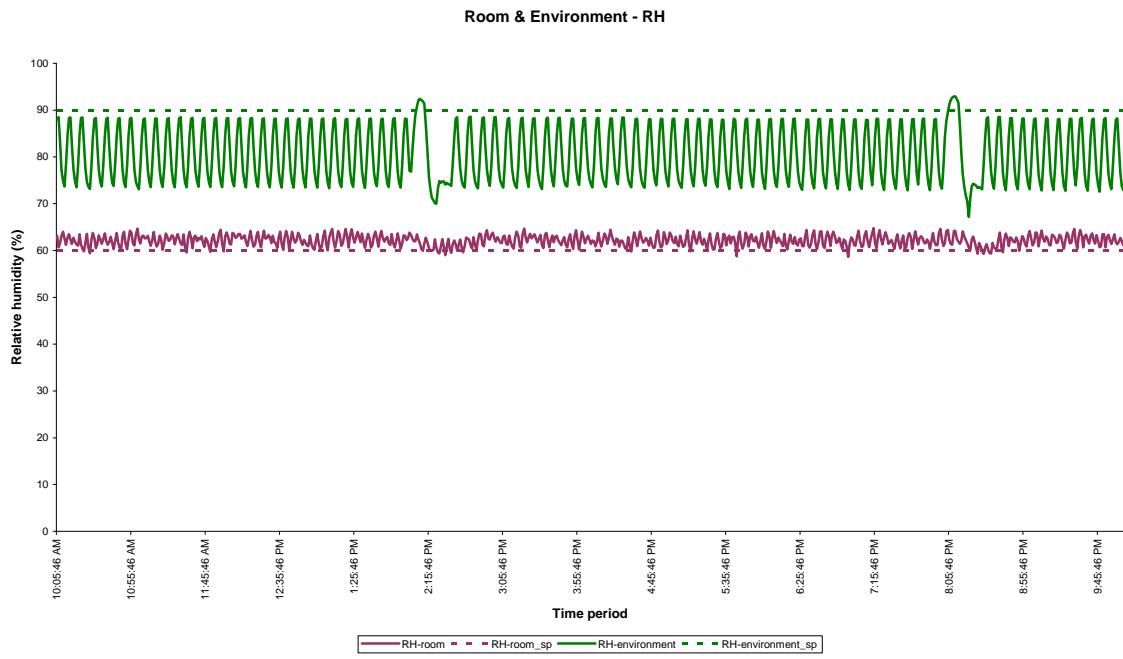


Figure B-198: Relative humidity of the room and environmental side during C2-Alt2

Test cycle: C2 – Alt3

Table B-23: Average data during the last 24 hours for each specimen of C2-Alt3

| Specimen Measurement Data | | | | | Control Loop Data | |
|---------------------------|--|---|---|------|-------------------|--|
| B-G | A | B | C | Clay | | |
| 1 | A1_Soil-T 18.856 degC A1_Soil-RH 100.000 % A1_Wall-T 18.466 degC A1_Ext-T 19.457 degC A1_Int-T 18.423 degC A1_Inside-RH 69.532 % A1_Wall-RH 84.105 % | B1_Soil-T 19.248 degC B1_Soil-RH 100.000 % B1_Wall-T 18.927 degC B1_Ext-T 18.929 degC B1_Int-T 17.777 degC B1_Inside-RH 100.000 % B1_Wall-RH 93.842 % | C1_Soil-T 20.455 degC C1_Soil-RH 100.000 % C1_Wall-T 20.238 degC C1_Ext-T 20.083 degC C1_Int-T 18.756 degC C1_Inside-RH 100.000 % C1_Wall-RH 88.136 % | 1 | | |
| 2 | A2_Soil-T 18.697 degC A2_Soil-RH 100.000 % A2_Wall-T 17.916 degC A2_Ext-T 18.870 degC A2_Int-T 17.640 degC A2_Inside-RH 67.590 % A2_Wall-RH 68.604 % | B2_Soil-T 18.629 degC B2_Soil-RH 100.000 % B2_Wall-T 18.271 degC B2_Ext-T 18.042 degC B2_Int-T 17.052 degC B2_Inside-RH 97.589 % B2_Wall-RH 96.712 % | C2_Soil-T 20.272 degC C2_Soil-RH 100.000 % C2_Ext-T 19.240 degC C2_Int-T 18.496 degC C2_Inside-RH 100.000 % | 2 | | |
| 3 | A3_Soil-T 18.703 degC A3_Soil-RH 100.000 % A3_Wall-T 17.967 degC A3_Ext-T 18.701 degC A3_Int-T 17.720 degC A3_Inside-RH 68.170 % A3_Wall-RH 72.393 % | B3_Soil-T 19.677 degC B3_Soil-RH 100.000 % B3_Wall-T 18.363 degC B3_Ext-T 18.267 degC B3_Int-T 17.606 degC B3_Inside-RH 99.893 % B3_Wall-RH 81.381 % | C3_Soil-T 19.946 degC C3_Soil-RH 100.000 % C3_Ext-T 22.684 degC C3_Int-T 18.566 degC C3_Inside-RH 100.000 % | 3 | | |
| Yes | A | B | C | | Alt3 | |

* Measured pressure difference between Room Side & Environmental Side

| Remarks |
|--------------------------------|
| Type: B-G |
| Soil type: Clay |
| Damproofing: Yes |
| Alternative: Alt3 |
| Legend |
| T - Temperature (degC) |
| RH - Relative Humidity (%) |
| SP - Setpoint (either T or RH) |

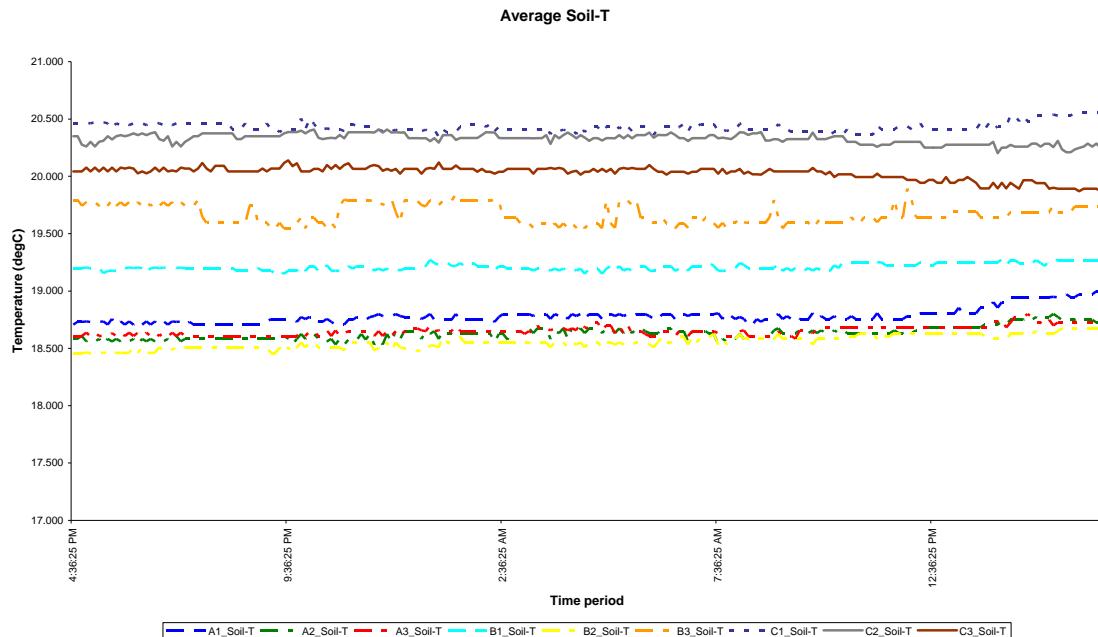


Figure B-199: Average soil temperature of C2-Alt3

Insulated Concrete Masonry Below-grade Walls

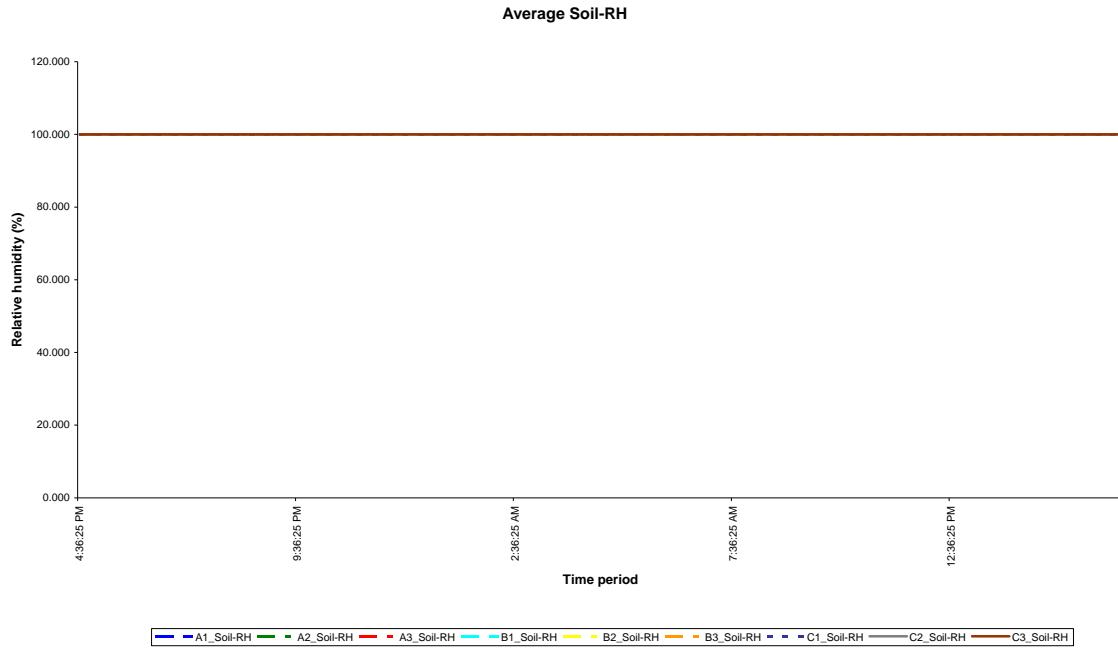


Figure B-200: Average soil relative humidity of C2-Alt3

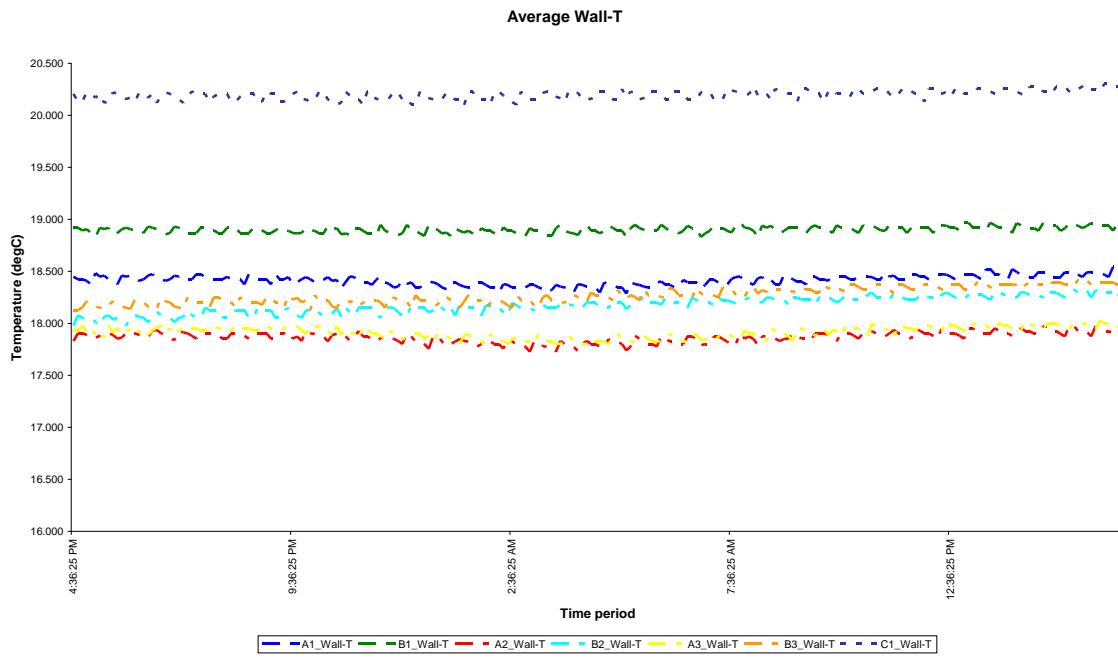


Figure B-201: Average wall temperature of C2-Alt3

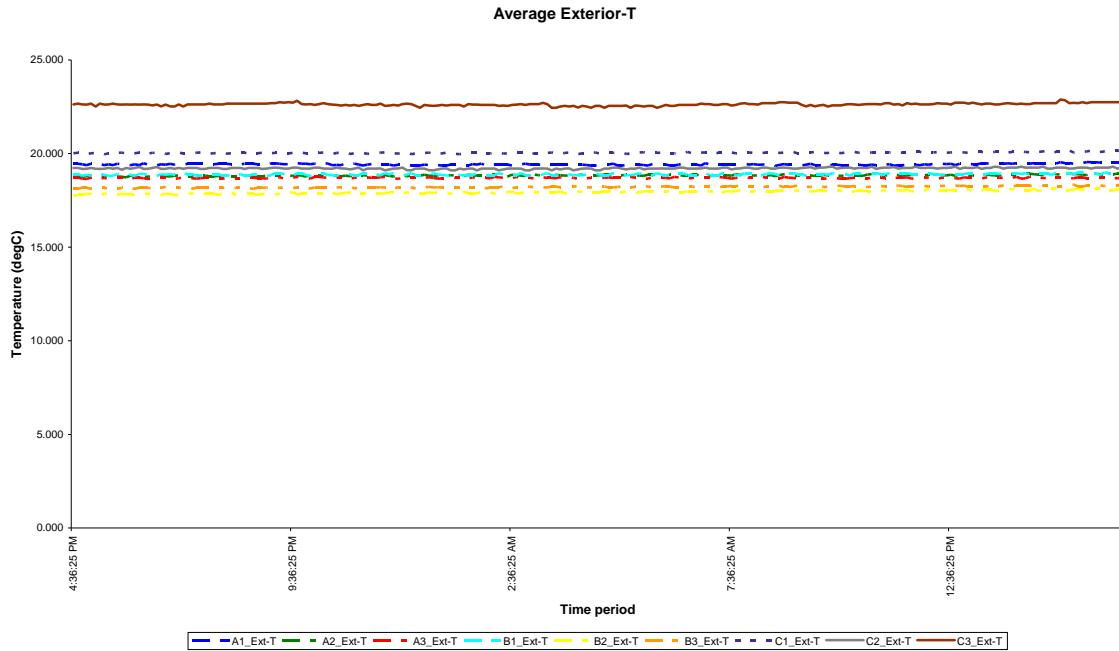


Figure B-202: Average exterior temperature of C2-Alt3

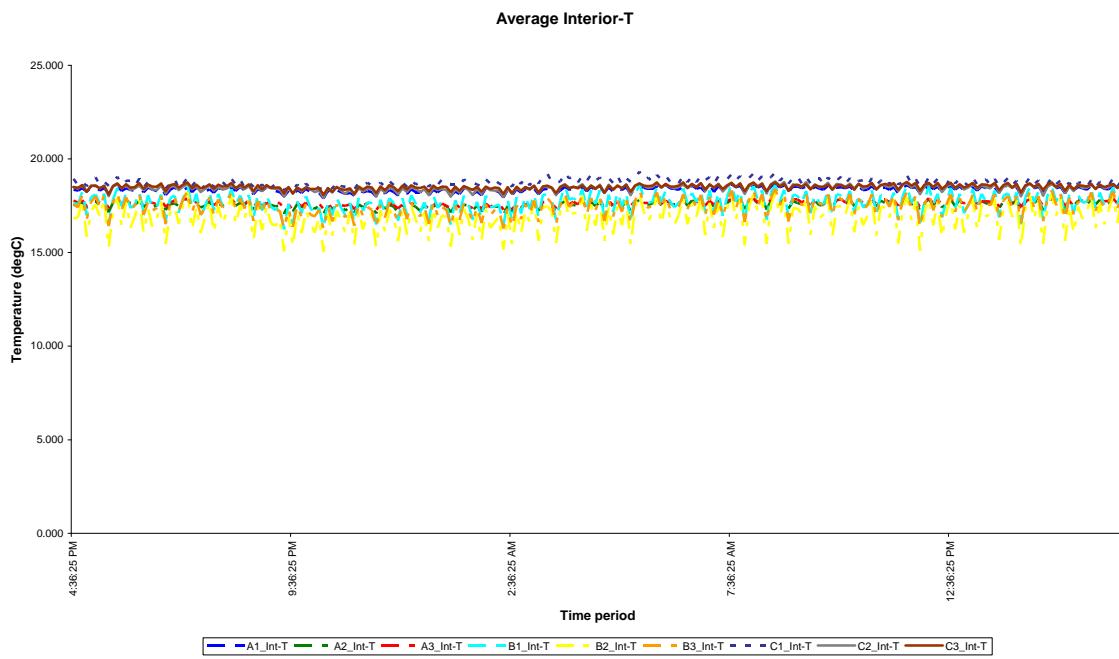


Figure B-203: Average interior temperature of C2-Alt3

Insulated Concrete Masonry Below-grade Walls

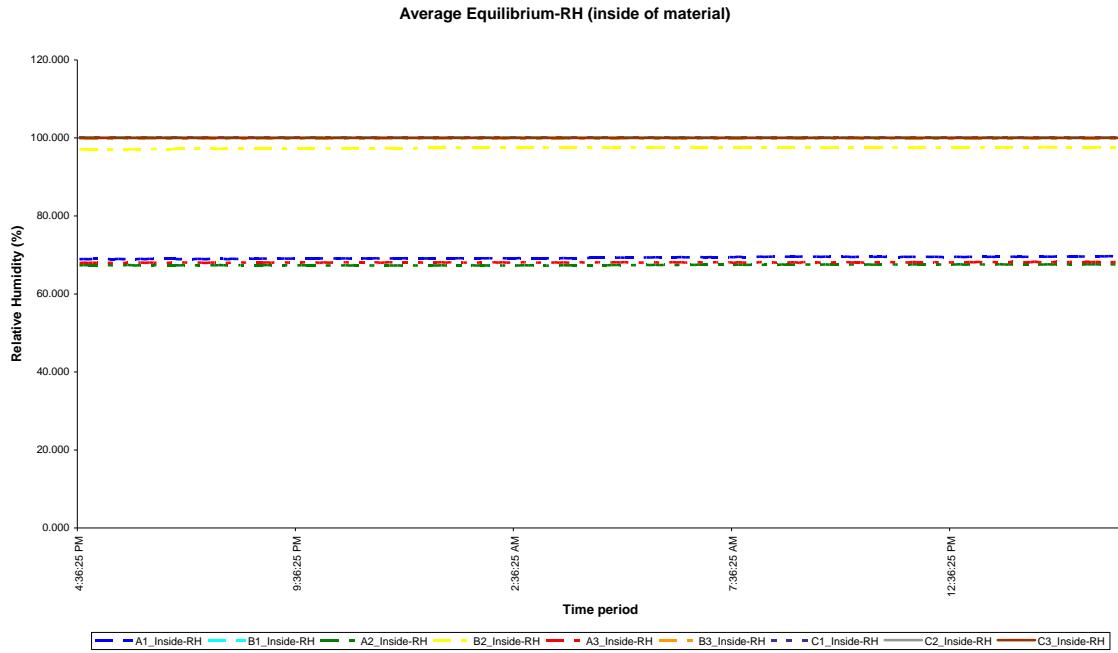


Figure B-204: Average equilibrium of relative humidity in a cavity of C2-Alt3

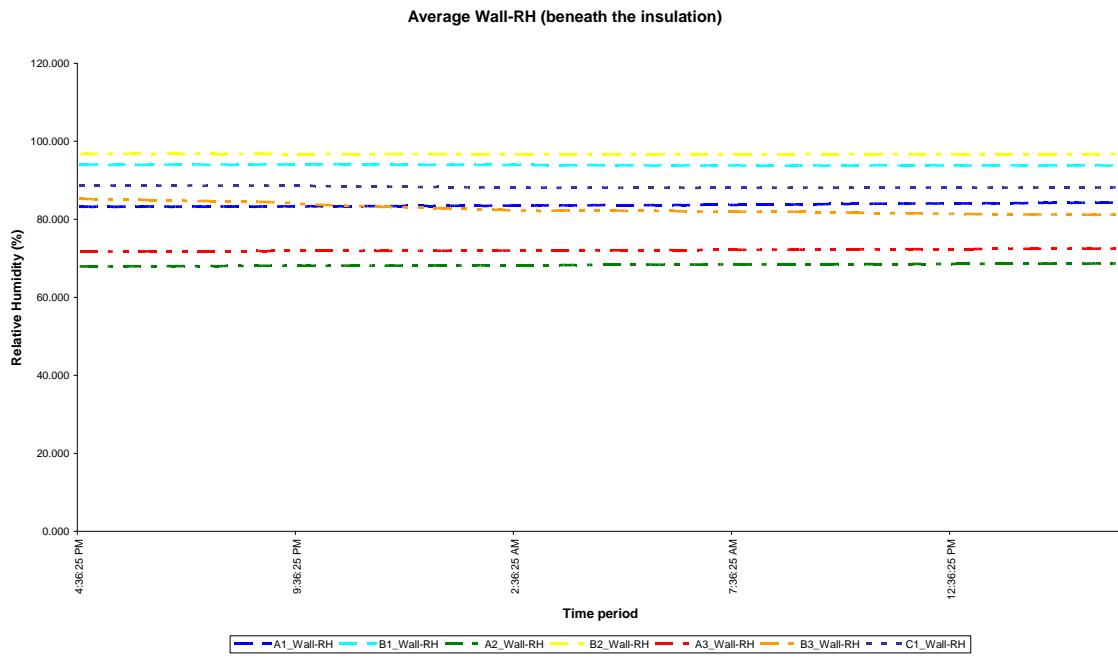


Figure B-205: Average wall relative humidity beneath the insulation of C2-Alt3

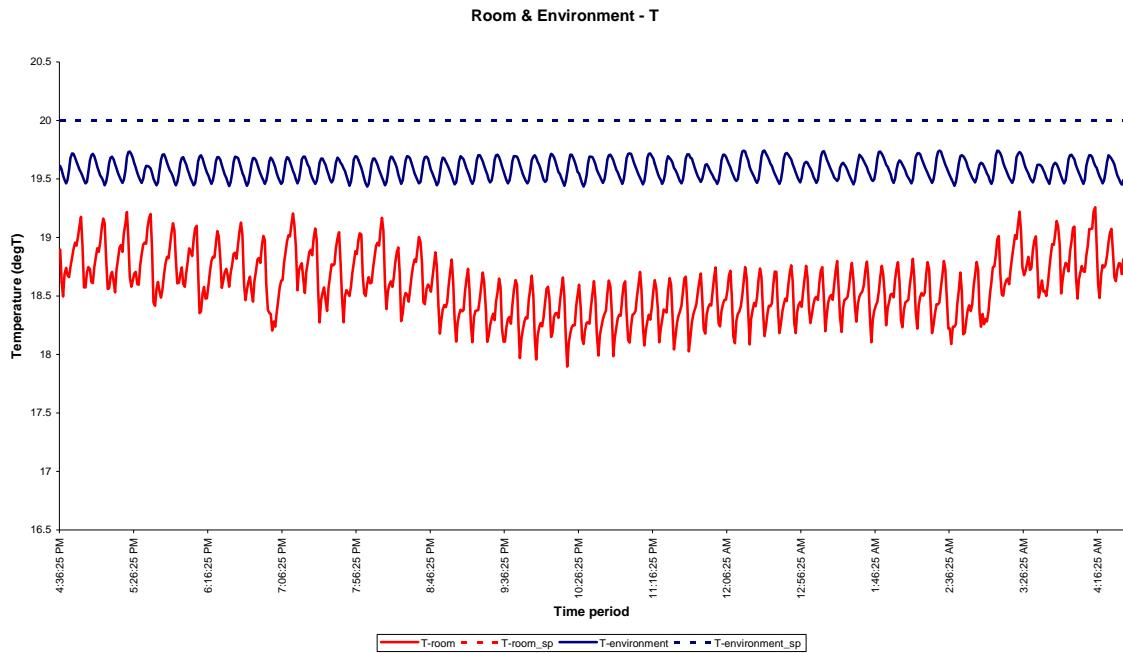


Figure B-206: Temperature of the room and environmental side during C2-Alt3

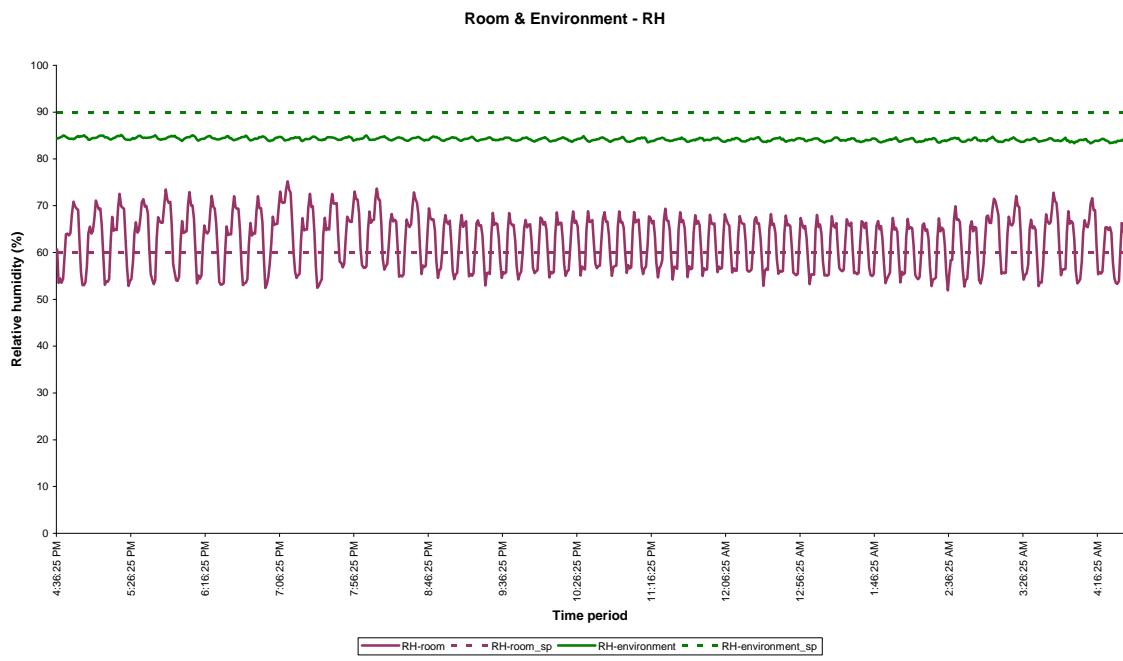


Figure B-207: Relative humidity of the room and environmental side during C2-Alt3

Test cycle: C2 – Alt4

Table B-24: Average data during the last 24 hours for each specimen of C2-Alt4

| Specimen Measurement Data | | | | | Control Loop Data | | |
|---------------------------|--|---|---|------|--|---------|--|
| B-G | A | B | C | Clay | Environmental / Room Side | | |
| 1 | A1_Soil-T 18.861 degC A1_Soil-RH 100.000 % A1_Wall-T 18.607 degC A1_Ext-T 19.952 degC A1_Int-T 18.485 degC A1_Inside-RH 67.821 % A1_Wall-RH 84.350 % | B1_Soil-T 19.355 degC B1_Soil-RH 100.000 % B1_Wall-T 19.215 degC B1_Ext-T 19.174 degC B1_Int-T 17.965 degC B1_Inside-RH 100.000 % B1_Wall-RH 88.876 % | C1_Soil-T 20.604 degC C1_Soil-RH 100.000 % C1_Wall-T 20.322 degC C1_Ext-T 20.171 degC C1_Int-T 19.153 degC C1_Inside-RH 100.000 % C1_Wall-RH 81.855 % | 1 | T-room 19.216 degC RH-room 42.715 % T-room_sp 20.000 degC RH-room_sp 30.000 % T-environment 19.528 degC RH-environment 74.025 % T-environment_sp 20.000 degC RH-environment_sp 90.000 % | Remarks | |
| | A2_Soil-T 18.740 degC A2_Soil-RH 100.000 % A2_Wall-T 17.983 degC A2_Ext-T 19.147 degC A2_Int-T 17.624 degC A2_Inside-RH 62.601 % A2_Wall-RH 68.342 % | B2_Soil-T 18.808 degC B2_Soil-RH 100.000 % B2_Wall-T 18.728 degC B2_Ext-T 18.501 degC B2_Int-T 17.005 degC B2_Inside-RH 97.013 % B2_Wall-RH 86.105 % | C2_Soil-T 20.458 degC C2_Soil-RH 100.000 % C2_Ext-T 19.549 degC C2_Int-T 18.855 degC C2_Inside-RH 99.482 % | | Type: B-G Soil type: Clay Damproofing: Yes Alternative: Alt4 | | |
| | A3_Soil-T 18.746 degC A3_Soil-RH 100.000 % A3_Wall-T 17.826 degC A3_Ext-T 18.774 degC A3_Int-T 17.469 degC A3_Inside-RH 62.177 % A3_Wall-RH 71.583 % | B3_Soil-T 19.366 degC B3_Soil-RH 100.000 % B3_Wall-T 18.628 degC B3_Ext-T 18.547 degC B3_Int-T 16.977 degC B3_Inside-RH 92.851 % B3_Wall-RH 55.787 % | C3_Soil-T 20.104 degC C3_Soil-RH 100.000 % C3_Ext-T 21.605 degC C3_Int-T 18.482 degC C3_Inside-RH 99.656 % | | | | |
| | Yes | A | B | | | | |
| | | | | | | | |
| | | | | | | | |

* Measured pressure difference between Room Side & Environmental Side

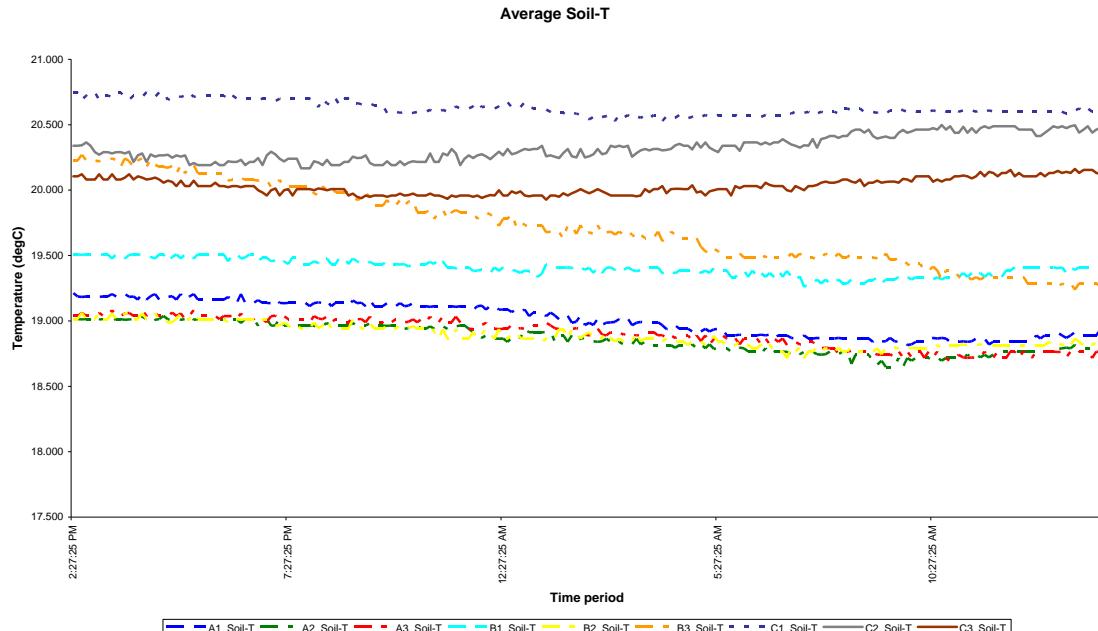


Figure B-208: Average soil temperature of C2-Alt4

Insulated Concrete Masonry Below-grade Walls

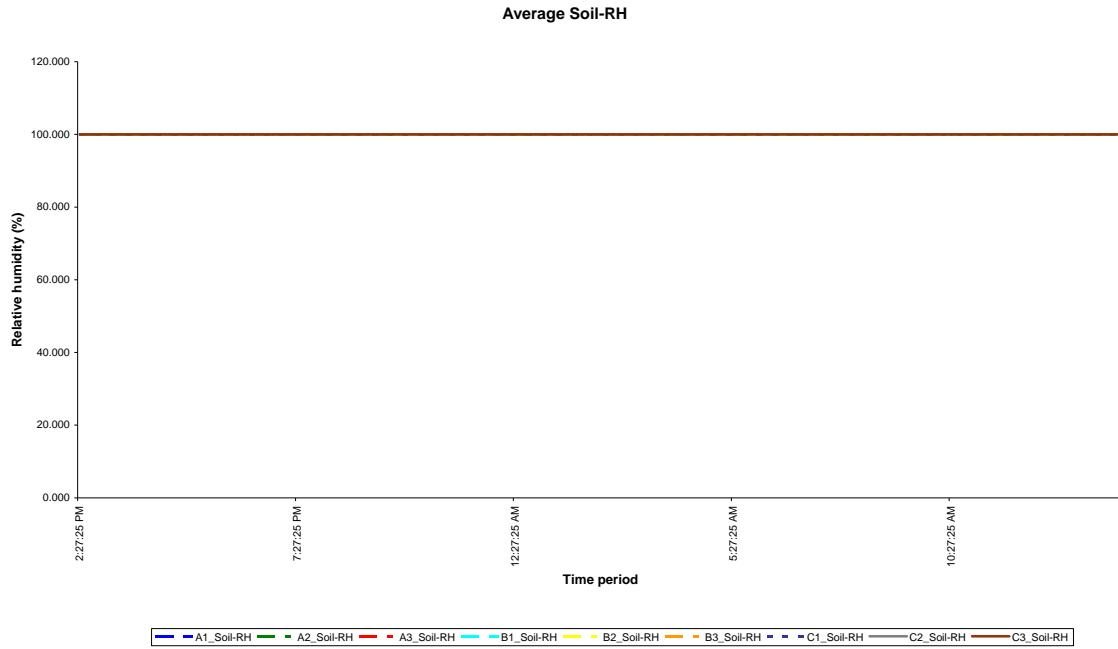


Figure B-209: Average soil relative humidity of C2-Alt4

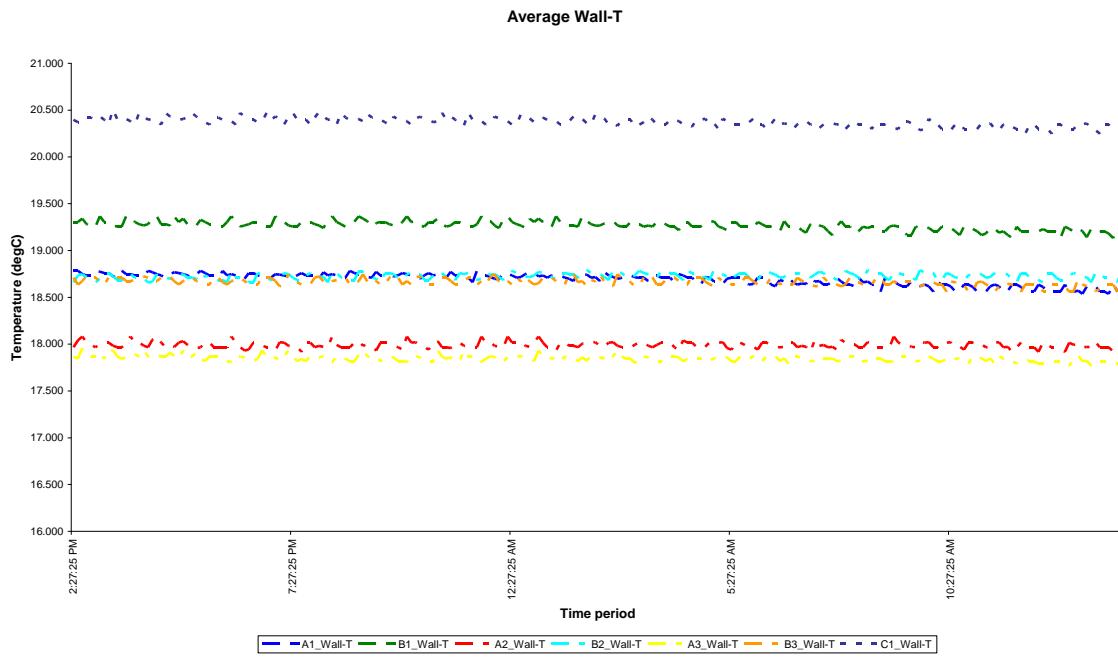


Figure B-210: Average wall temperature of C2-Alt4

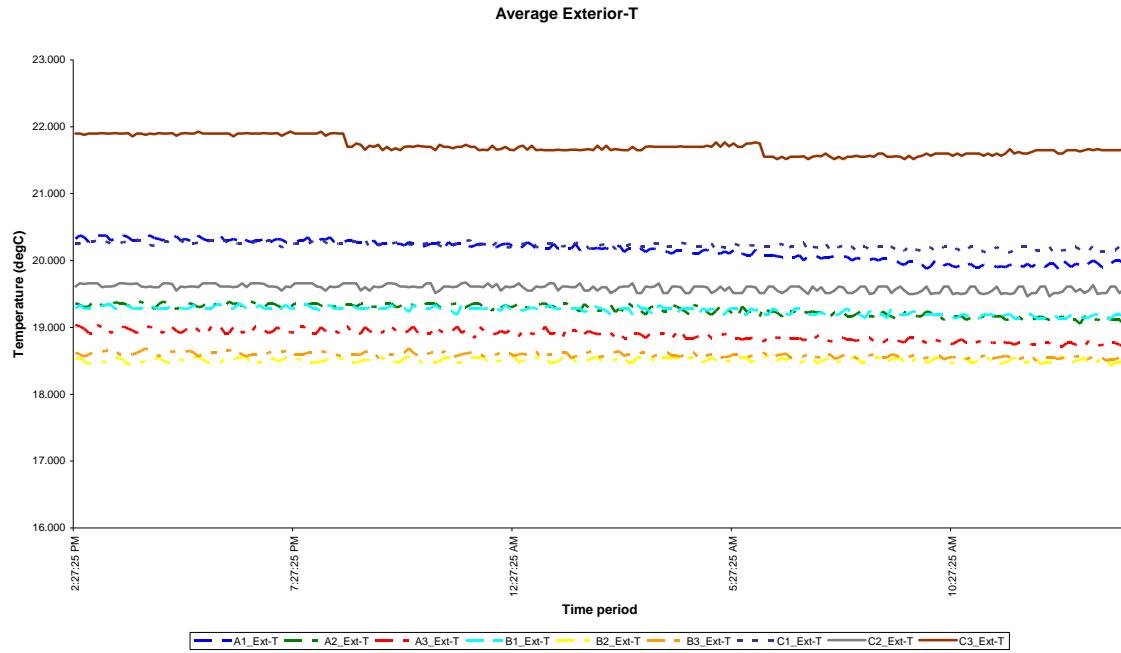


Figure B-211: Average exterior temperature of C2-Alt4

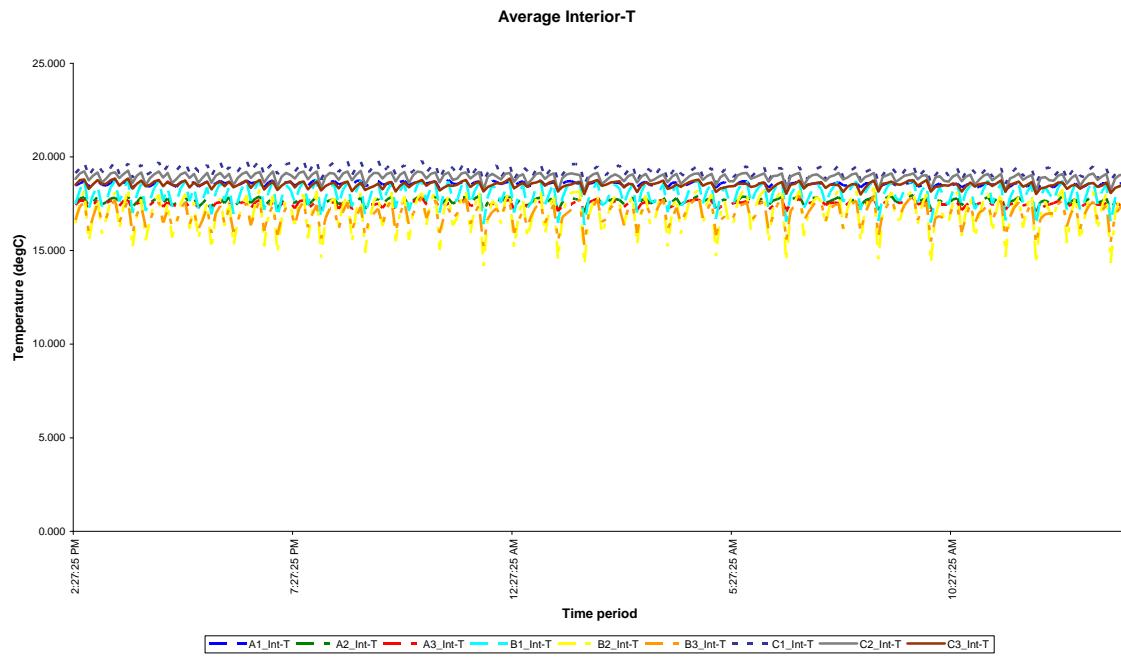


Figure B-212: Average interior temperature of C2-Alt4

Insulated Concrete Masonry Below-grade Walls

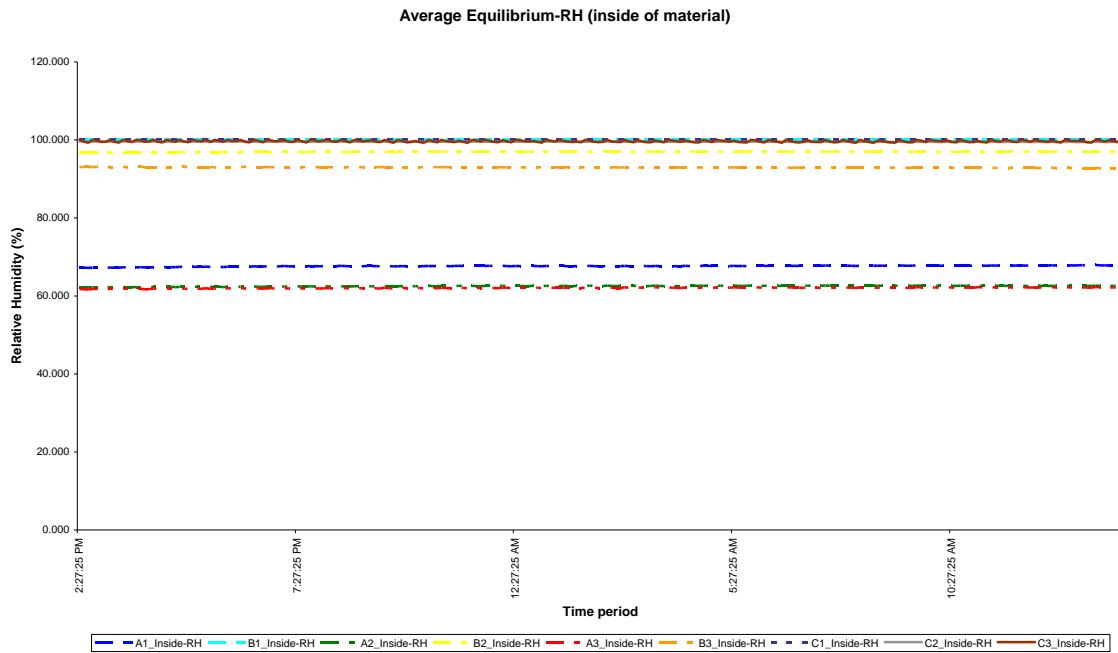


Figure B-213: Average equilibrium of relative humidity in a cavity of C2-Alt4

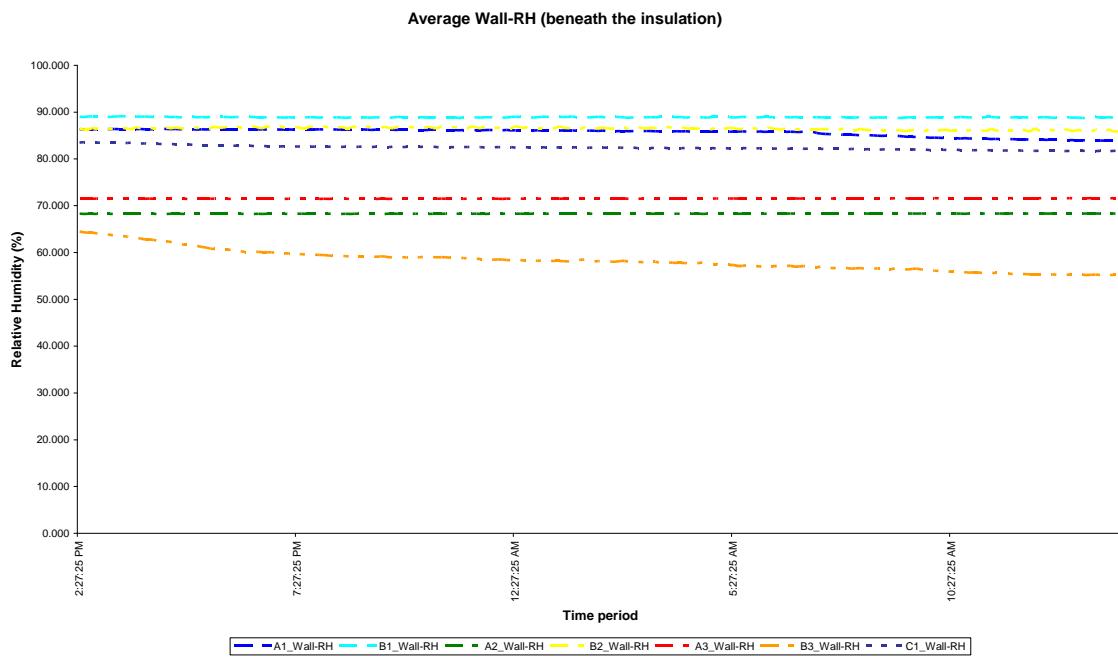


Figure B-214: Average wall relative humidity beneath the insulation of C2-Alt4

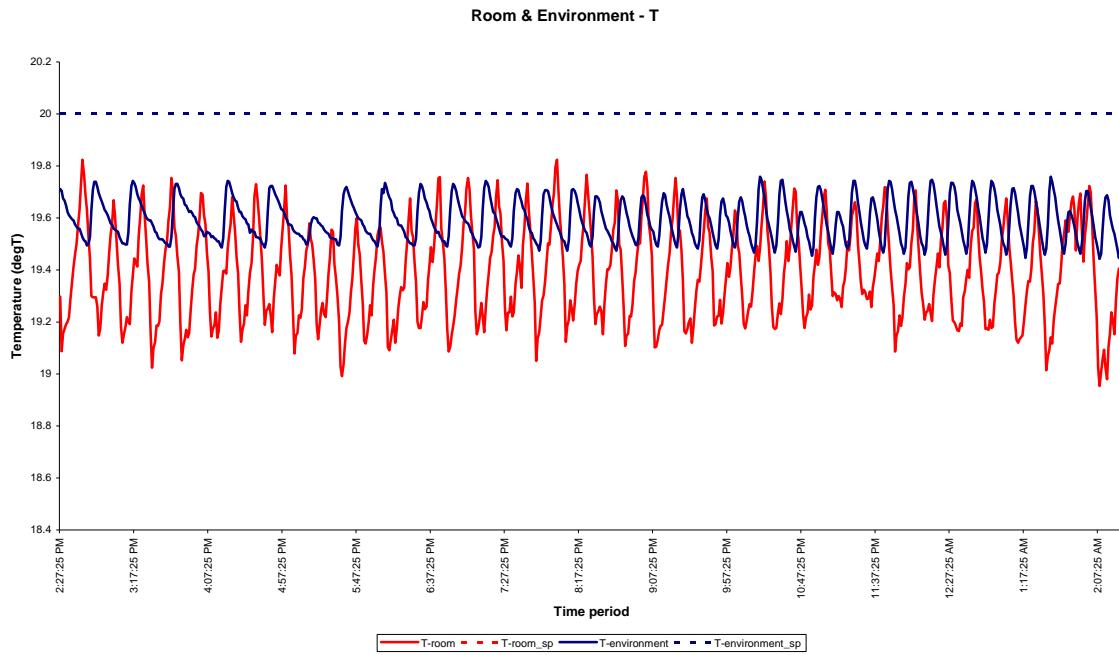


Figure B-215: Temperature of the room and environmental side during C2-Alt4

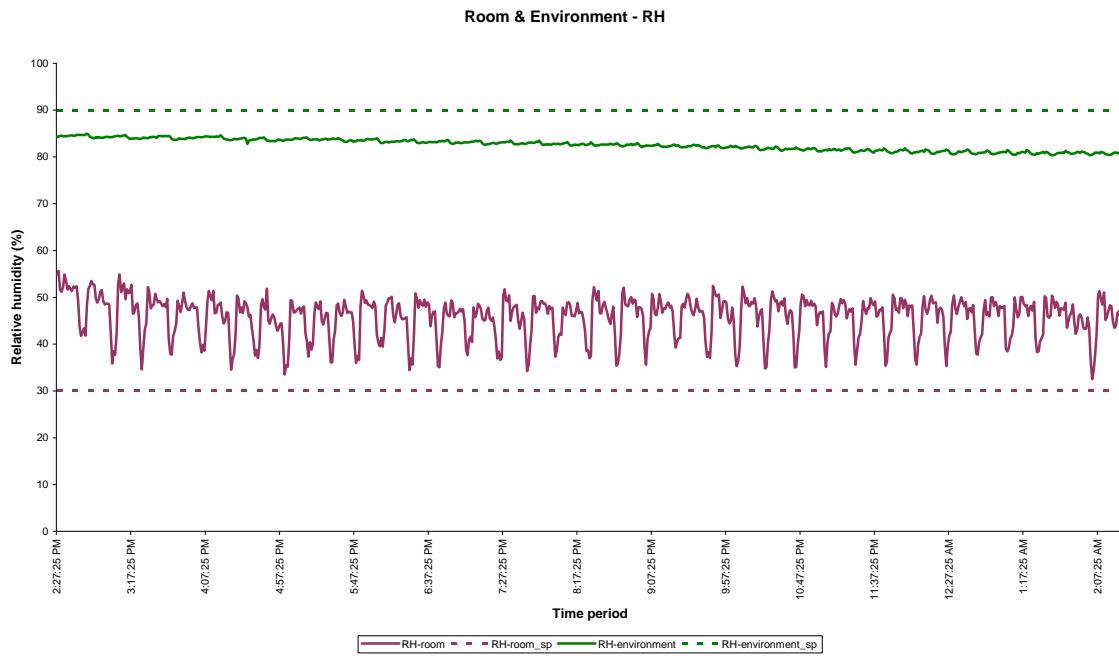
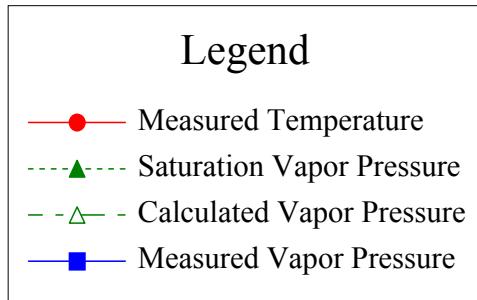


Figure B-216: Relative humidity of the room and environmental side during C2-Alt4

Appendix C – Measurement evaluations

The measured data are graphically summarized in appendix C. Wall fragments depicted, using dew-point method, are shown below. The legend of measured and depicted values is following:



Wall fragments evaluation is shown according to the following order:

1. Measurement series: S1
 - 1.1. Test cycle: S1-Alt1
 - 1.2. Test cycle: S1-Alt2
 - 1.3. Test cycle: S1-Alt3
 - 1.4. Test cycle: S1-Alt4
 - 1.5. Test cycle: S1-Alt5
 - 1.6. Test cycle: S1-Alt6
 - 1.7. Test cycle: S1-Alt7
 - 1.8. Test cycle: S1-Alt8
2. Measurement series: S2
 - 2.1. Test cycle: S2-Alt1
 - 2.2. Test cycle: S2-Alt2
 - 2.3. Test cycle: S2-Alt3
 - 2.4. Test cycle: S2-Alt4
3. Measurement series: C1
 - 3.1. Test cycle: C1-Alt1
 - 3.2. Test cycle: C1-Alt2
 - 3.3. Test cycle: C1-Alt3
 - 3.4. Test cycle: C1-Alt4
 - 3.5. Test cycle: C1-Alt5
 - 3.6. Test cycle: C1-Alt6
 - 3.7. Test cycle: C1-Alt7
 - 3.8. Test cycle: C1-Alt8
4. Measurement series: C2
 - 4.1. Test cycle: C2-Alt1
 - 4.2. Test cycle: C2-Alt2
 - 4.3. Test cycle: C2-Alt3
 - 4.4. Test cycle: C2-Alt4

Measurement series: **S1**

Test cycle: **S1 – Alt1**

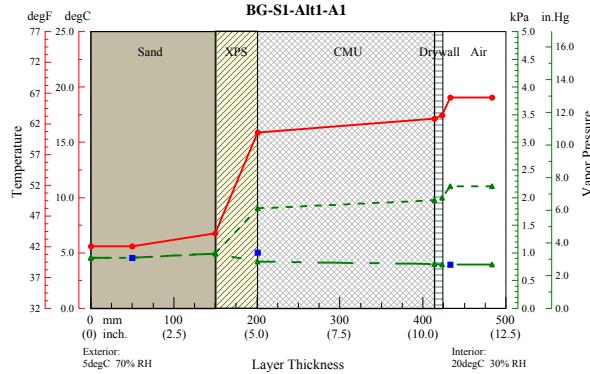


Figure C-1: Wall diagram of S1-Alt1-A1

Measurement series: **C1**

Test cycle: **C1 – Alt1**

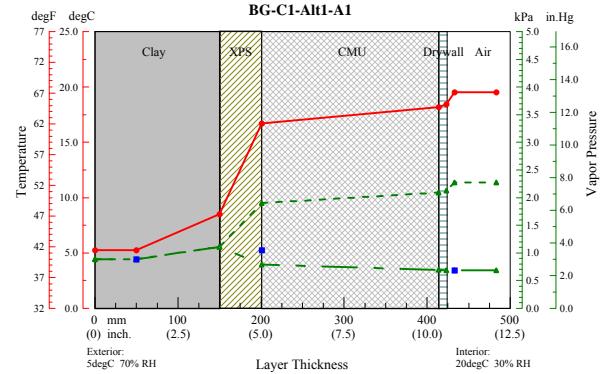


Figure C-2: Wall diagram of C1-Alt1-A1

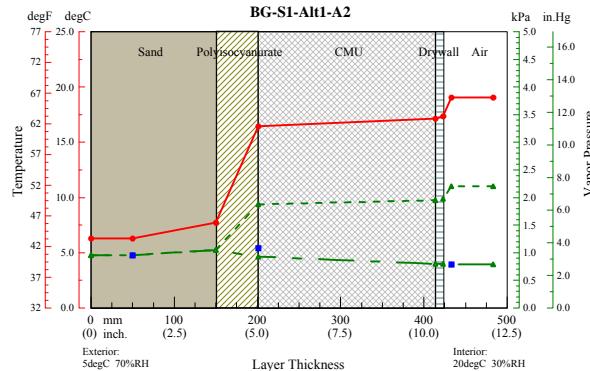


Figure C-3: Wall diagram of S1-Alt1-A2

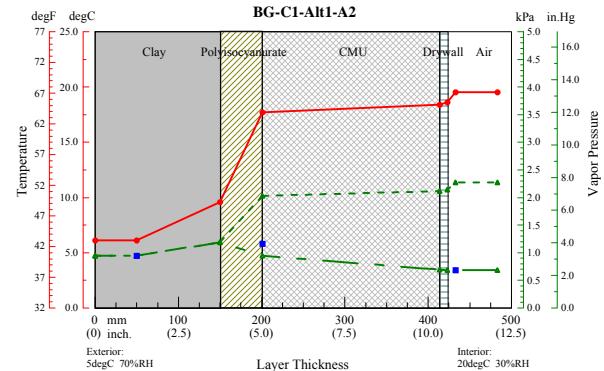


Figure C-4: Wall diagram of C1-Alt1-A2

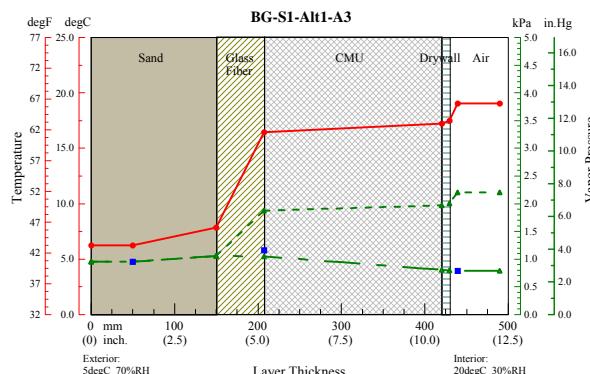


Figure C-5: Wall diagram of S1-Alt1-A3

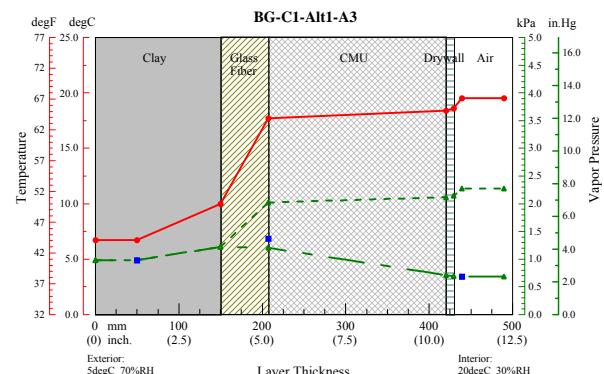


Figure C-6: Wall diagram of C1-Alt1-A3

Test cycle: **S1 – Alt1 (continued)**

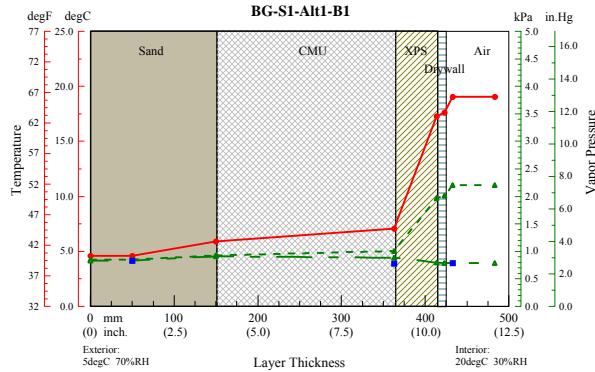


Figure C-7: Wall diagram of S1-Alt1-B1

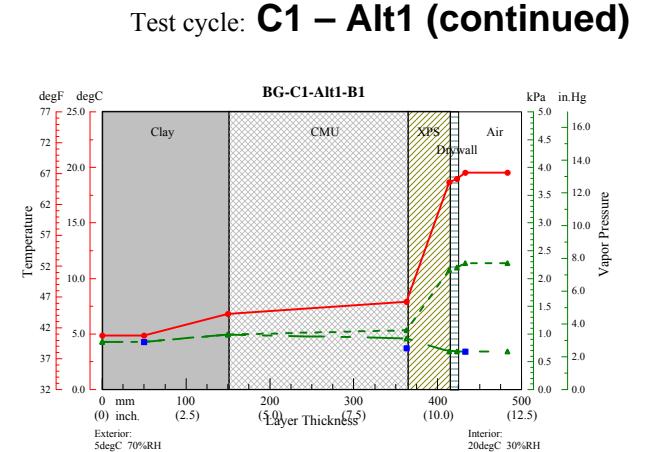


Figure C-8: Wall diagram of C1-Alt1-B1

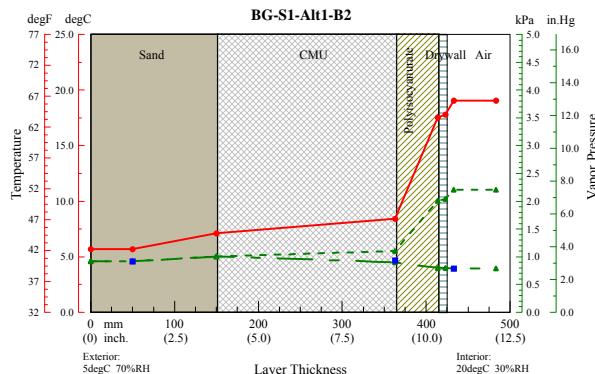


Figure C-9: Wall diagram of S1-Alt1-B2

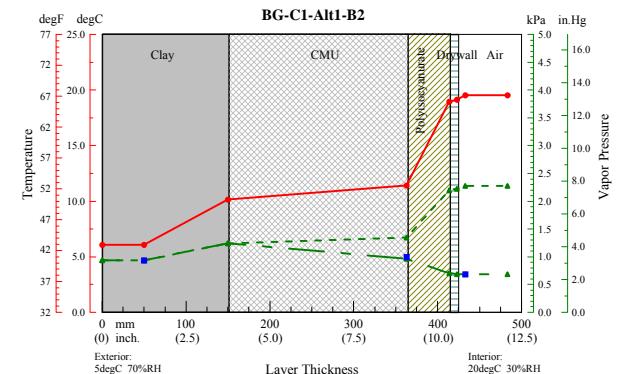


Figure C-10: Wall diagram of C1-Alt1-B2

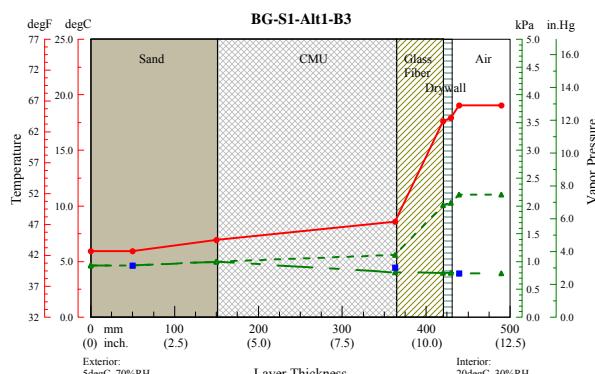


Figure C-11: Wall diagram of S1-Alt1-B3

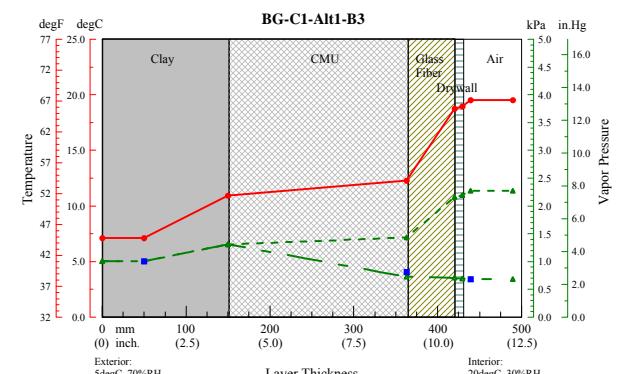


Figure C-12: Wall diagram of C1-Alt1-B3

Test cycle: **S1 – Alt1 (continued)**

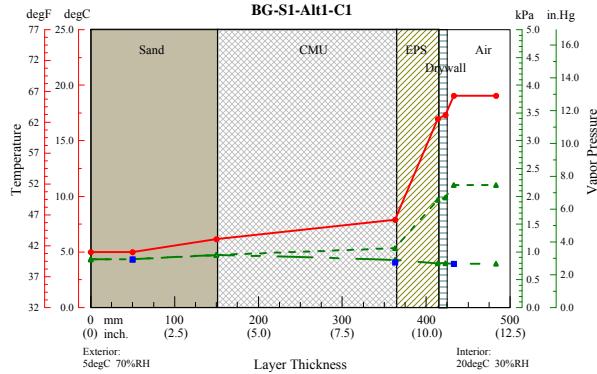


Figure C-13: Wall diagram of S1-Alt1-C1

Test cycle: **C1 – Alt1 (continued)**

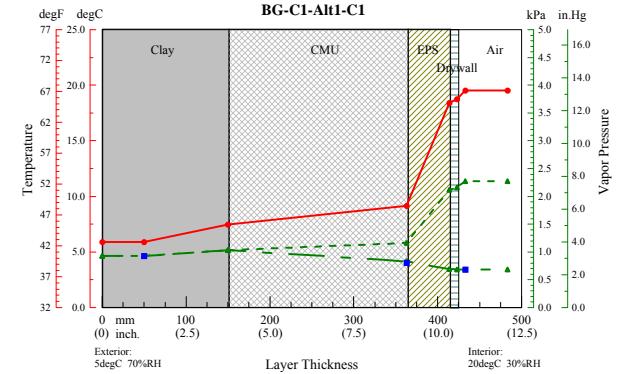


Figure C-14: Wall diagram of C1-Alt1-C1

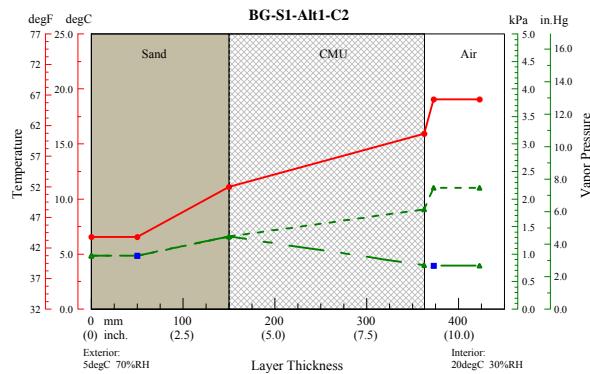


Figure C-15: Wall diagram of S1-Alt1-C2

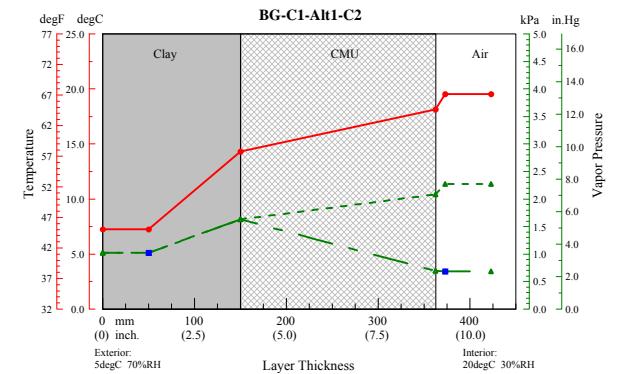


Figure C-16: Wall diagram of C1-Alt1-C2

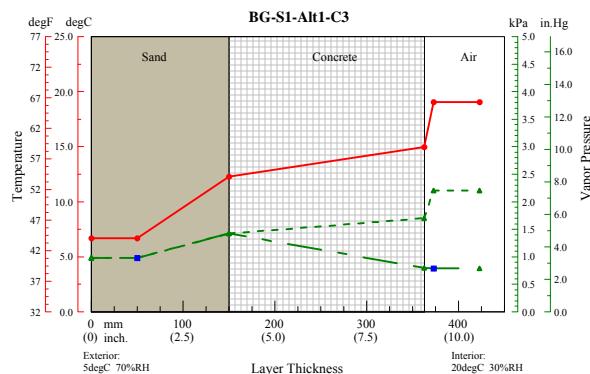


Figure C-17: Wall diagram of S1-Alt1-C3

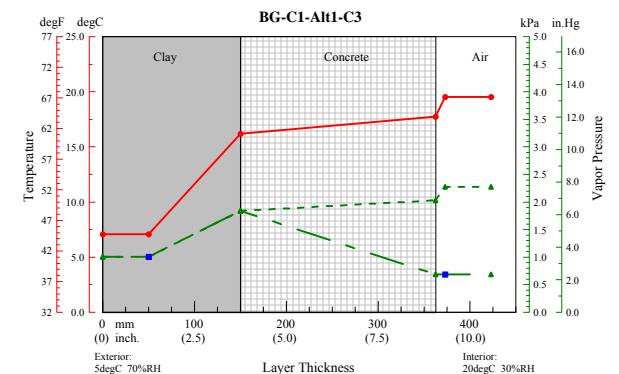


Figure C-18: Wall diagram of C1-Alt1-C3

Test cycle: **S1 – Alt2**

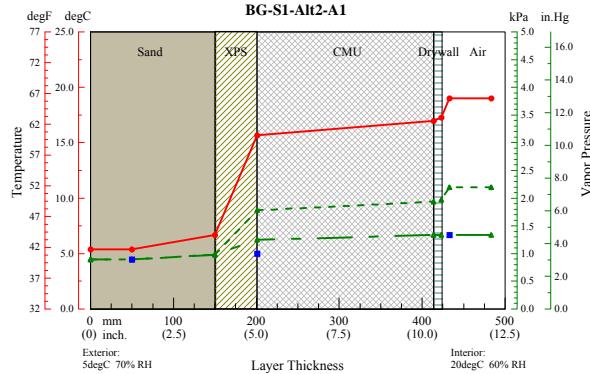


Figure C-19: Wall diagram of S1-Alt2-A1

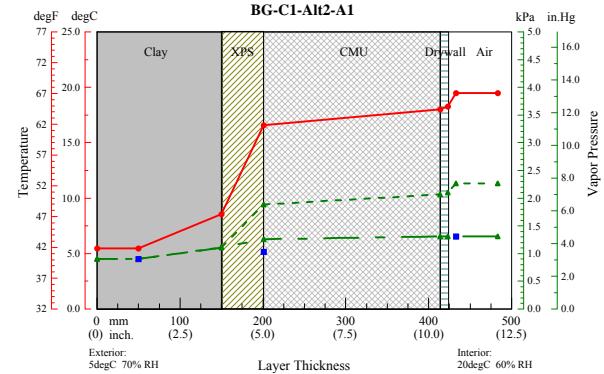


Figure C-20: Wall diagram of C1-Alt2-A1

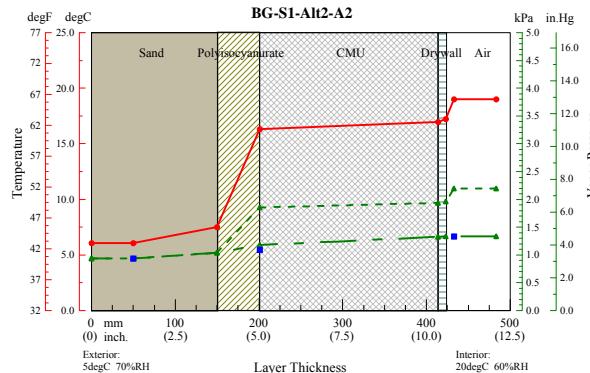


Figure C-21: Wall diagram of S1-Alt2-A2

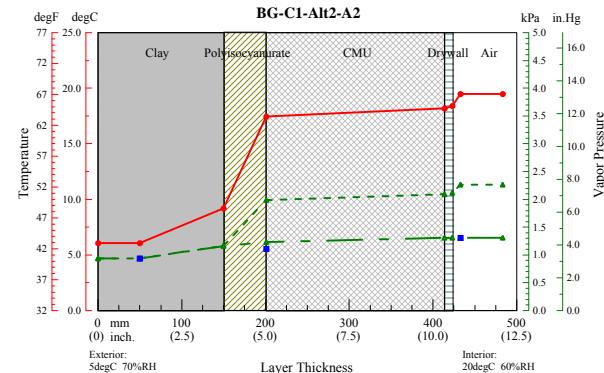


Figure C-22: Wall diagram of C1-Alt2-A2

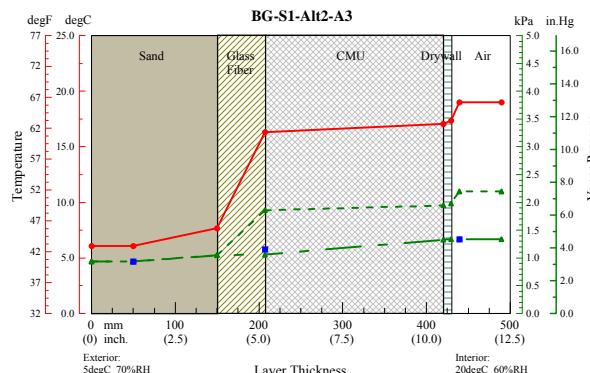


Figure C-23: Wall diagram of S1-Alt2-A3

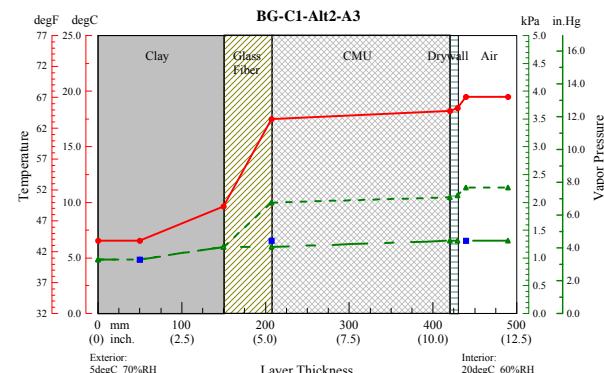


Figure C-24: Wall diagram of C1-Alt2-A3

Test cycle: **S1 – Alt2 (continued)**

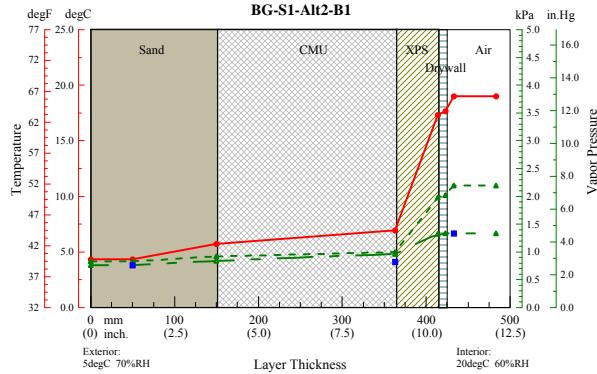


Figure C-25: Wall diagram of S1-Alt2-B1

Test cycle: **C1 – Alt2 (continued)**

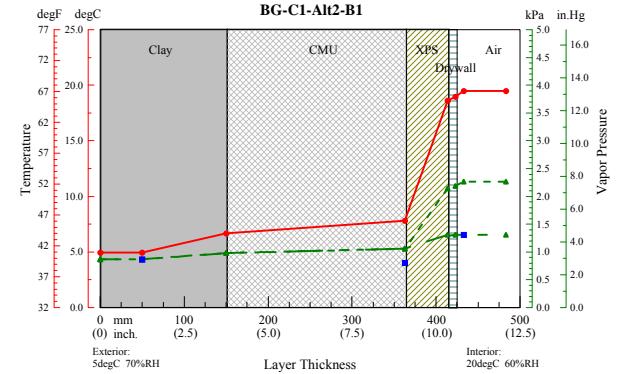


Figure C-26: Wall diagram of C1-Alt2-B1

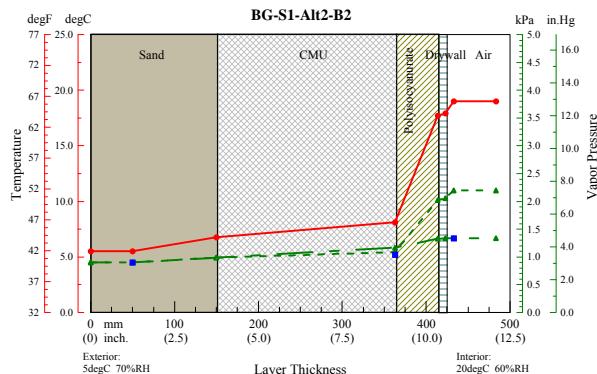


Figure C-27: Wall diagram of S1-Alt2-B2

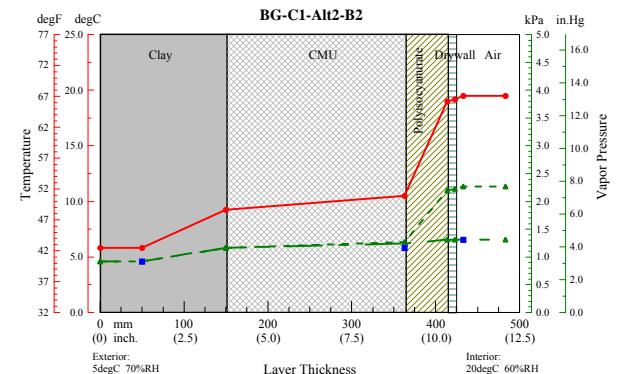


Figure C-28: Wall diagram of C1-Alt2-B2

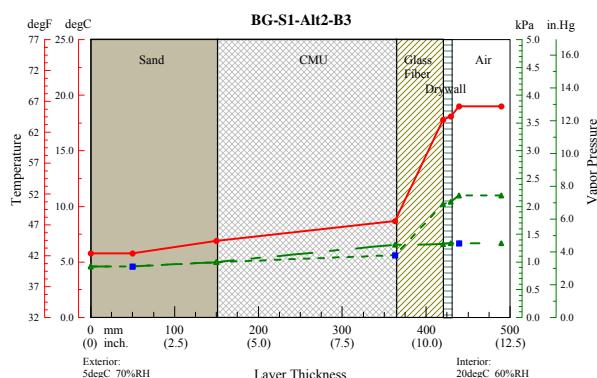


Figure C-29: Wall diagram of S1-Alt2-B3

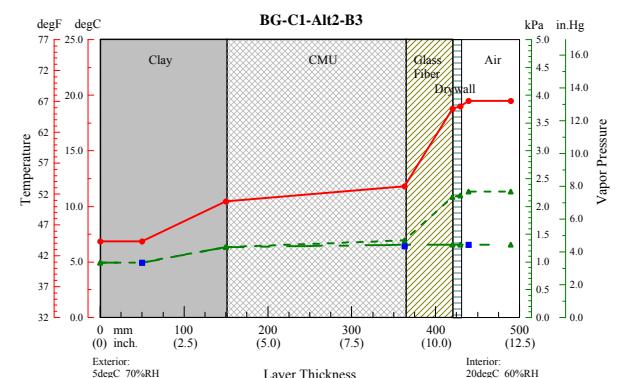


Figure C-30: Wall diagram of C1-Alt2-B3

Test cycle: **S1 – Alt2 (continued)**

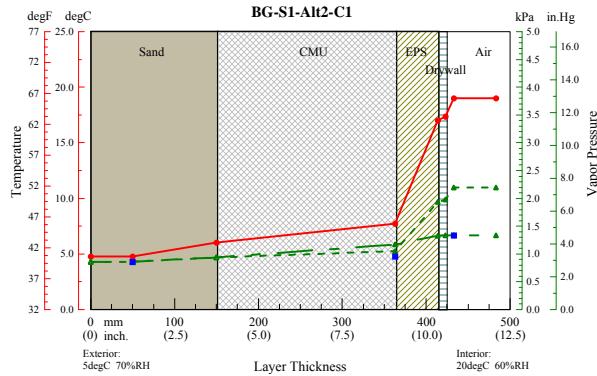


Figure C-31: Wall diagram of S1-Alt2-C1

Test cycle: **C1 – Alt2 (continued)**

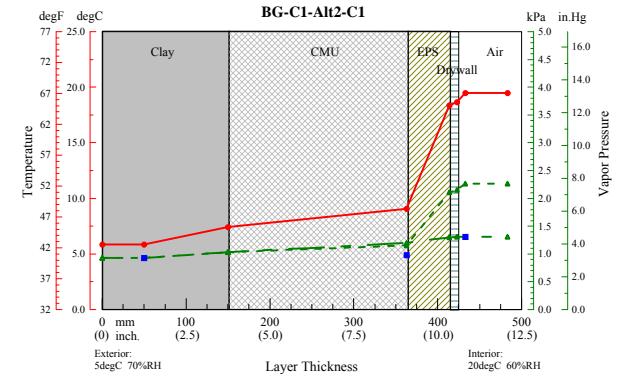


Figure C-32: Wall diagram of C1-Alt2-C1

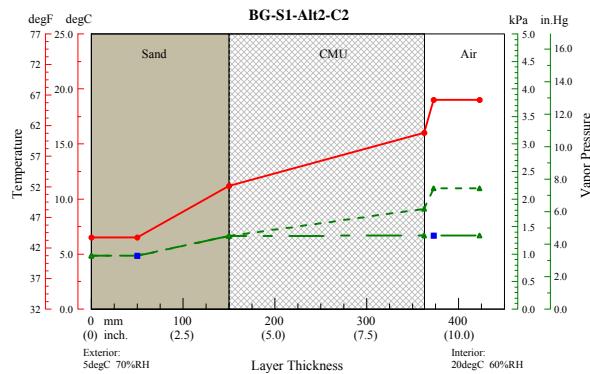


Figure C-33: Wall diagram of S1-Alt2-C2

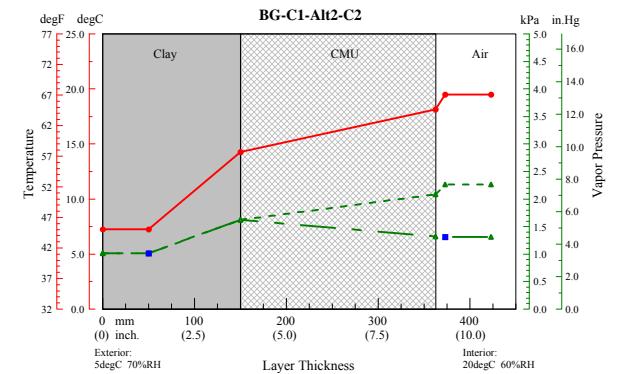


Figure C-34: Wall diagram of C1-Alt2-C2

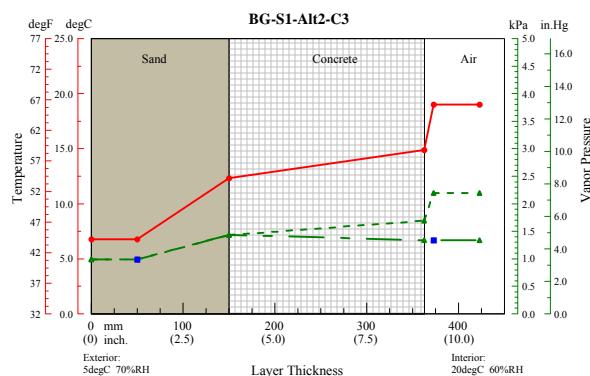


Figure C-35: Wall diagram of S1-Alt2-C3

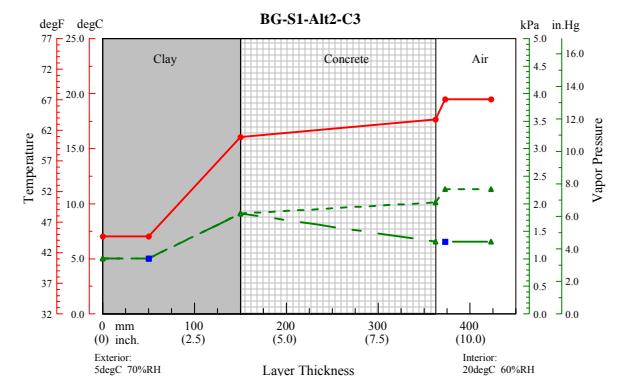


Figure C-36: Wall diagram of C1-Alt2-C3

Test cycle: **S1 – Alt3**

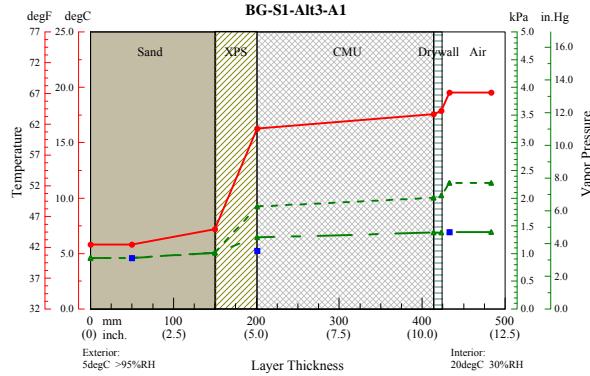


Figure C-37: Wall diagram of S1-Alt3-A1

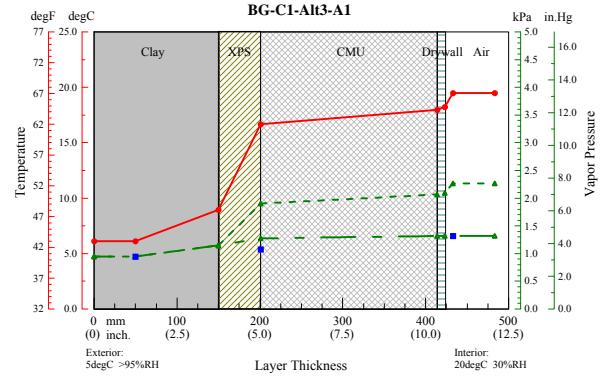


Figure C-38: Wall diagram of C1-Alt3-A1

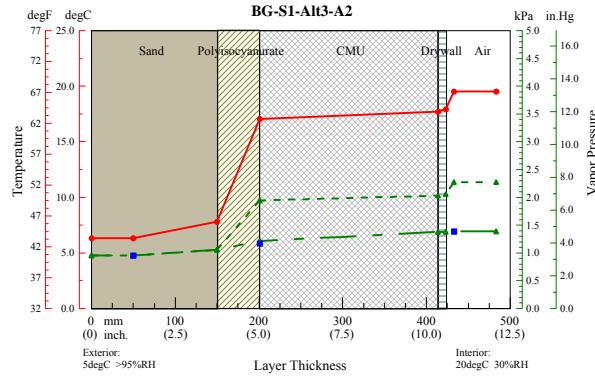


Figure C-39: Wall diagram of S1-Alt3-A2

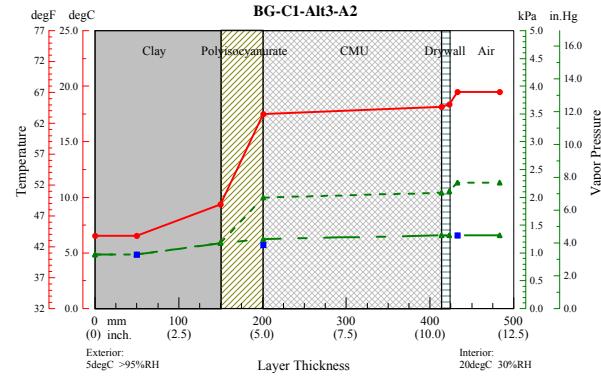


Figure C-40: Wall diagram of C1-Alt3-A2

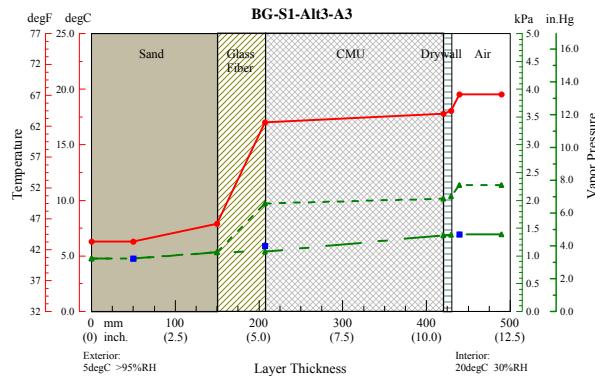


Figure C-41: Wall diagram of S1-Alt3-A3

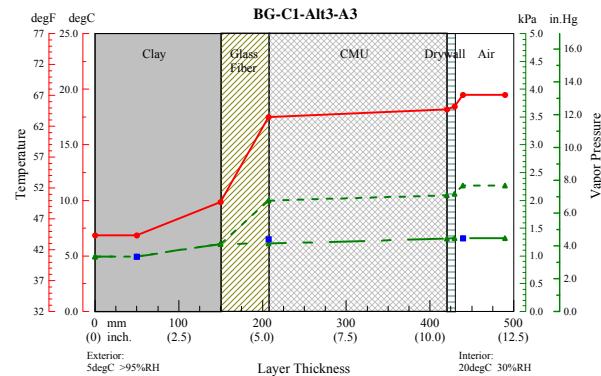


Figure C-42: Wall diagram of C1-Alt3-A3

Test cycle: **S1 – Alt3 (continued)**

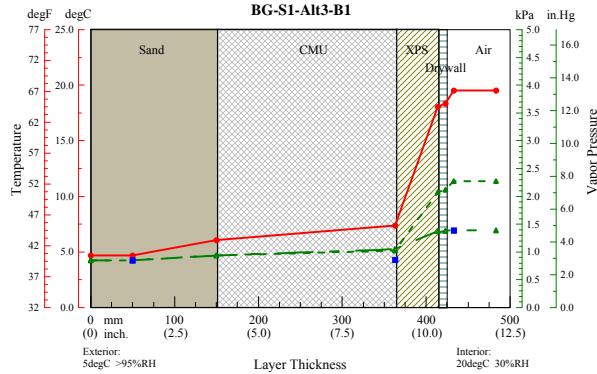


Figure C-43: Wall diagram of S1-Alt3-B1

Test cycle: **C1 – Alt3 (continued)**

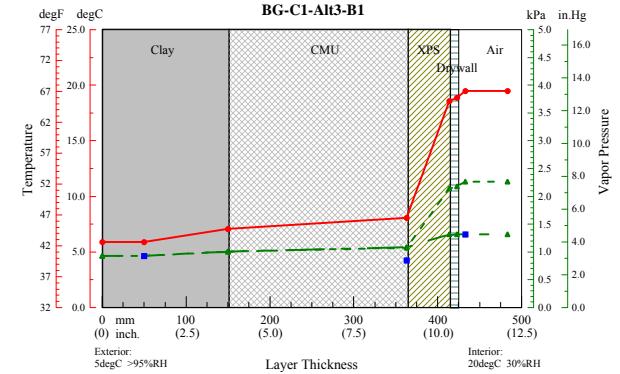


Figure C-44: Wall diagram of C1-Alt3-B1

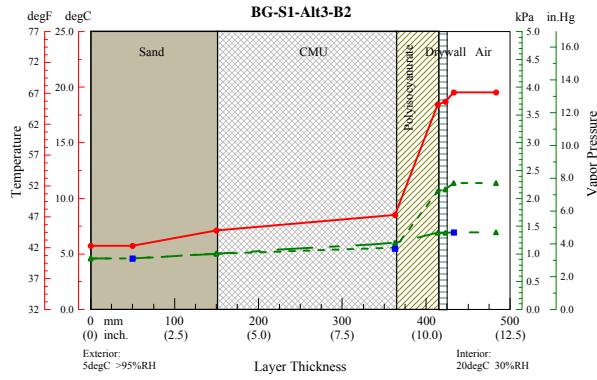


Figure C-45: Wall diagram of S1-Alt3-B2

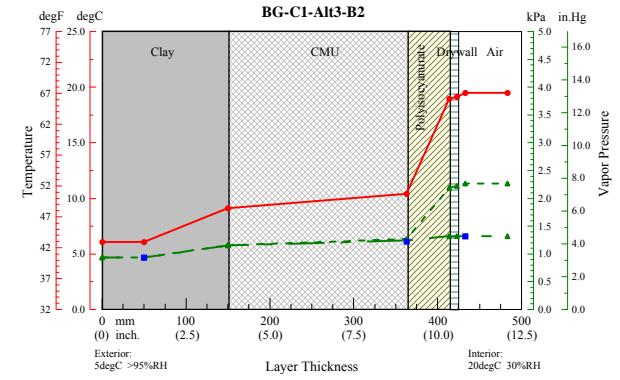


Figure C-46: Wall diagram of C1-Alt3-B2

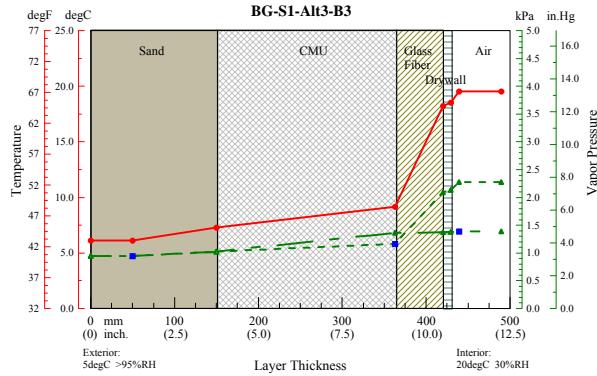


Figure C-47: Wall diagram of S1-Alt3-B3

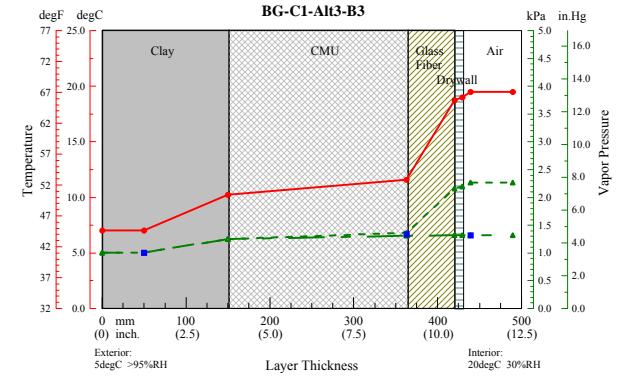


Figure C-48: Wall diagram of C1-Alt3-B3

Test cycle: **S1 – Alt3 (continued)**

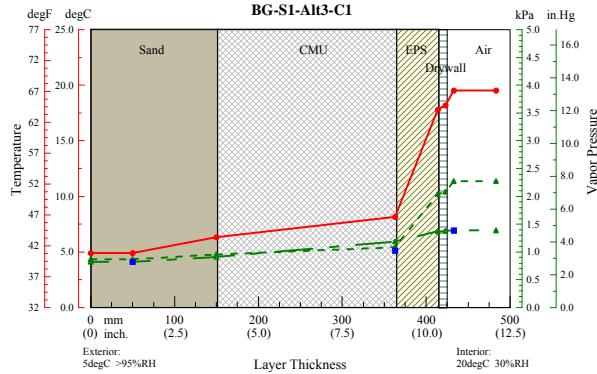


Figure C-49: Wall diagram of S1-Alt3-C1

Test cycle: **C1 – Alt3 (continued)**

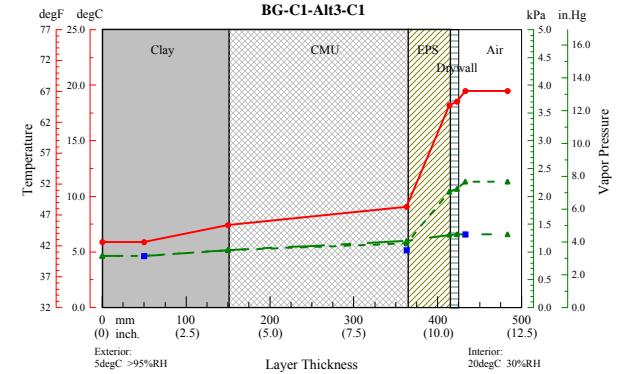


Figure C-50: Wall diagram of C1-Alt3-C1

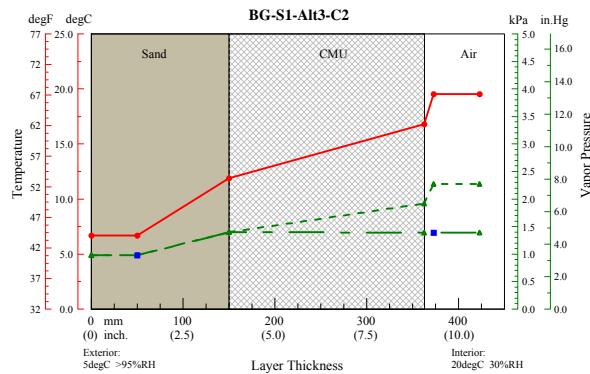


Figure C-51: Wall diagram of S1-Alt3-C2

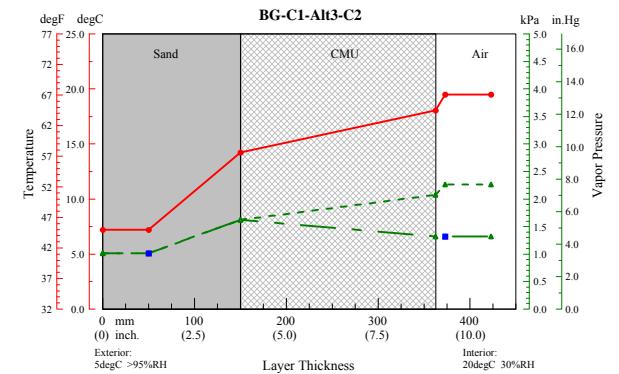


Figure C-52: Wall diagram of C1-Alt3-C2

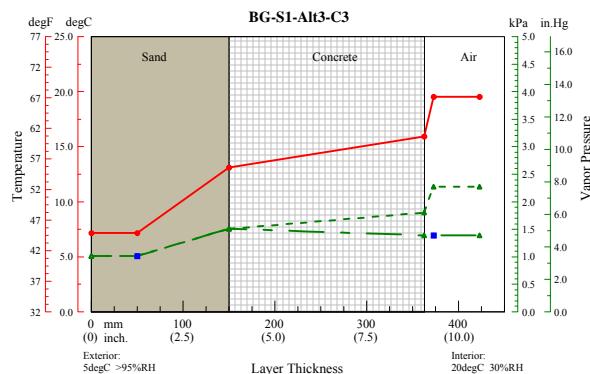


Figure C-53: Wall diagram of S1-Alt3-C3

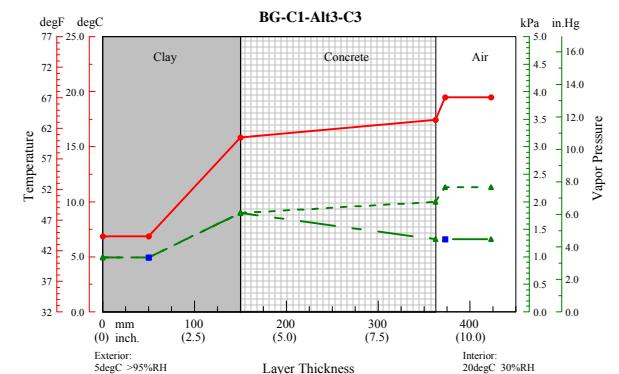


Figure C-54: Wall diagram of C1-Alt3-C3

Test cycle: **S1 – Alt4**

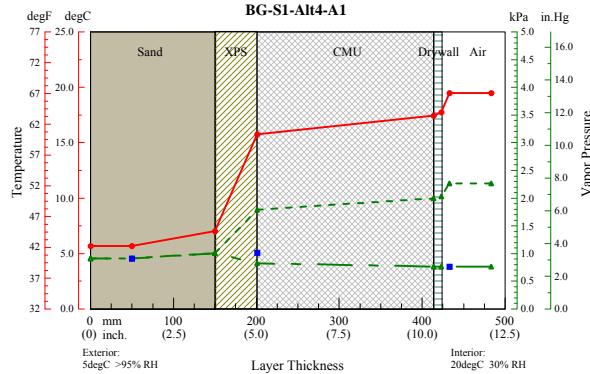


Figure C-55: Wall diagram of S1-Alt4-A1

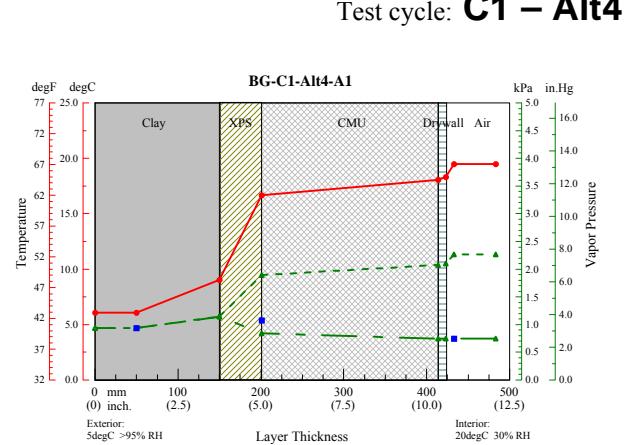


Figure C-56: Wall diagram of C1-Alt4-A1

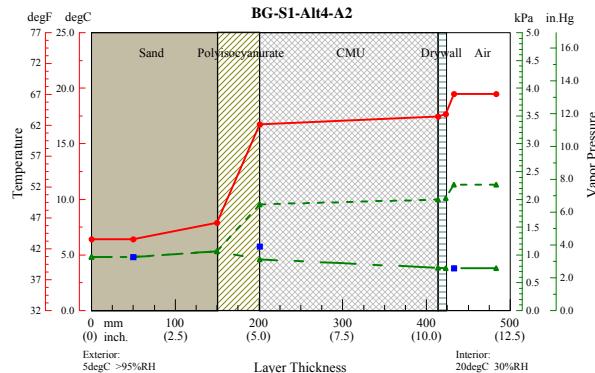


Figure C-57: Wall diagram of S1-Alt4-A2

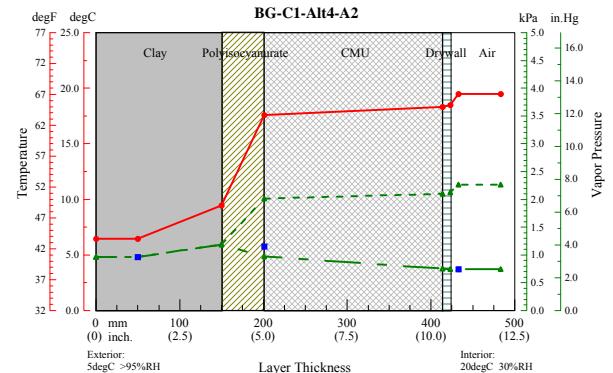


Figure C-58: Wall diagram of C1-Alt4-A2

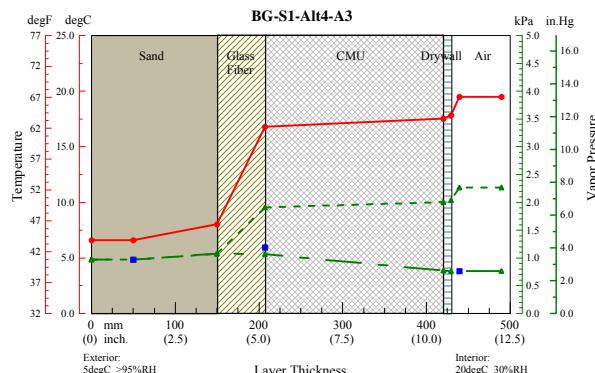


Figure C-59: Wall diagram of S1-Alt4-A3

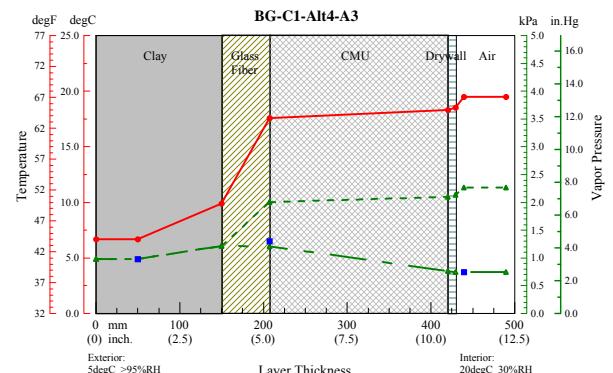


Figure C-60: Wall diagram of C1-Alt4-A3

Test cycle: **S1 – Alt4 (continued)**

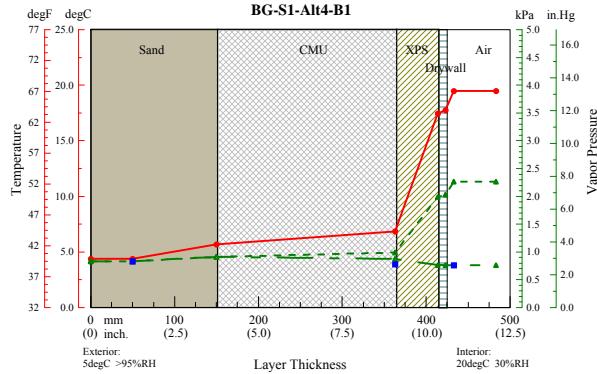


Figure C-61: Wall diagram of S1-Alt4-B1

Test cycle: **C1 – Alt4 (continued)**

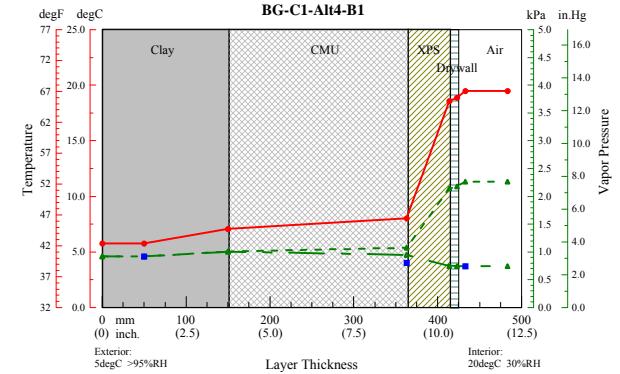


Figure C-62: Wall diagram of C1-Alt4-B1

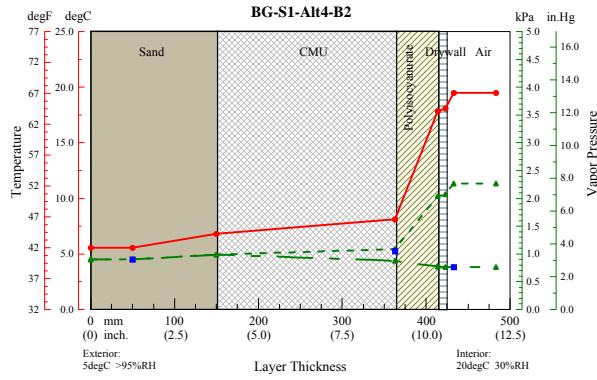


Figure C-63: Wall diagram of S1-Alt4-B2

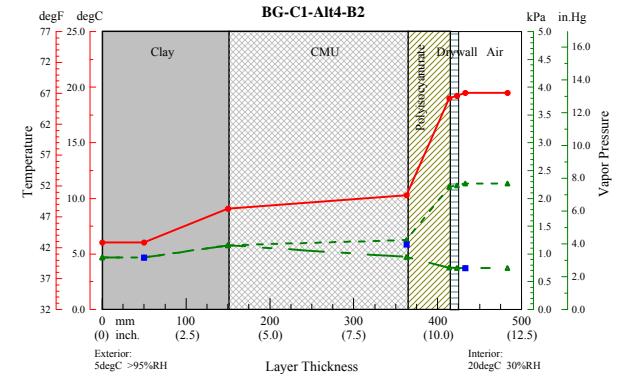


Figure C-64: Wall diagram of C1-Alt4-B2

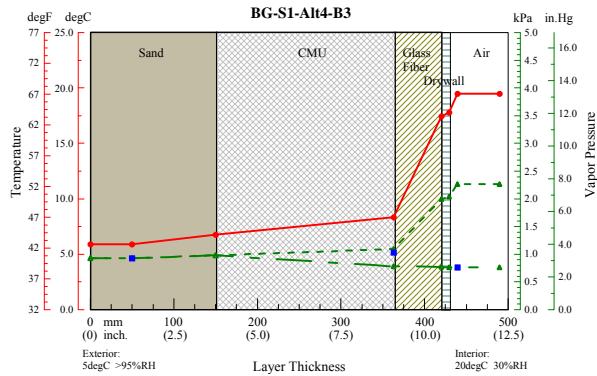


Figure C-65: Wall diagram of S1-Alt4-B3

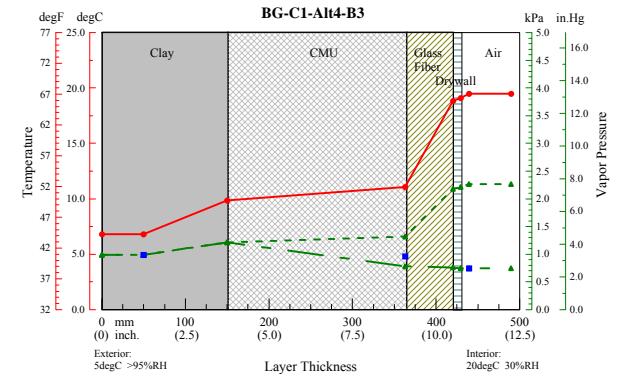


Figure C-66: Wall diagram of C1-Alt4-B3

Test cycle: **S1 – Alt4 (continued)**

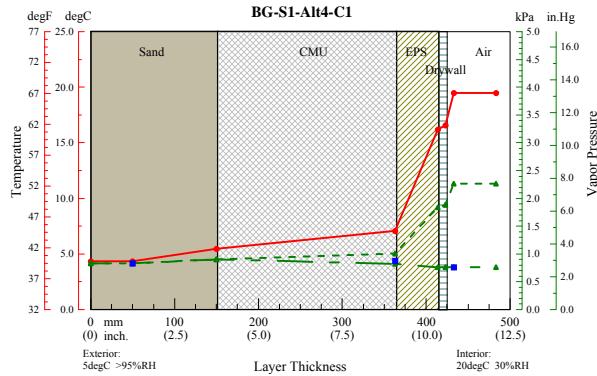


Figure C-67: Wall diagram of S1-Alt4-C1

Test cycle: **C1 – Alt4 (continued)**

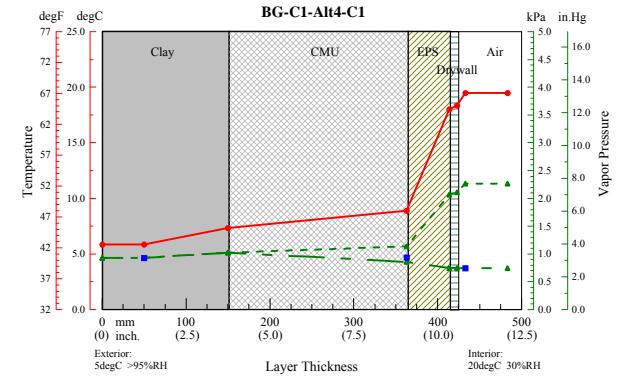


Figure C-68: Wall diagram of C1-Alt4-C1

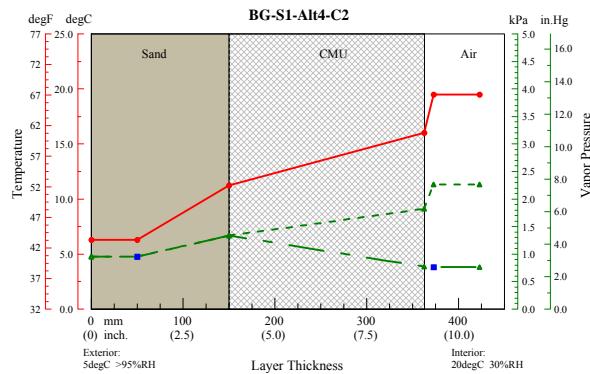


Figure C-69: Wall diagram of S1-Alt4-C2

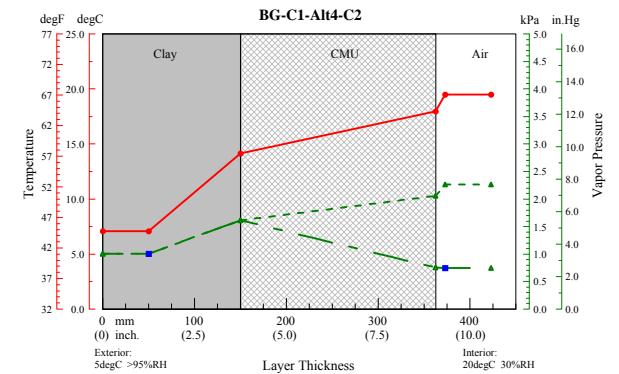


Figure C-70: Wall diagram of C1-Alt4-C2

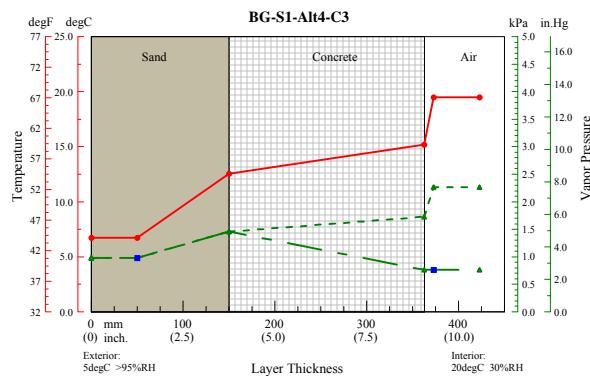


Figure C-71: Wall diagram of S1-Alt4-C3

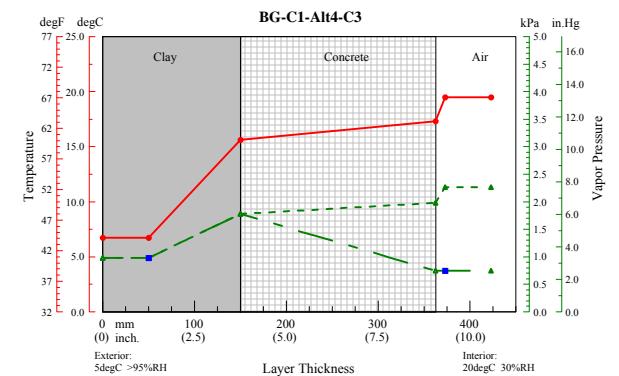


Figure C-72: Wall diagram of C1-Alt4-C3

Test cycle: **S1 – Alt5**

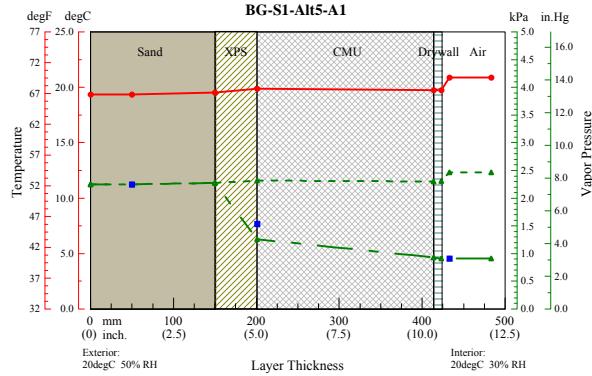


Figure C-73: Wall diagram of S1-Alt5-A1

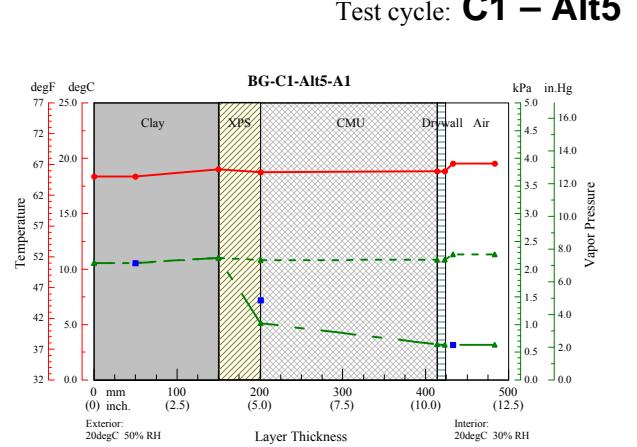


Figure C-74: Wall diagram of C1-Alt5-A1

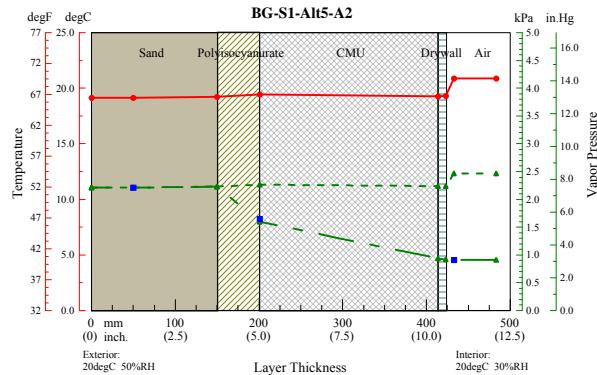


Figure C-75: Wall diagram of S1-Alt5-A2

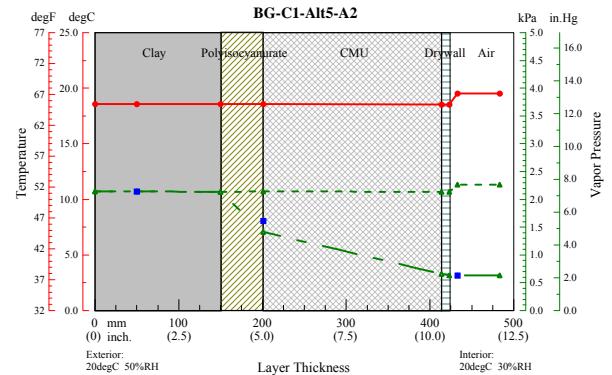


Figure C-76: Wall diagram of C1-Alt5-A2

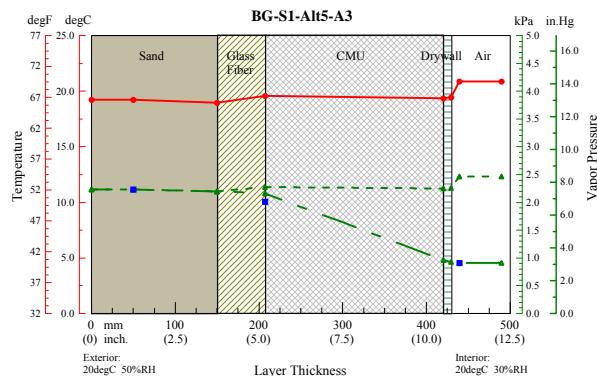


Figure C-77: Wall diagram of S1-Alt5-A3

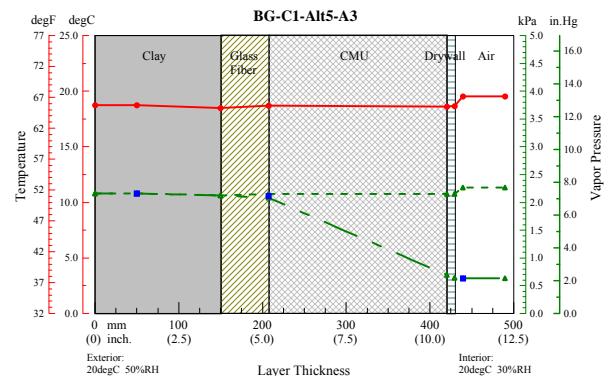


Figure C-78: Wall diagram of C1-Alt5-A3

Test cycle: **S1 – Alt5 (continued)**

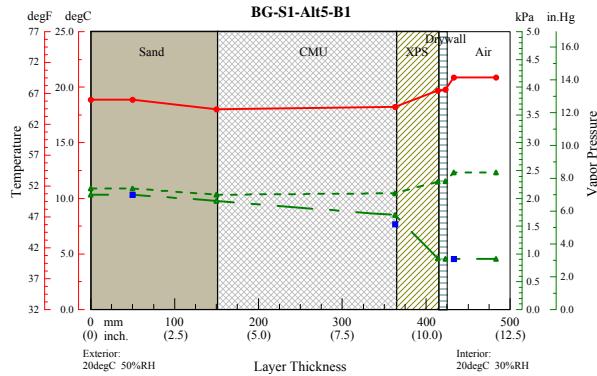


Figure C-79: Wall diagram of S1-Alt5-B1

Test cycle: **C1 – Alt5 (continued)**

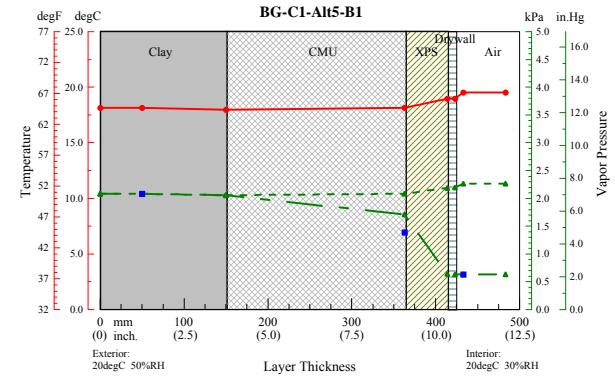


Figure C-80: Wall diagram of C1-Alt5-B1

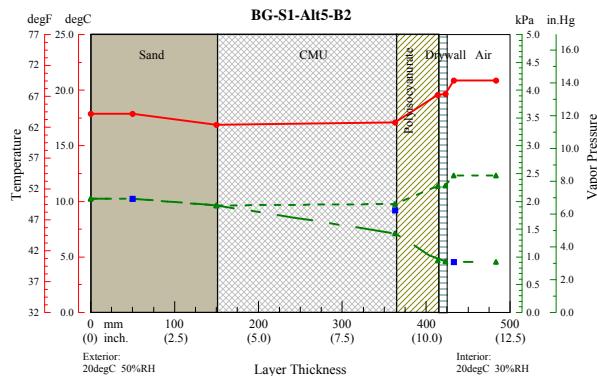


Figure C-81: Wall diagram of S1-Alt5-B2

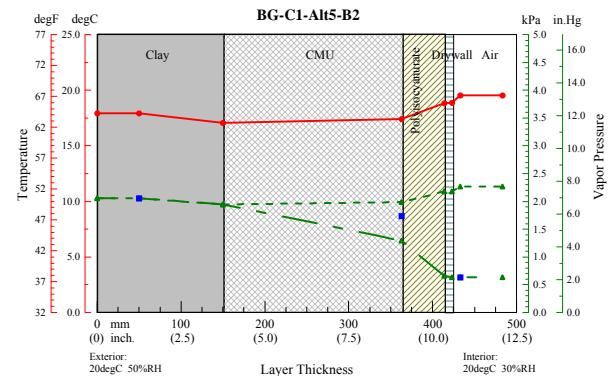


Figure C-82: Wall diagram of C1-Alt5-B2

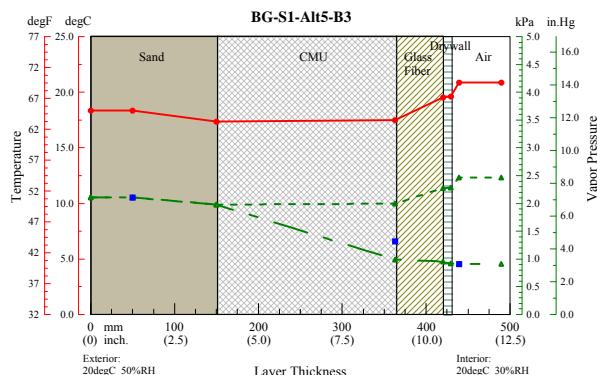


Figure C-83: Wall diagram of S1-Alt5-B3

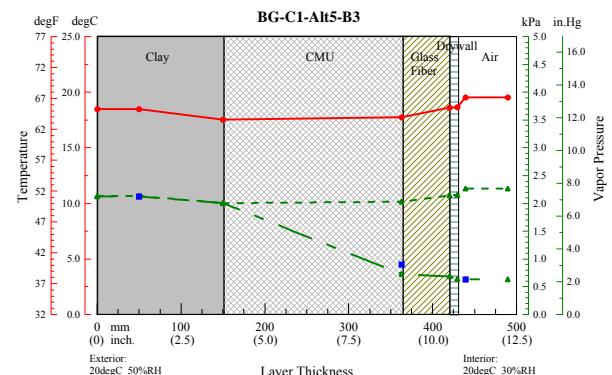


Figure C-84: Wall diagram of C1-Alt5-B3

Test cycle: **S1 – Alt5 (continued)**

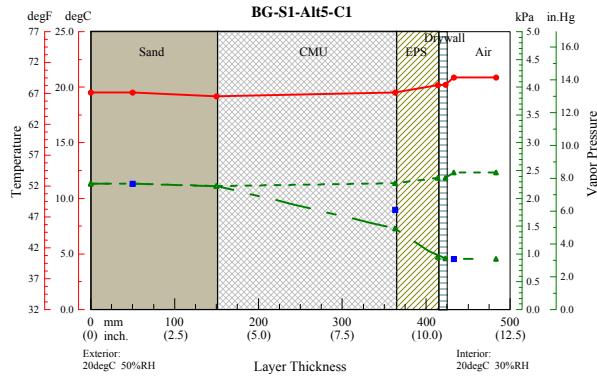


Figure C-85: Wall diagram of S1-Alt5-C1

Test cycle: **C1 – Alt5 (continued)**

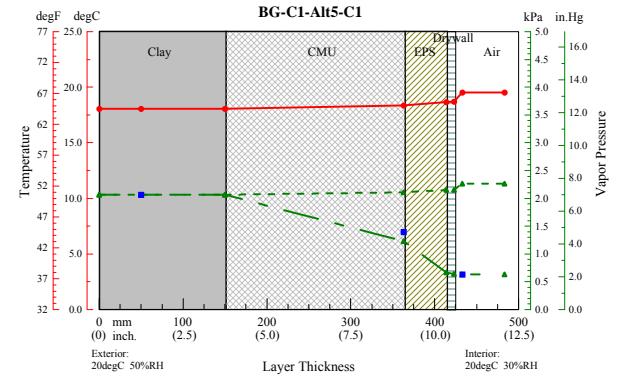


Figure C-86: Wall diagram of C1-Alt5-C1

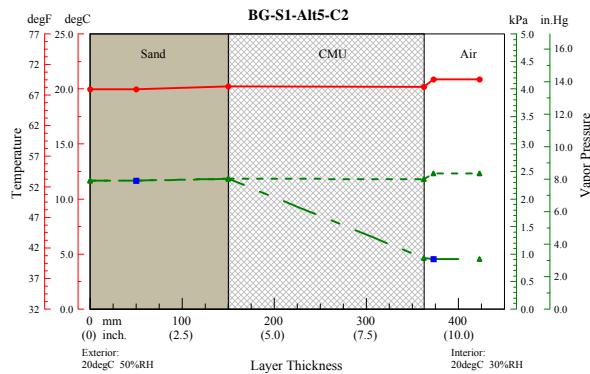


Figure C-87: Wall diagram of S1-Alt5-C2

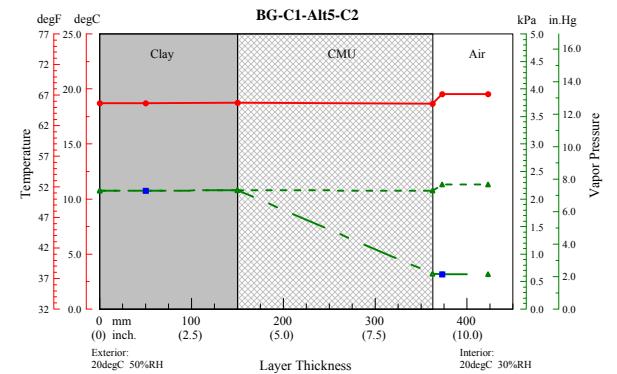


Figure C-88: Wall diagram of C1-Alt5-C2

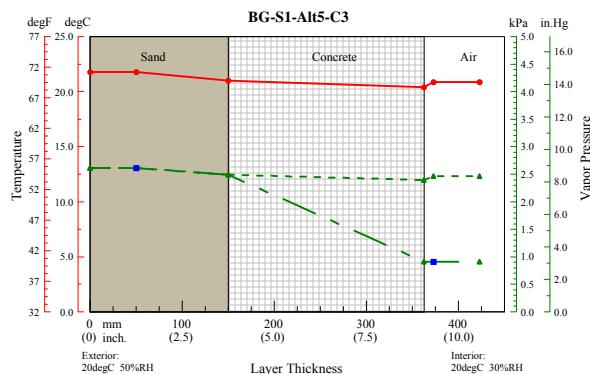


Figure C-89: Wall diagram of S1-Alt5-C3

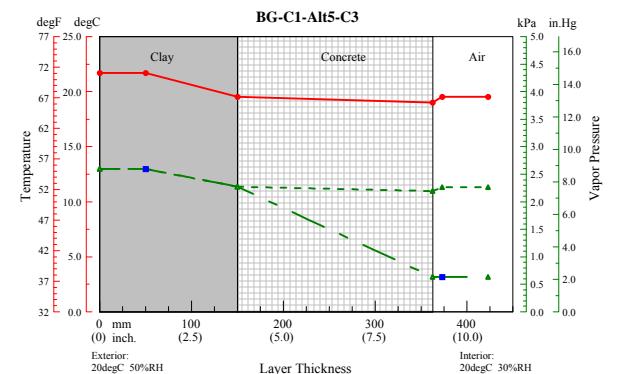


Figure C-90: Wall diagram of C1-Alt5-C3

Test cycle: **S1 – Alt6**

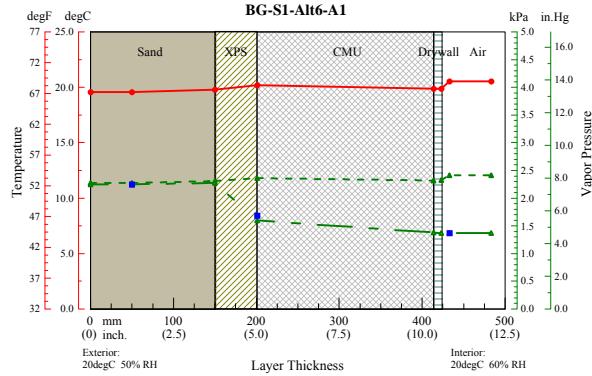


Figure C-91: Wall diagram of S1-Alt6-A1

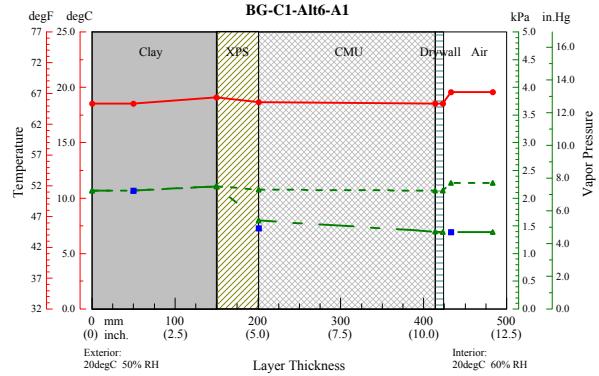


Figure C-92: Wall diagram of C1-Alt6-A1

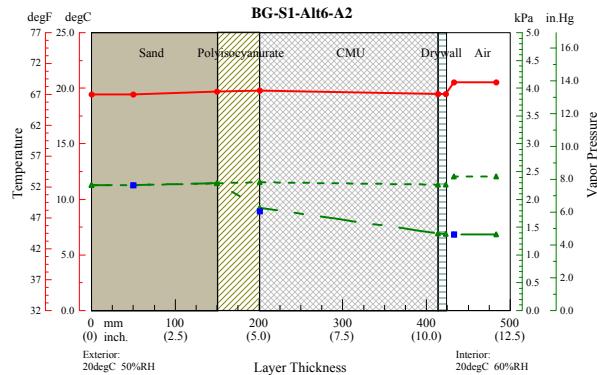


Figure C-93: Wall diagram of S1-Alt6-A2

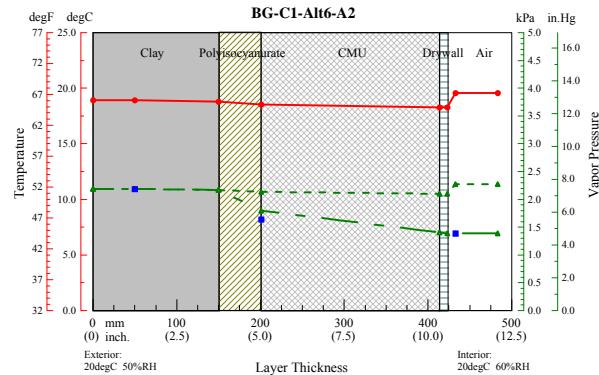


Figure C-94: Wall diagram of C1-Alt6-A2

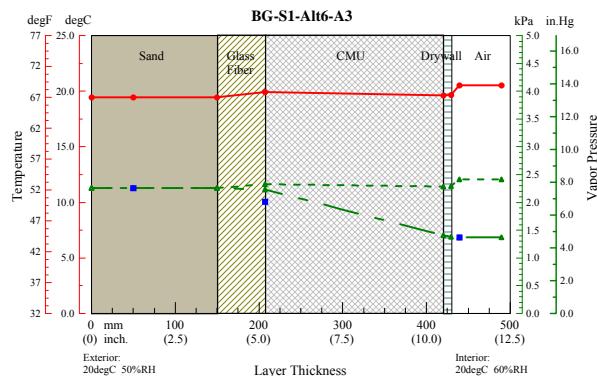


Figure C-95: Wall diagram of S1-Alt6-A3

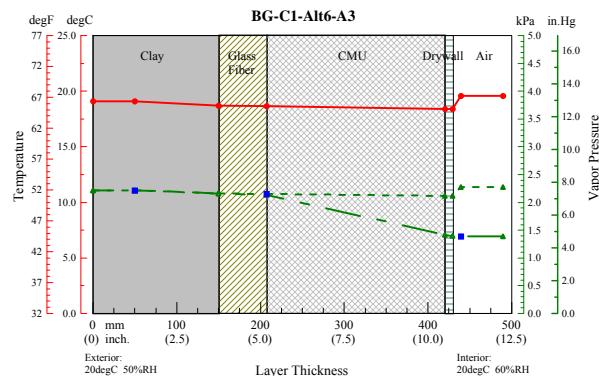


Figure C-96: Wall diagram of C1-Alt6-A3

Test cycle: **S1 – Alt6 (continued)**

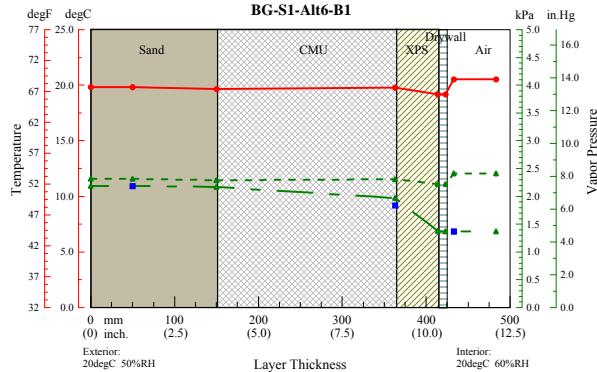


Figure C-97: Wall diagram of S1-Alt6-B1

Test cycle: **C1 – Alt6 (continued)**

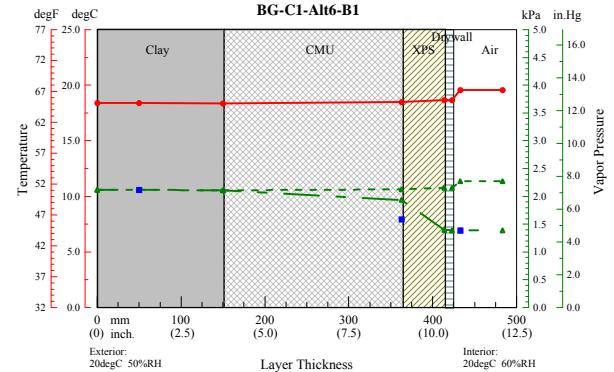


Figure C-98: Wall diagram of C1-Alt6-B1

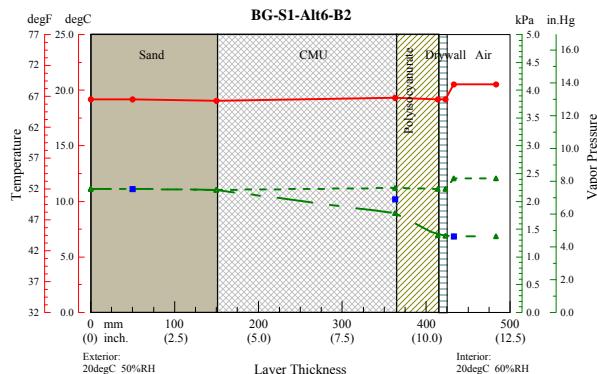


Figure C-99: Wall diagram of S1-Alt6-B2

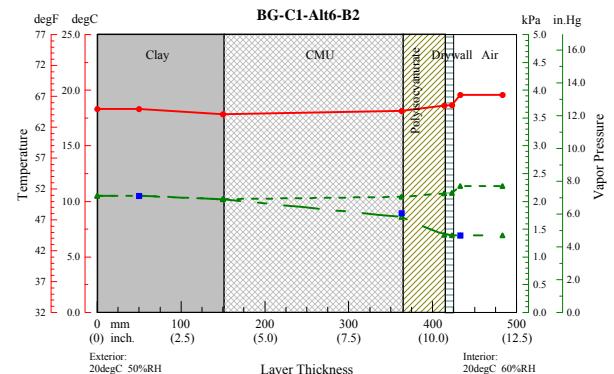


Figure C-100: Wall diagram of C1-Alt6-B2

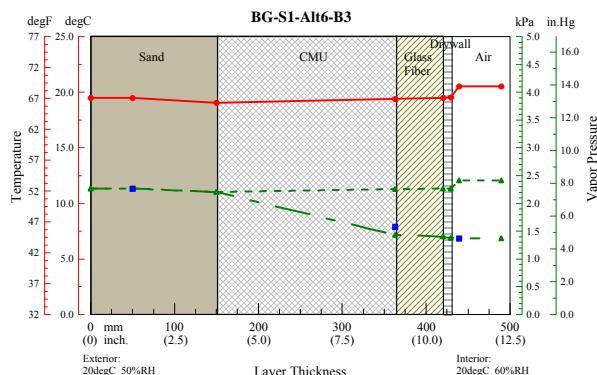


Figure C-101: Wall diagram of S1-Alt6-B3

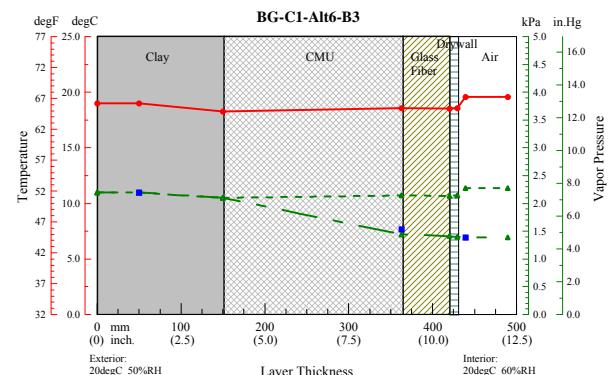


Figure C-102: Wall diagram of C1-Alt6-B3

Test cycle: **S1 – Alt6 (continued)**

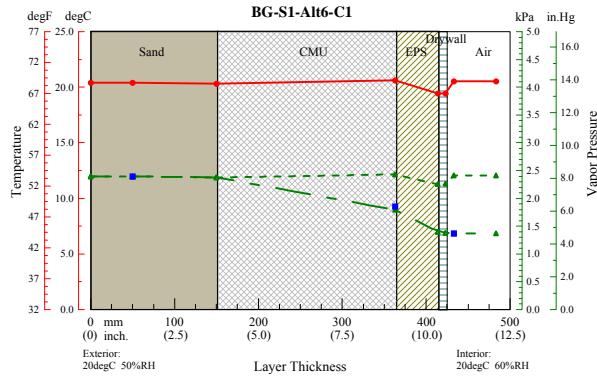


Figure C-103: Wall diagram of S1-Alt6-C1

Test cycle: **C1 – Alt6 (continued)**

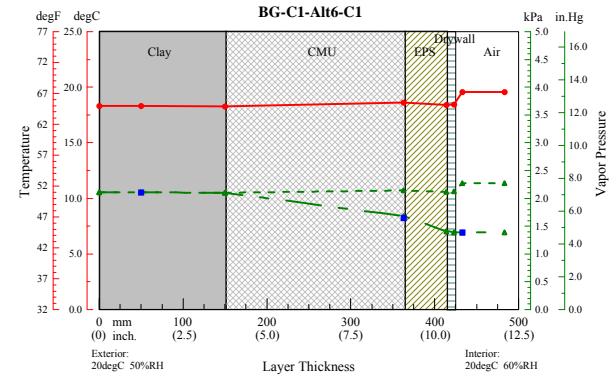


Figure C-104: Wall diagram of C1-Alt6-C1

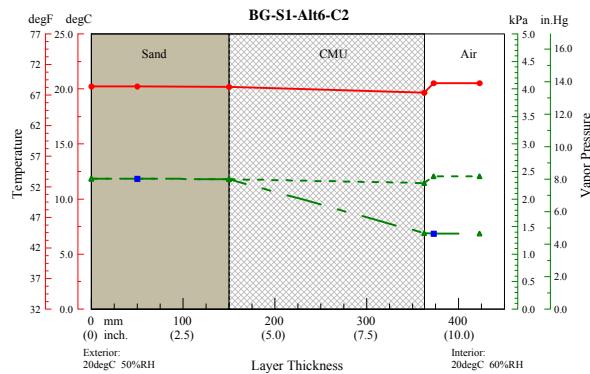


Figure C-105: Wall diagram of S1-Alt6-C2

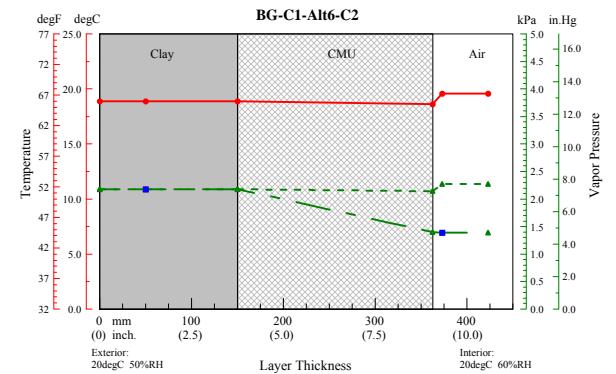


Figure C-106: Wall diagram of C1-Alt6-C2

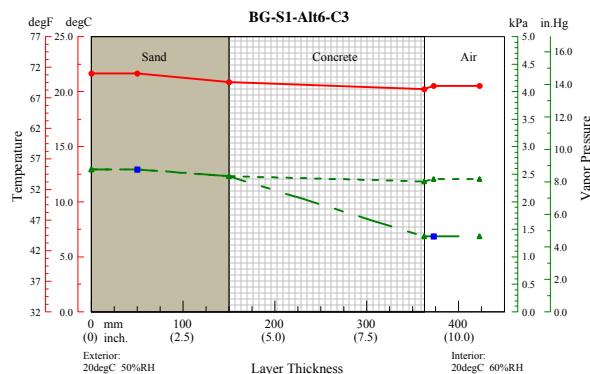


Figure C-107: Wall diagram of S1-Alt6-C3

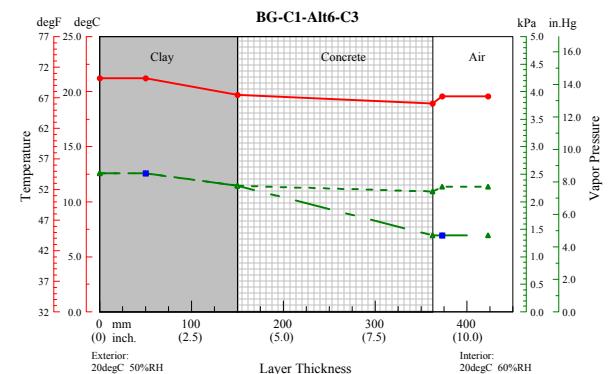


Figure C-108: Wall diagram of C1-Alt6-C3

Test cycle: **S1 – Alt7**

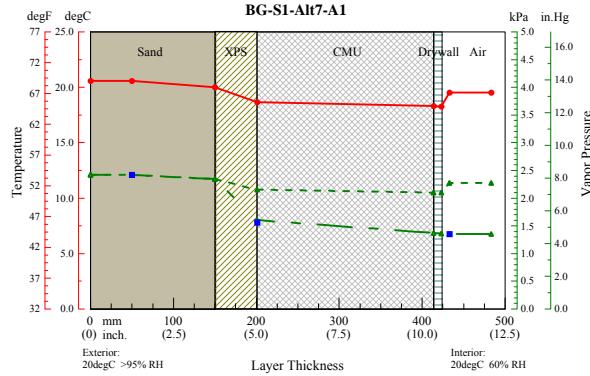


Figure C-109: Wall diagram of S1-Alt7-A1

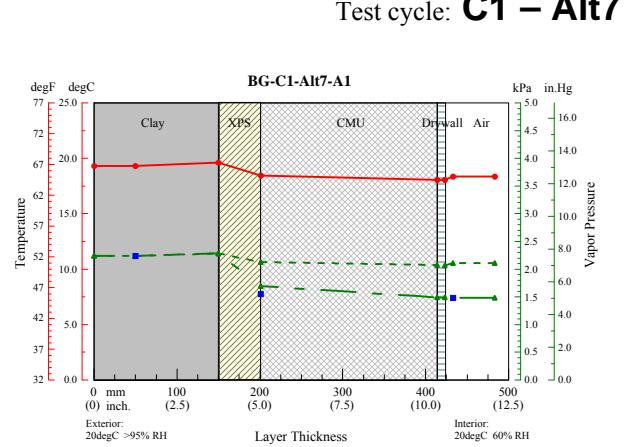


Figure C-110: Wall diagram of C1-Alt7-A1

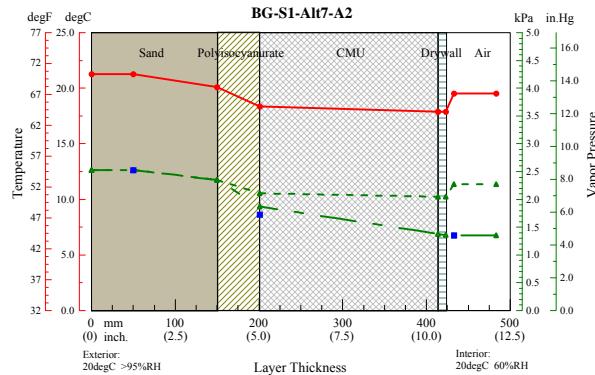


Figure C-111: Wall diagram of S1-Alt7-A2

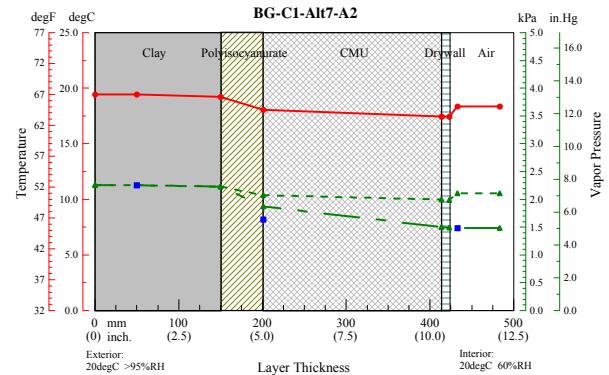


Figure C-112: Wall diagram of C1-Alt7-A2

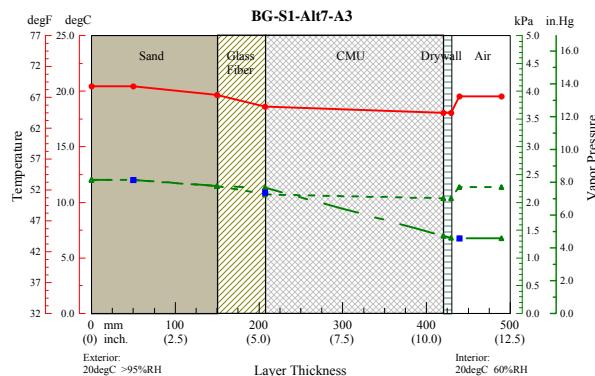


Figure C-113: Wall diagram of S1-Alt7-A3

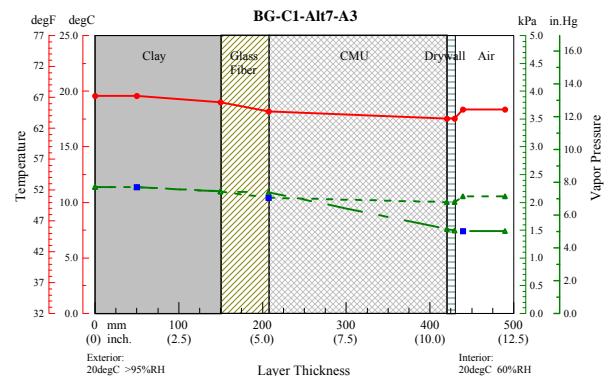


Figure C-114: Wall diagram of C1-Alt7-A3

Test cycle: **S1 – Alt7 (continued)**

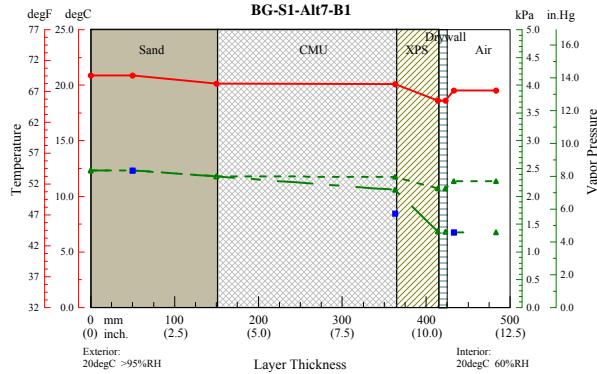


Figure C-115: Wall diagram of S1-Alt7-B1

Test cycle: **C1 – Alt7 (continued)**

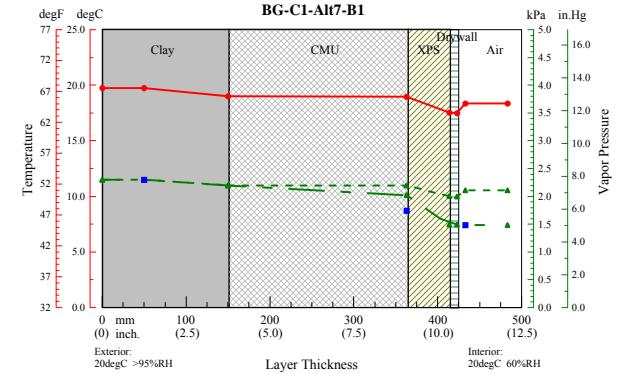


Figure C-116: Wall diagram of C1-Alt7-B1

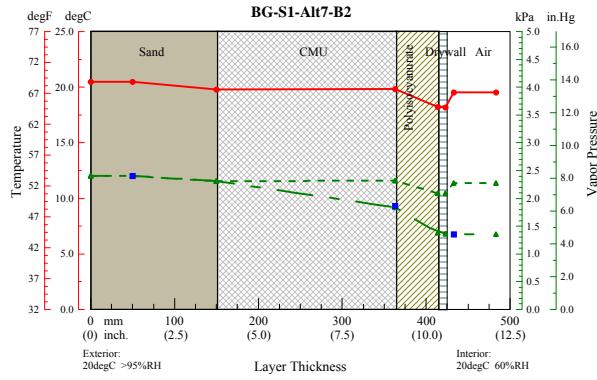


Figure C-117: Wall diagram of S1-Alt7-B2

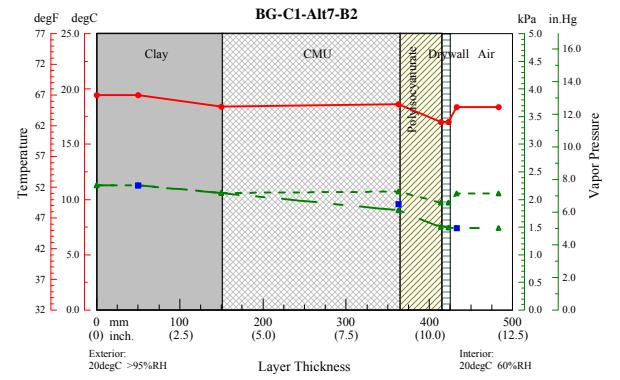


Figure C-118: Wall diagram of C1-Alt7-B2

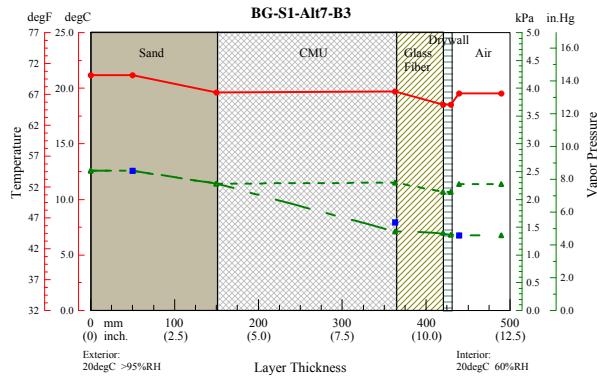


Figure C-119: Wall diagram of S1-Alt7-B3

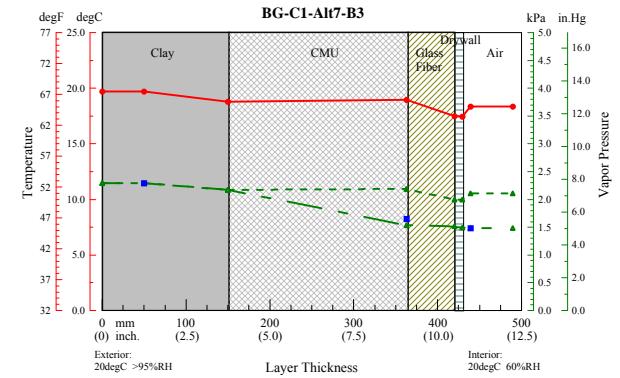


Figure C-120: Wall diagram of C1-Alt7-B3

Test cycle: **S1 – Alt7 (continued)**

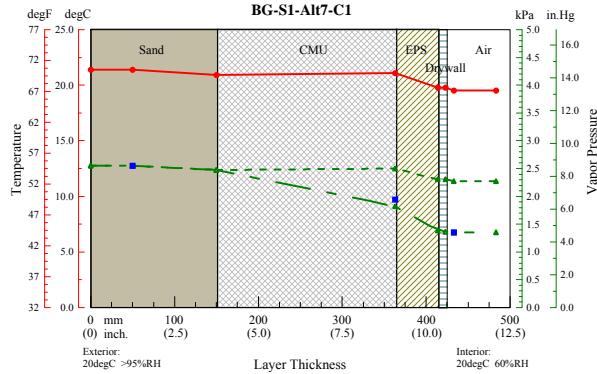


Figure C-121: Wall diagram of S1-Alt7-C1

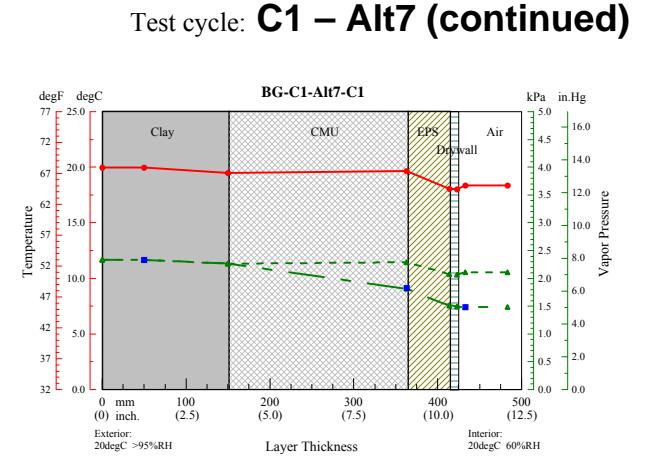


Figure C-122: Wall diagram of C1-Alt7-C1

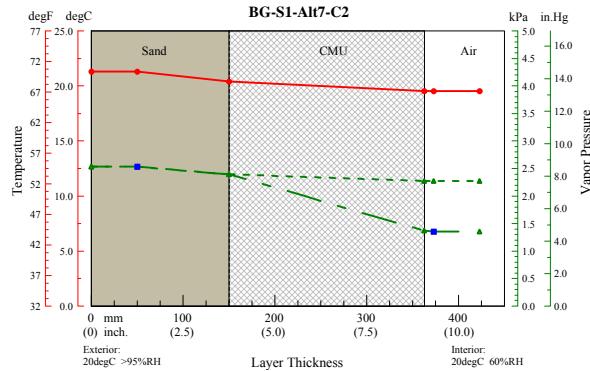


Figure C-123: Wall diagram of S1-Alt7-C2

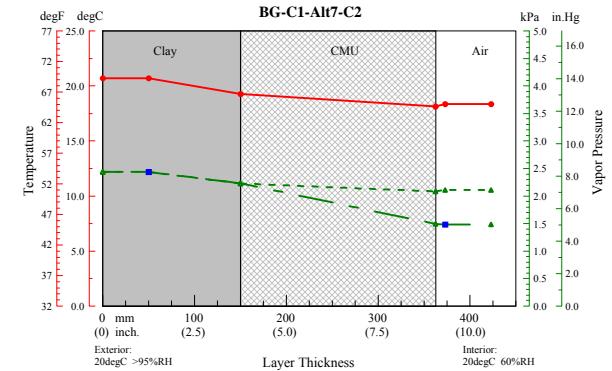


Figure C-124: Wall diagram of C1-Alt7-C2

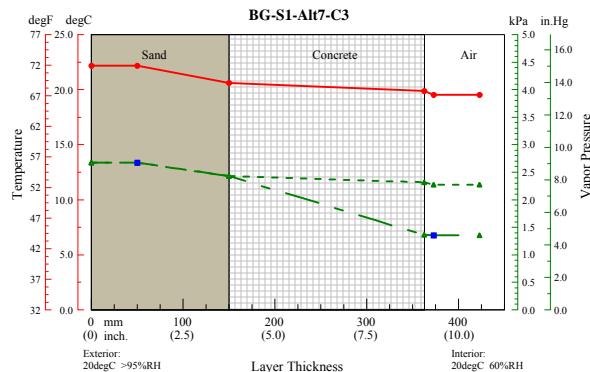


Figure C-125: Wall diagram of S1-Alt7-C3

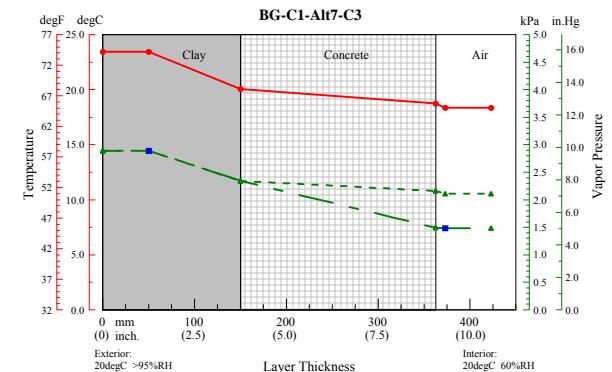


Figure C-126: Wall diagram of C1-Alt7-C3

Test cycle: **S1 – Alt8**

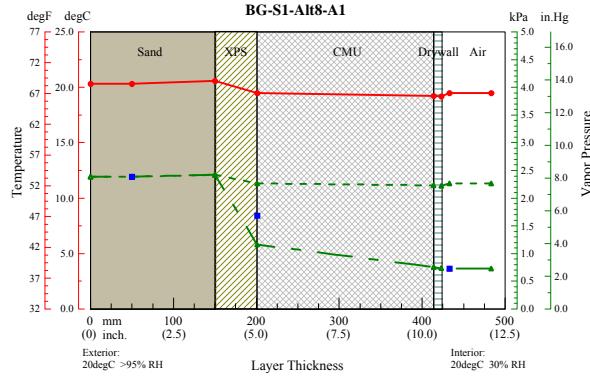


Figure C-127: Wall diagram of S1-Alt8-A1

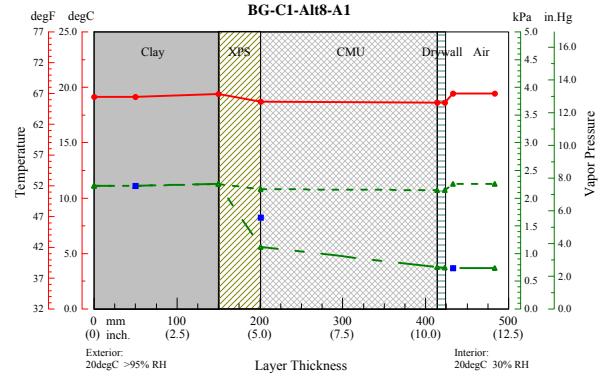


Figure C-128: Wall diagram of C1-Alt8-A1

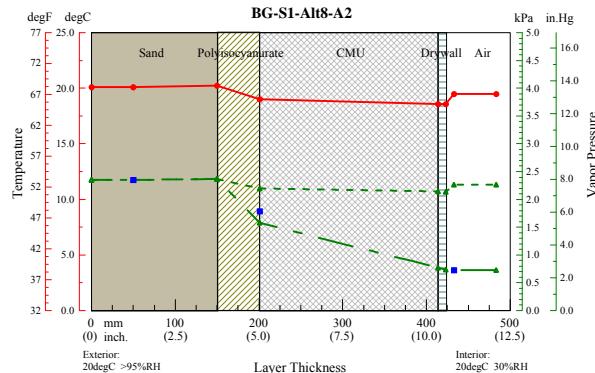


Figure C-129: Wall diagram of S1-Alt8-A2

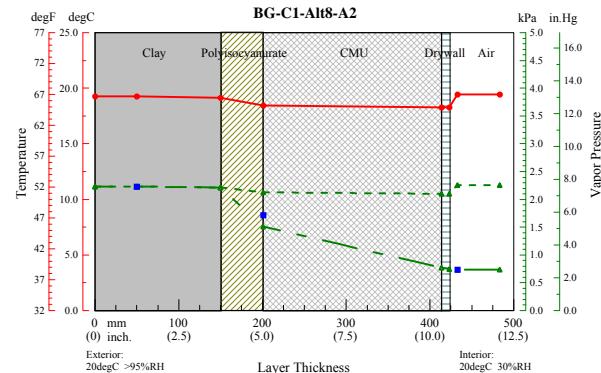


Figure C-130: Wall diagram of C1-Alt8-A2

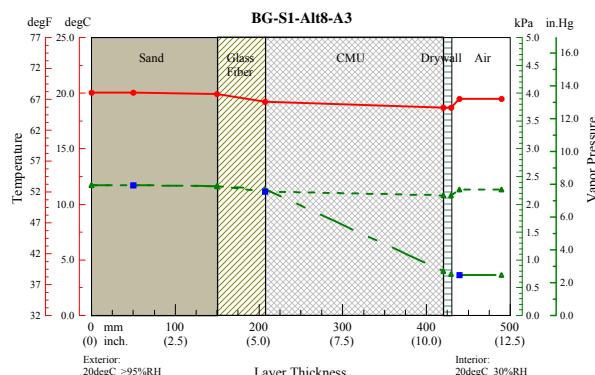


Figure C-131: Wall diagram of S1-Alt8-A3

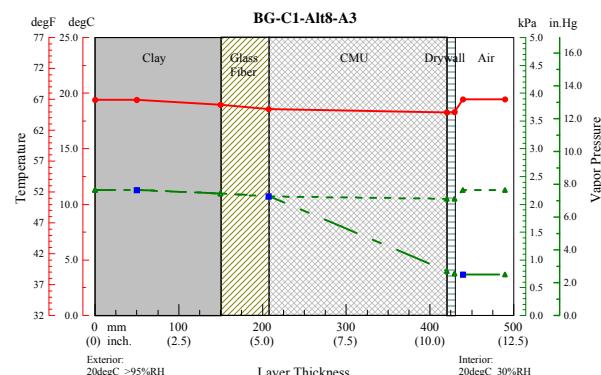


Figure C-132: Wall diagram of C1-Alt8-A3

Test cycle: **S1 – Alt8 (continued)**

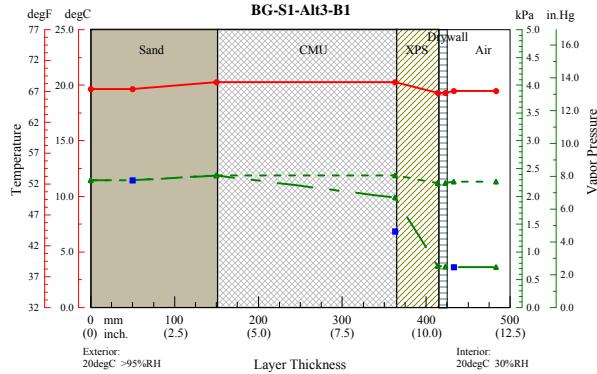


Figure C-133: Wall diagram of S1-Alt8-B1

Test cycle: **C1 – Alt8 (continued)**

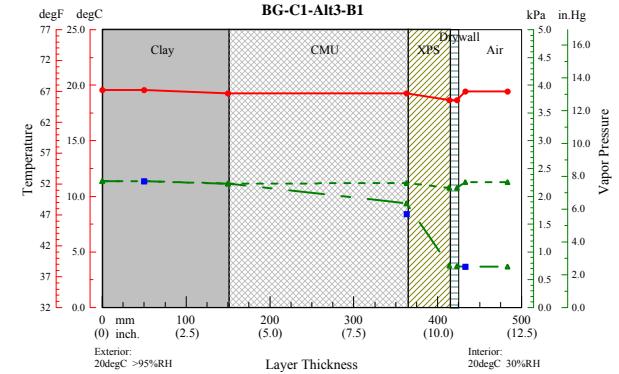


Figure C-134: Wall diagram of C1-Alt8-B1

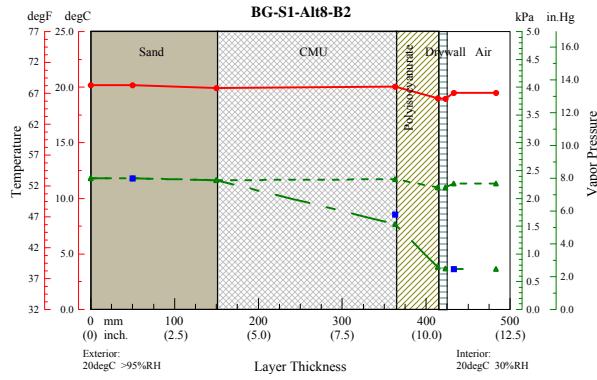


Figure C-135: Wall diagram of S1-Alt8-B2

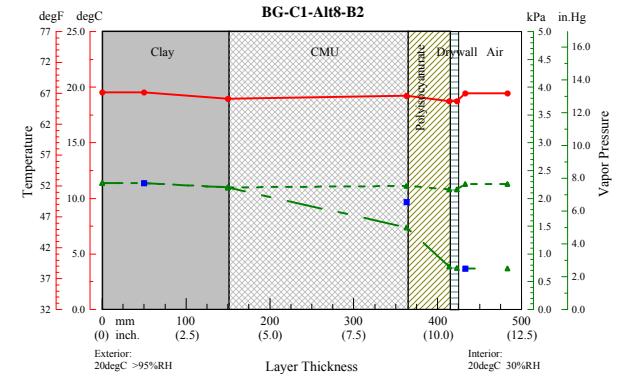


Figure C-136: Wall diagram of C1-Alt8-B2

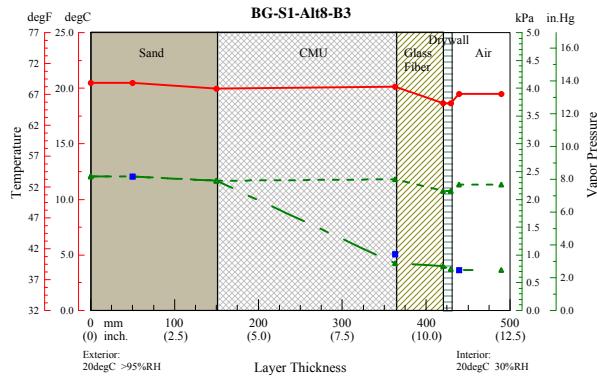


Figure C-137: Wall diagram of S1-Alt8-B3

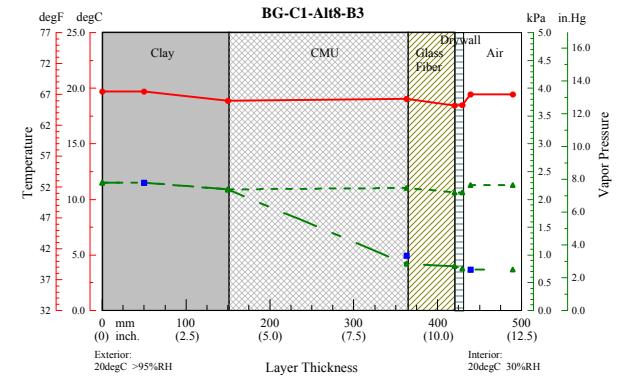


Figure C-138: Wall diagram of C1-Alt8-B3

Test cycle: **S1 – Alt8 (continued)**

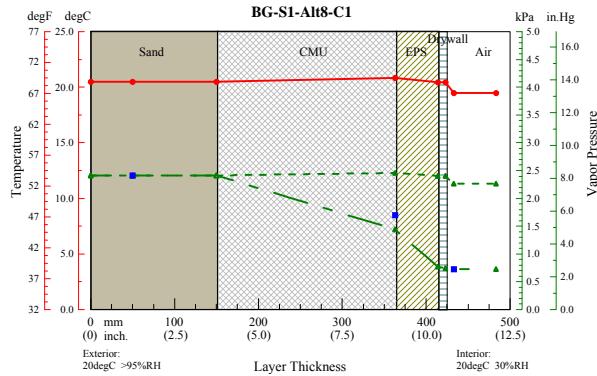


Figure C-139: Wall diagram of S1-Alt8-C1

Test cycle: **C1 – Alt8 (continued)**

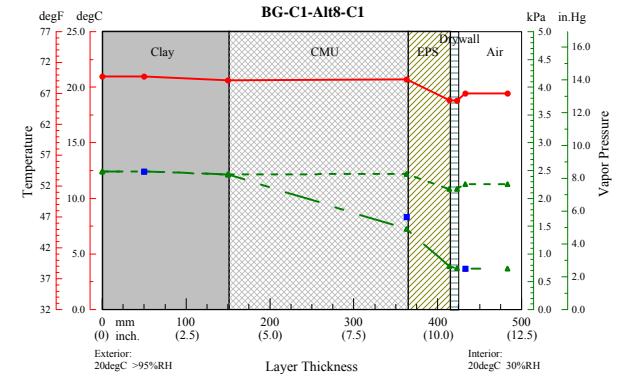


Figure C-140: Wall diagram of C1-Alt8-C1

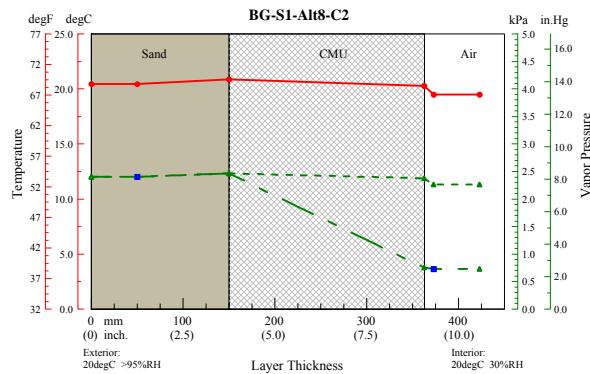


Figure C-141: Wall diagram of S1-Alt8-C2

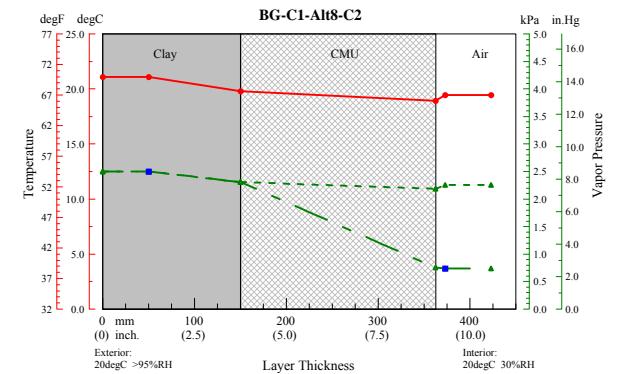


Figure C-142: Wall diagram of C1-Alt8-C2

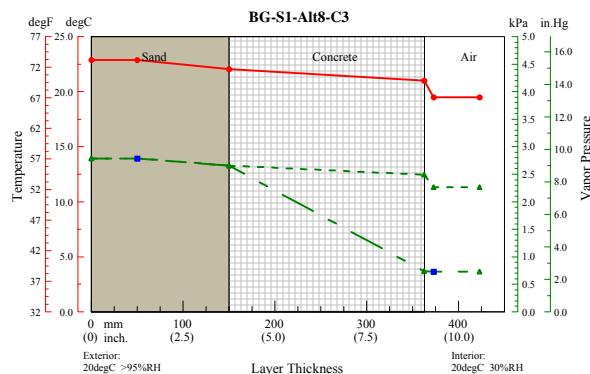


Figure C-143: Wall diagram of S1-Alt8-C3

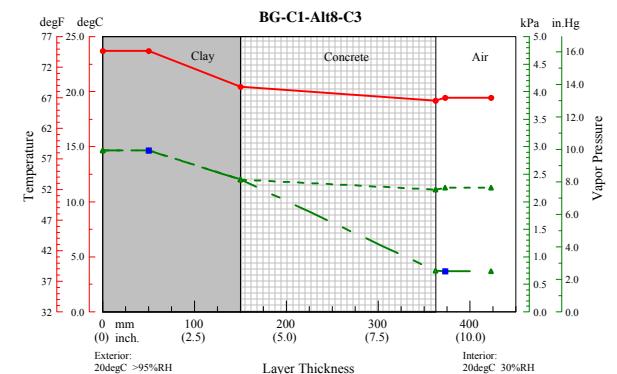


Figure C-144: Wall diagram of C1-Alt8-C3

Measurement series: **S2**

Test cycle: **S2 – Alt1**

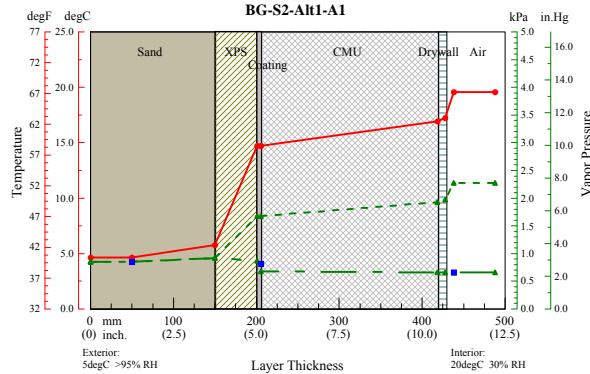


Figure C-145: Wall diagram of S2-Alt1-A1

Measurement series: **C2**

Test cycle: **C2 – Alt1**

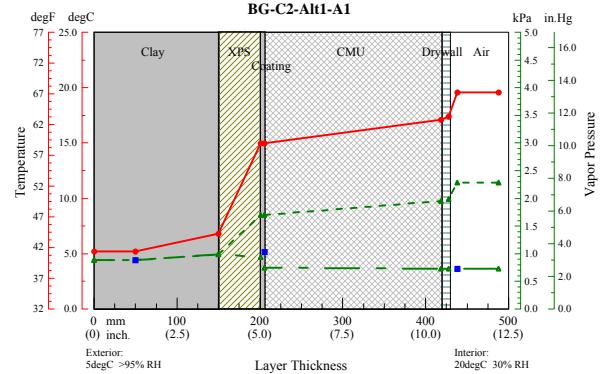


Figure C-146: Wall diagram of C2-Alt1-A1

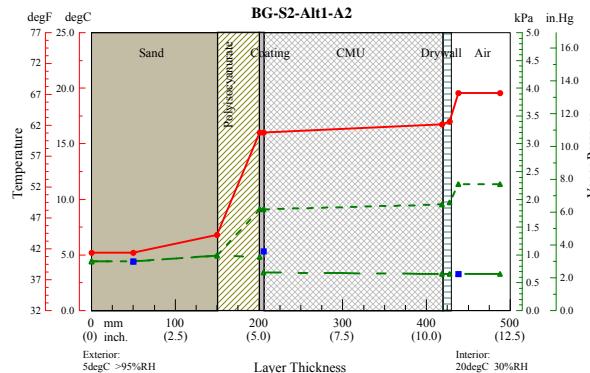


Figure C-147: Wall diagram of S2-Alt1-A2

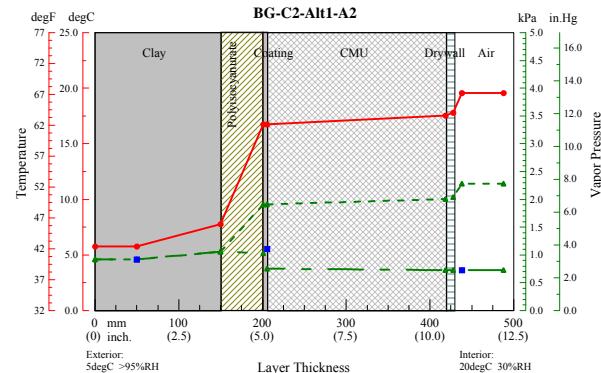


Figure C-148: Wall diagram of C2-Alt1-A2

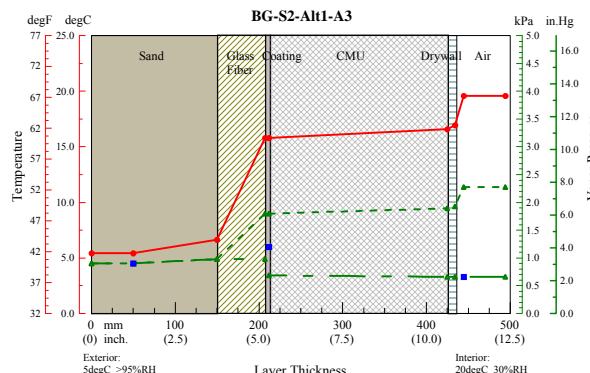


Figure C-149: Wall diagram of S2-Alt1-A3

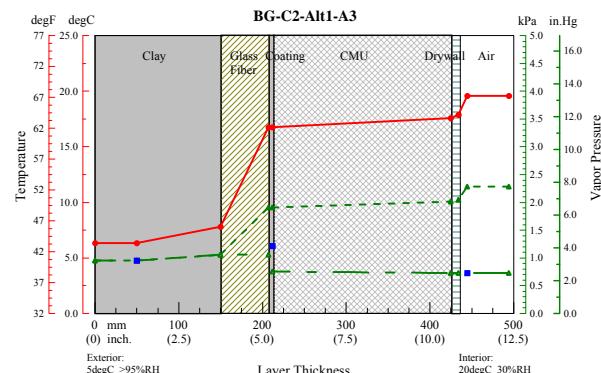


Figure C-150: Wall diagram of C2-Alt1-A3

Test cycle: **S2 – Alt1 (continued)**

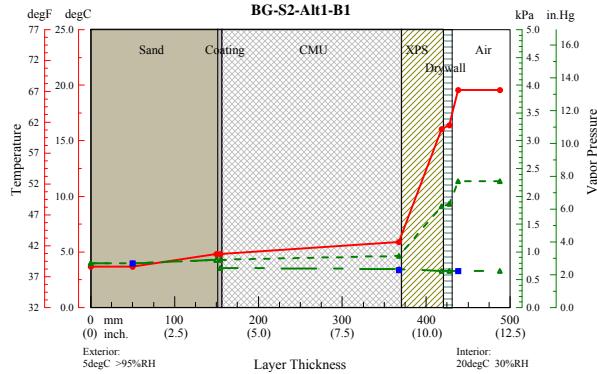


Figure C-151: Wall diagram of S2-Alt1-B1

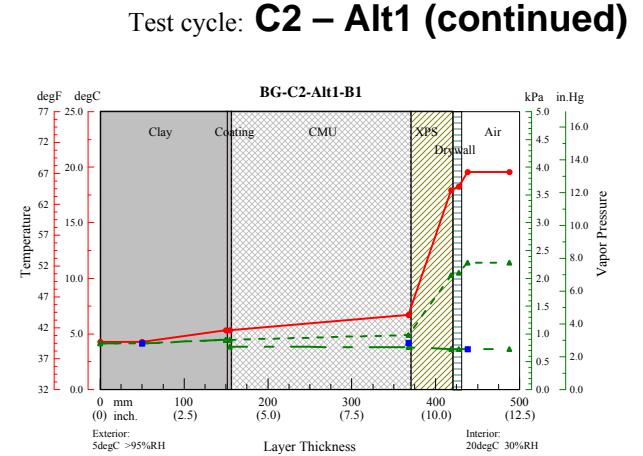


Figure C-152: Wall diagram of C2-Alt1-B1

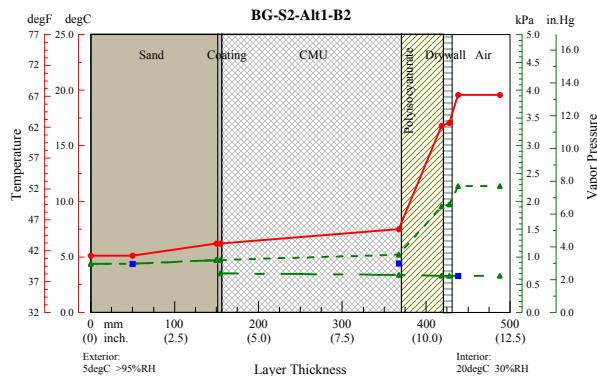


Figure C-153: Wall diagram of S2-Alt1-B2

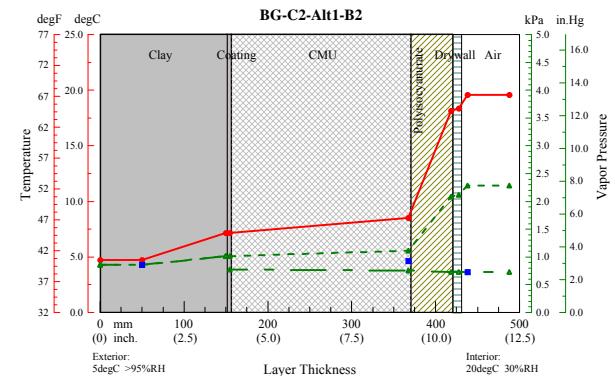


Figure C-154: Wall diagram of C2-Alt1-B2

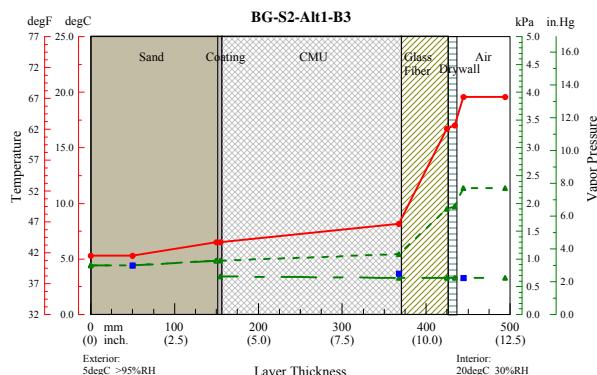


Figure C-155: Wall diagram of S2-Alt1-B3

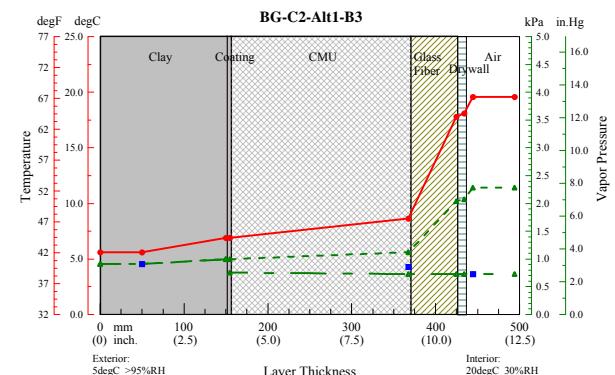


Figure C-156: Wall diagram of C2-Alt1-B3

Test cycle: **S2 – Alt1 (continued)**

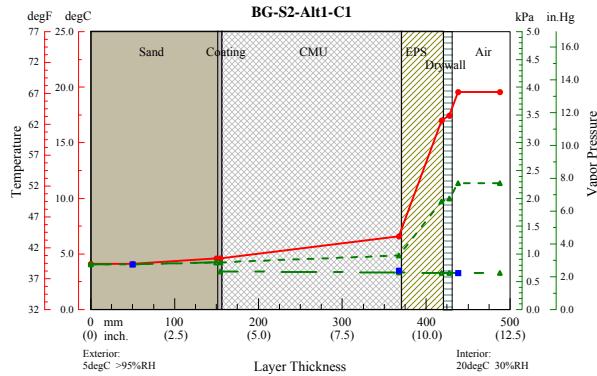


Figure C-157: Wall diagram of S2-Alt1-C1

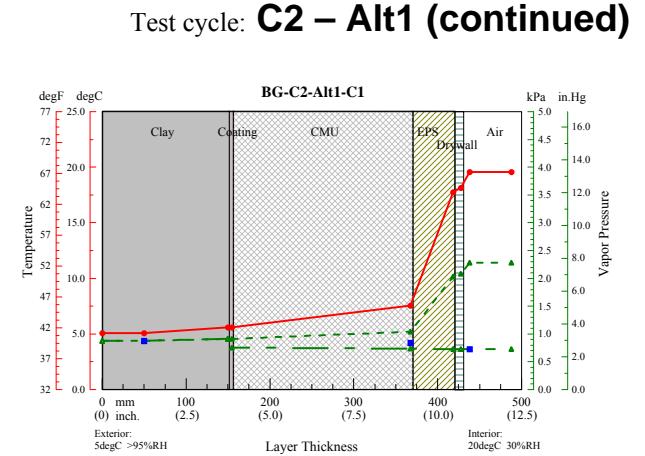


Figure C-158: Wall diagram of C2-Alt1-C1

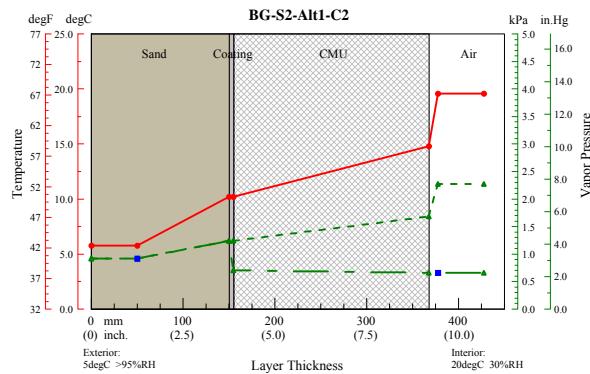


Figure C-159: Wall diagram of S2-Alt1-C2

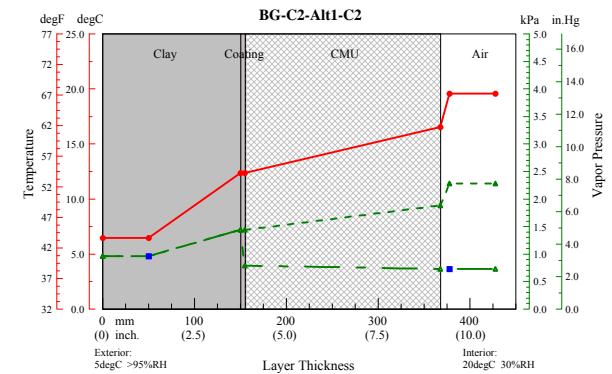


Figure C-160: Wall diagram of C2-Alt1-C2

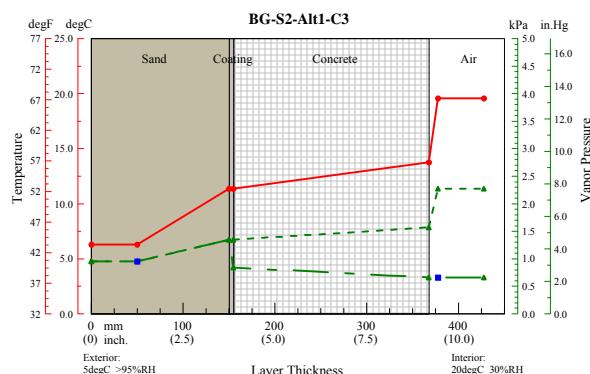


Figure C-161: Wall diagram of S2-Alt1-C3

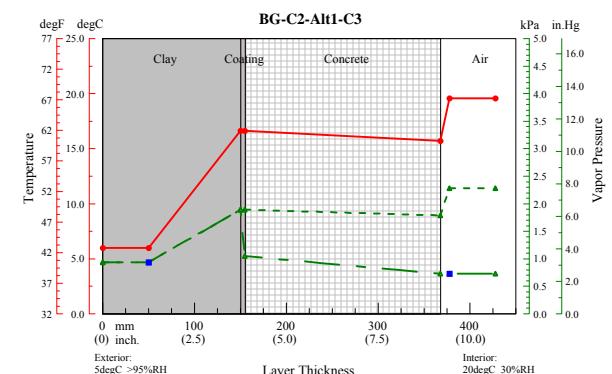


Figure C-162: Wall diagram of C2-Alt1-C3

Test cycle: **S2 – Alt2**

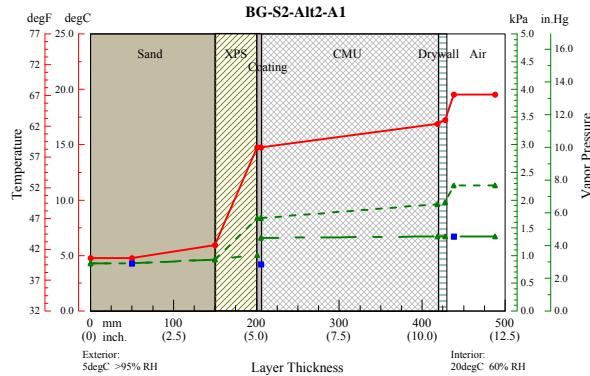


Figure C-163: Wall diagram of S2-Alt2-A1

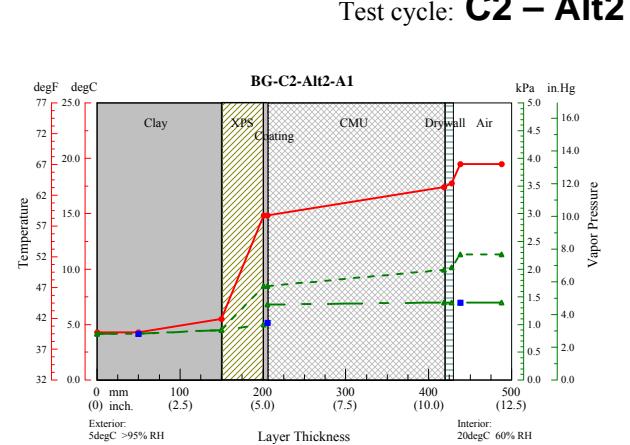


Figure C-164: Wall diagram of C2-Alt2-A1

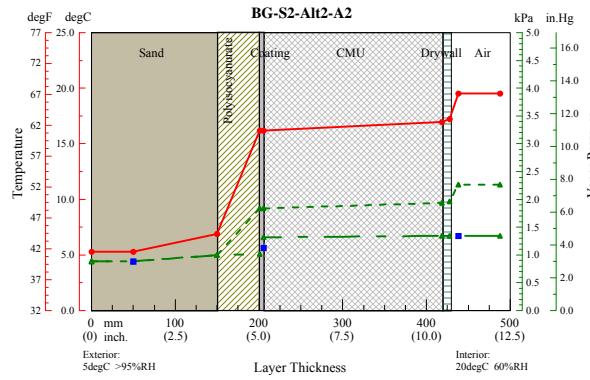


Figure C-165: Wall diagram of S2-Alt2-A2

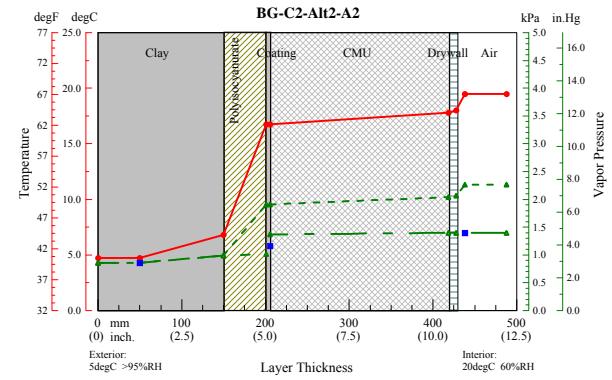


Figure C-166: Wall diagram of C2-Alt2-A2

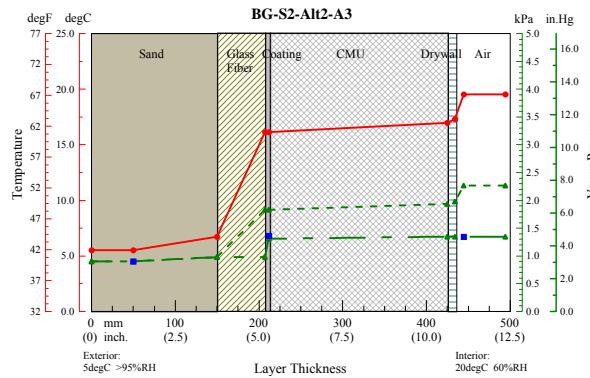


Figure C-167: Wall diagram of S2-Alt2-A3

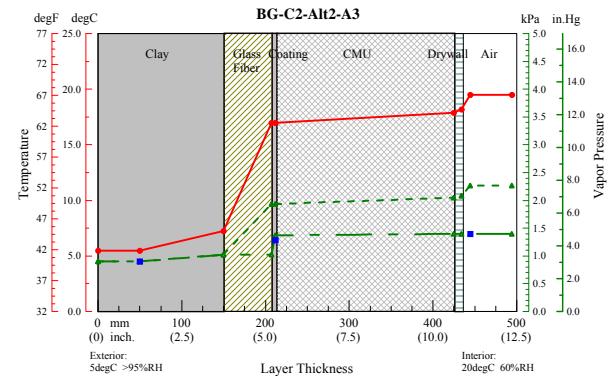


Figure C-168: Wall diagram of C2-Alt2-A3

Test cycle: **S2 – Alt2 (continued)**

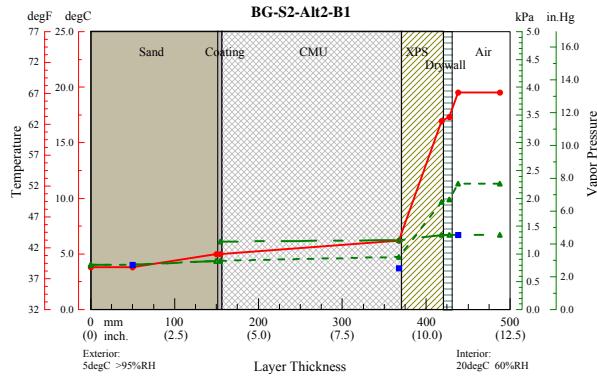


Figure C-169: Wall diagram of S2-Alt2-B1

Test cycle: **C2 – Alt2 (continued)**

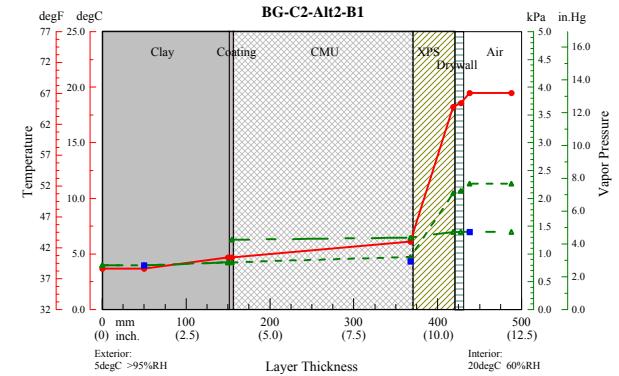


Figure C-170: Wall diagram of C2-Alt2-B1

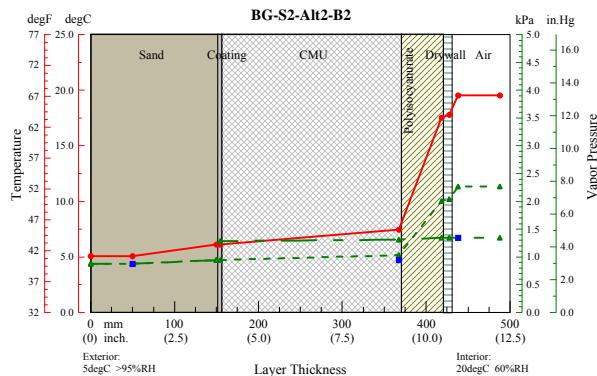


Figure C-171: Wall diagram of S2-Alt2-B2

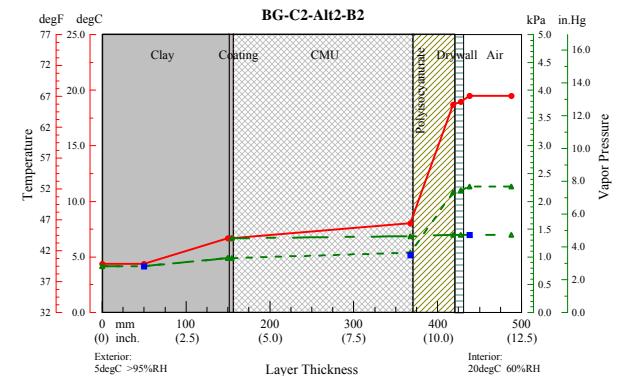


Figure C-172: Wall diagram of C2-Alt2-B2

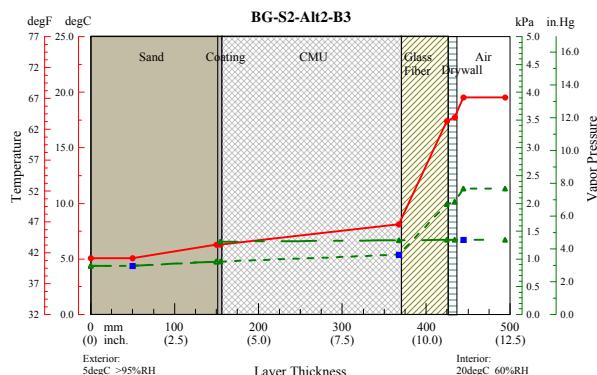


Figure C-173: Wall diagram of S2-Alt2-B3

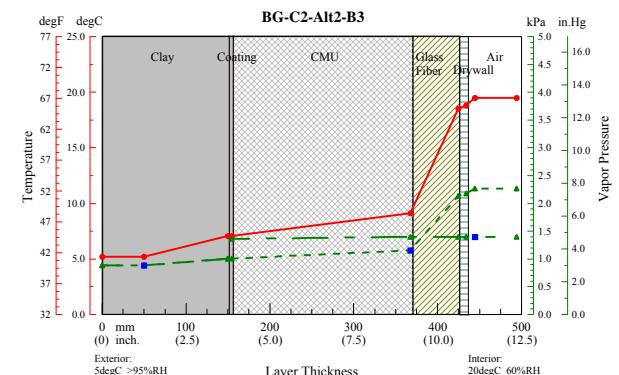


Figure C-174: Wall diagram of C2-Alt2-B3

Test cycle: **S2 – Alt2 (continued)**

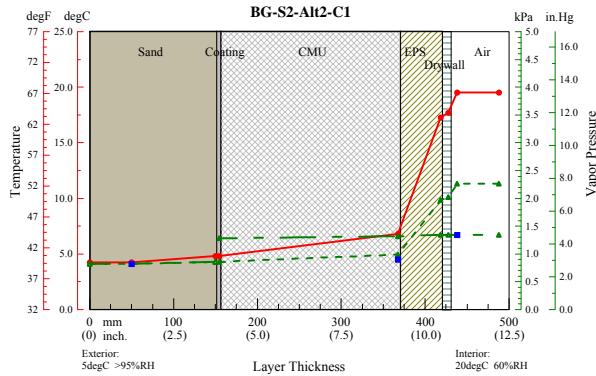


Figure C-175: Wall diagram of S2-Alt2-C1

Test cycle: **C2 – Alt2 (continued)**

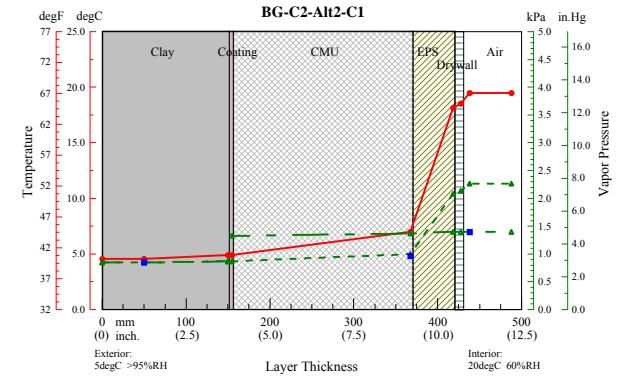


Figure C-176: Wall diagram of C2-Alt2-C1

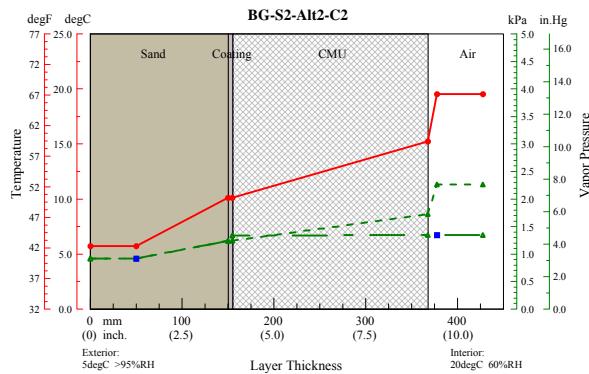


Figure C-177: Wall diagram of S2-Alt2-C2

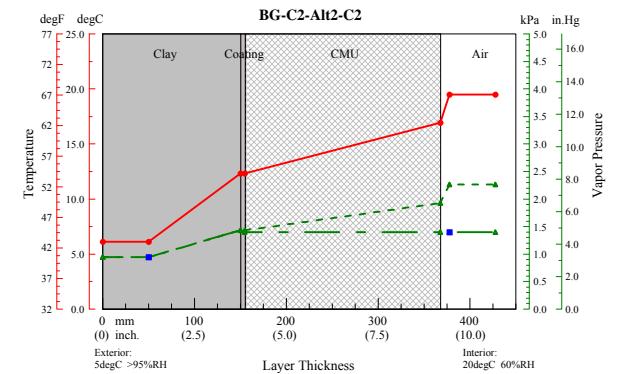


Figure C-178: Wall diagram of C2-Alt2-C2

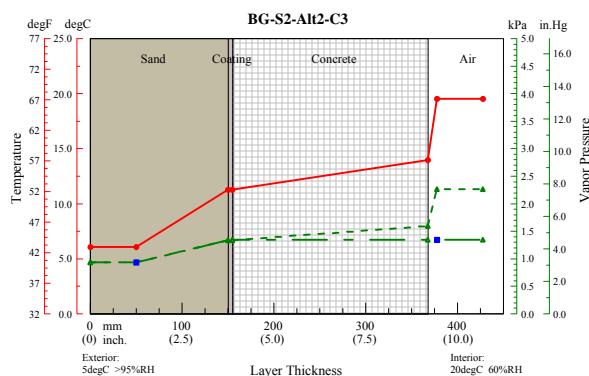


Figure C-179: Wall diagram of S2-Alt2-C3

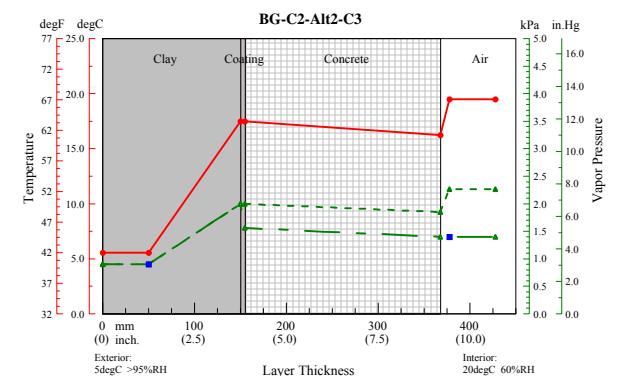


Figure C-180: Wall diagram of C2-Alt2-C3

Test cycle: **S2 – Alt3**

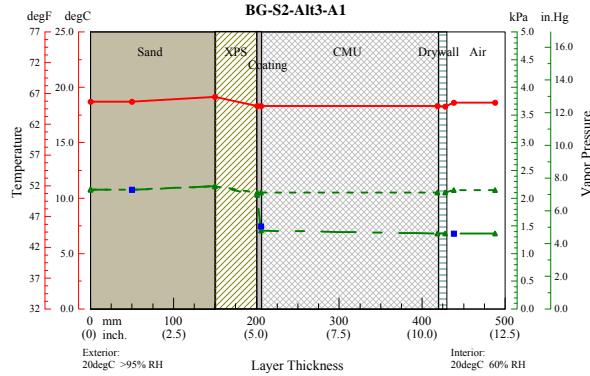


Figure C-181: Wall diagram of S2-Alt3-A1

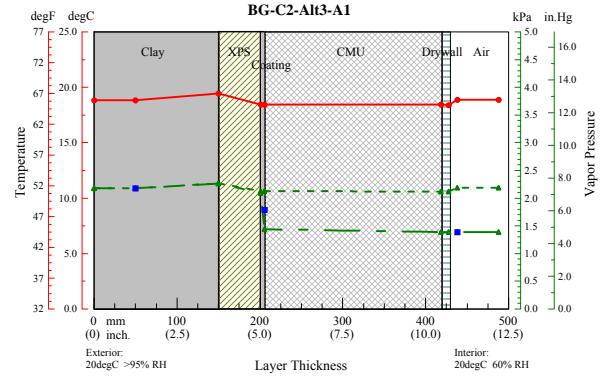


Figure C-182: Wall diagram of C2-Alt3-A1

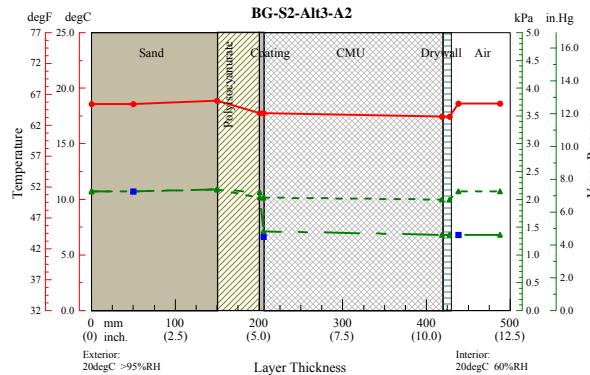


Figure C-183: Wall diagram of S2-Alt3-A2

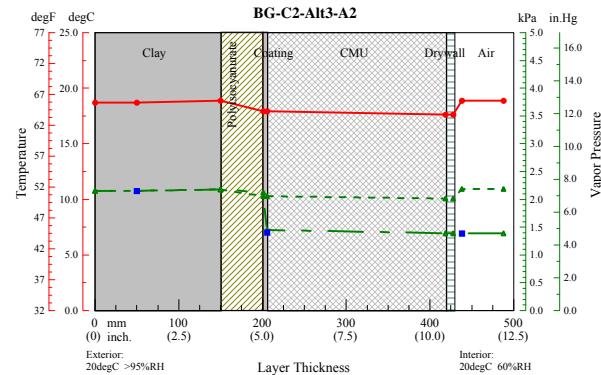


Figure C-184: Wall diagram of C2-Alt3-A2

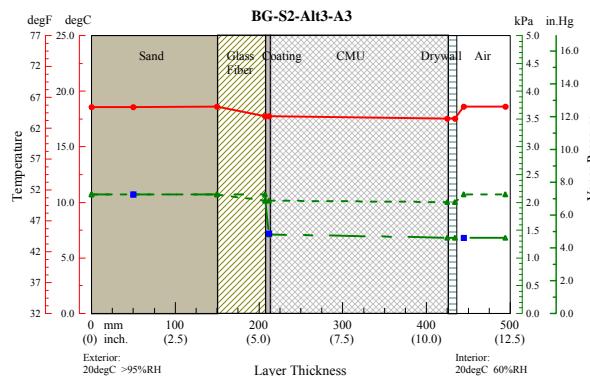


Figure C-185: Wall diagram of S2-Alt3-A3

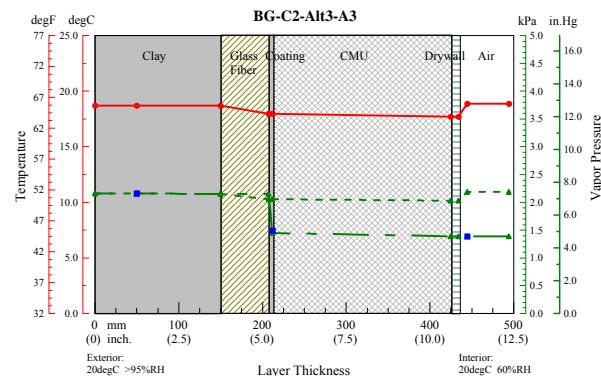


Figure C-186: Wall diagram of C2-Alt3-A3

Test cycle: **S2 – Alt3 (continued)**

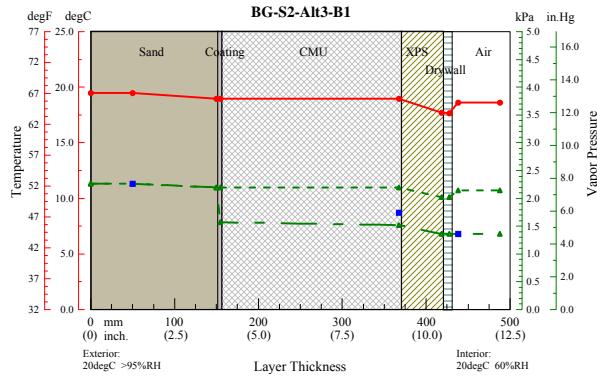


Figure C-187: Wall diagram of S2-Alt3-B1

Test cycle: **C2 – Alt3 (continued)**

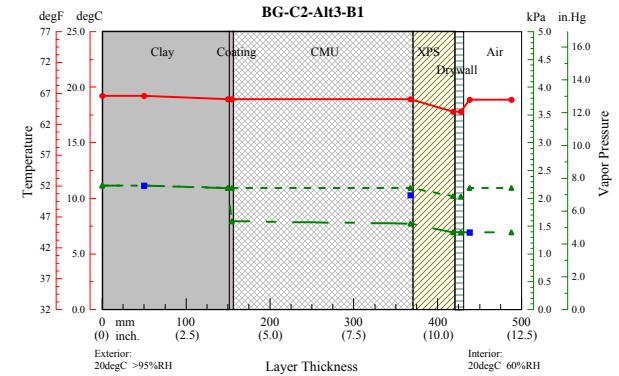


Figure C-188: Wall diagram of C2-Alt3-B1

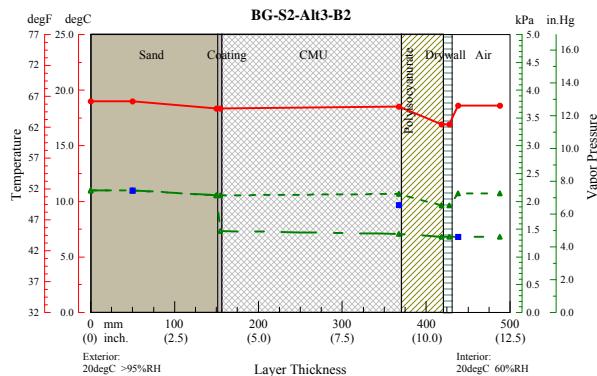


Figure C-189: Wall diagram of S2-Alt3-B2

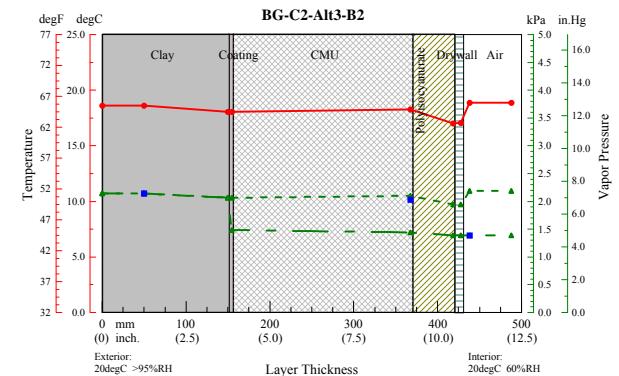


Figure C-190: Wall diagram of C2-Alt3-B2

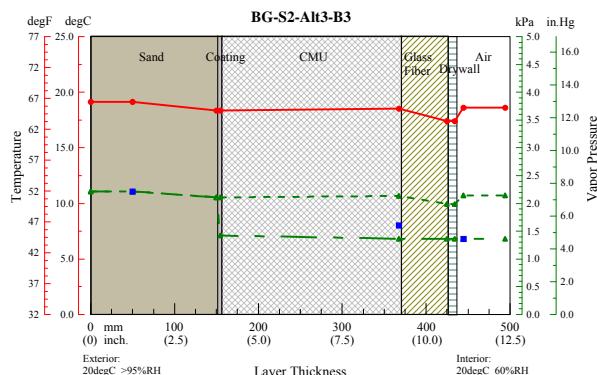


Figure C-191: Wall diagram of S2-Alt3-B3

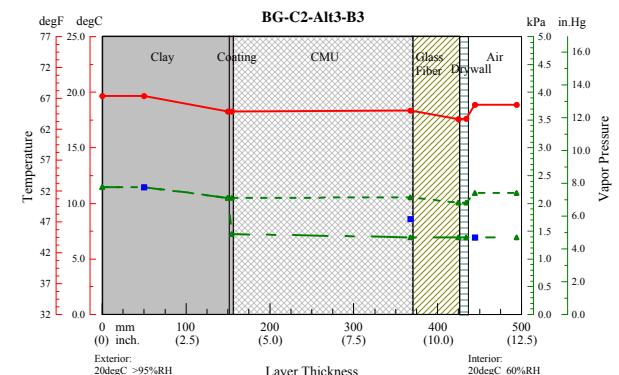


Figure C-192: Wall diagram of C2-Alt3-B3

Test cycle: **S2 – Alt3 (continued)**

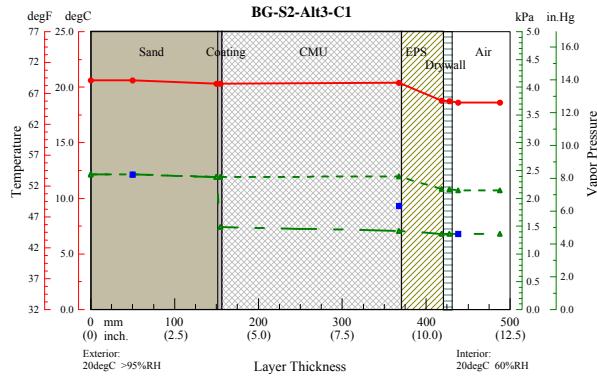


Figure C-193: Wall diagram of S2-Alt3-C1

Test cycle: **C2 – Alt3 (continued)**

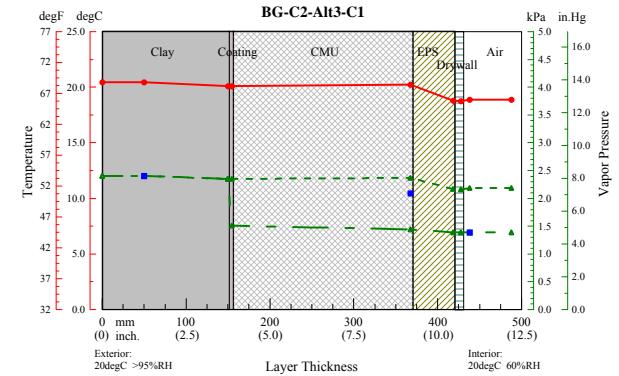


Figure C-194: Wall diagram of C2-Alt3-C1

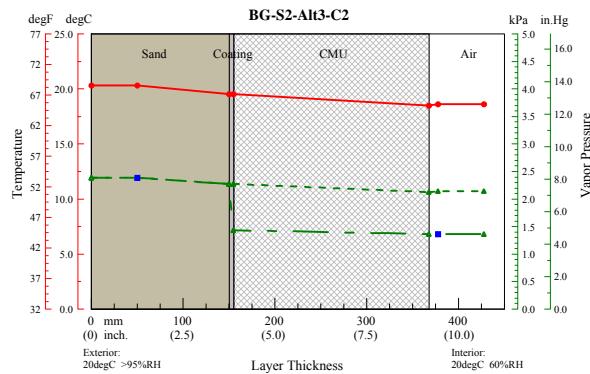


Figure C-195: Wall diagram of S2-Alt3-C2

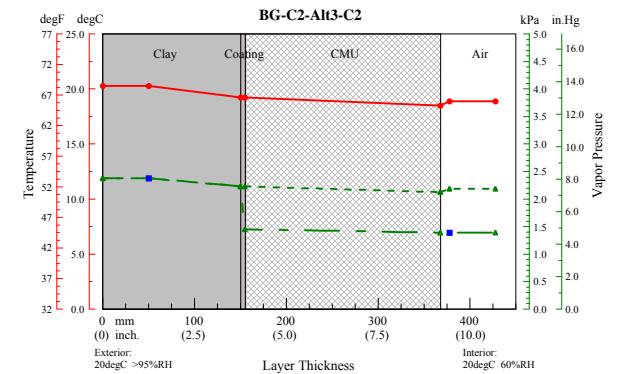


Figure C-196: Wall diagram of C2-Alt3-C2

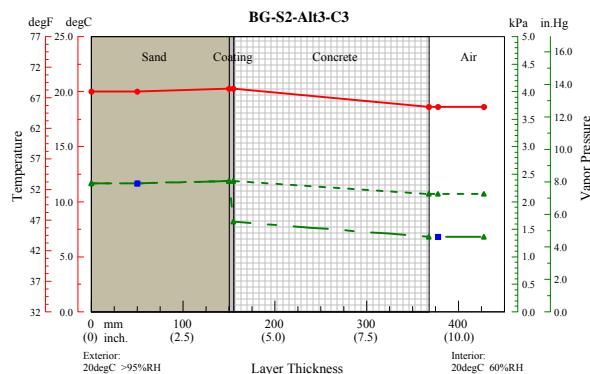


Figure C-197: Wall diagram of S2-Alt3-C3

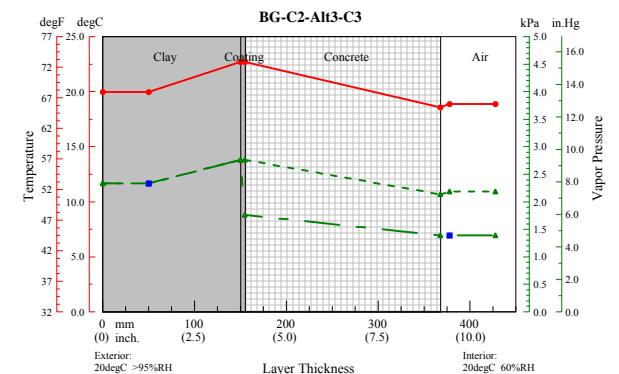


Figure C-198: Wall diagram of C2-Alt3-C3

Test cycle: **S2 – Alt4**

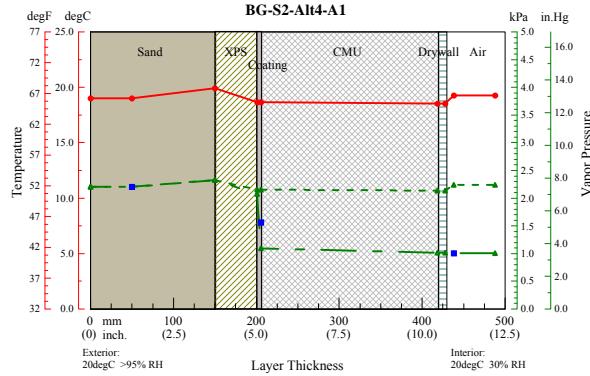


Figure C-199: Wall diagram of S2-Alt4-A1

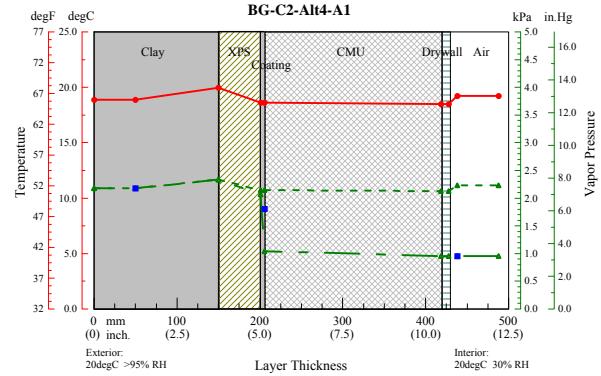


Figure C-200: Wall diagram of C2-Alt4-A1

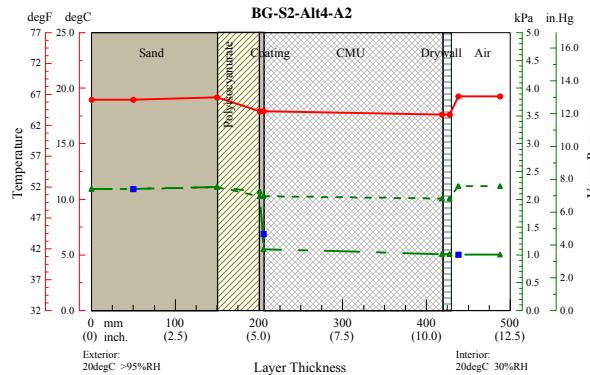


Figure C-201: Wall diagram of S2-Alt4-A2

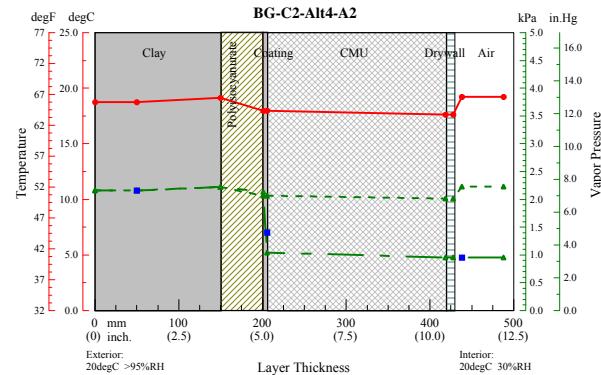


Figure C-202: Wall diagram of C2-Alt4-A2

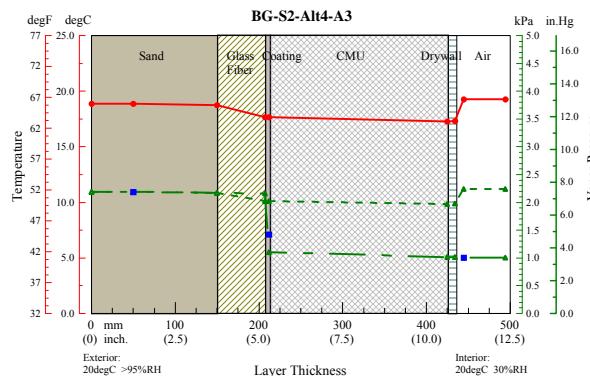


Figure C-203: Wall diagram of S2-Alt4-A3

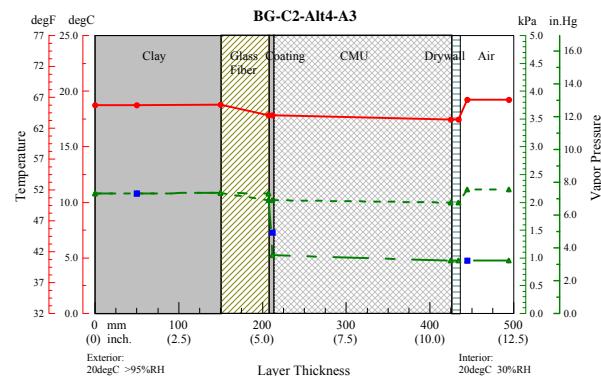


Figure C-204: Wall diagram of C2-Alt4-A3

Test cycle: **S2 – Alt4 (continued)**

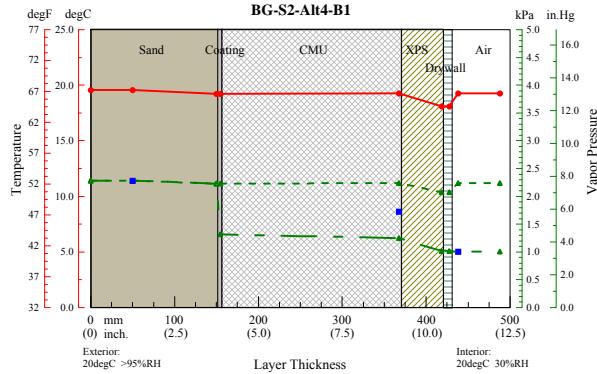


Figure C-205: Wall diagram of S2-Alt4-B1

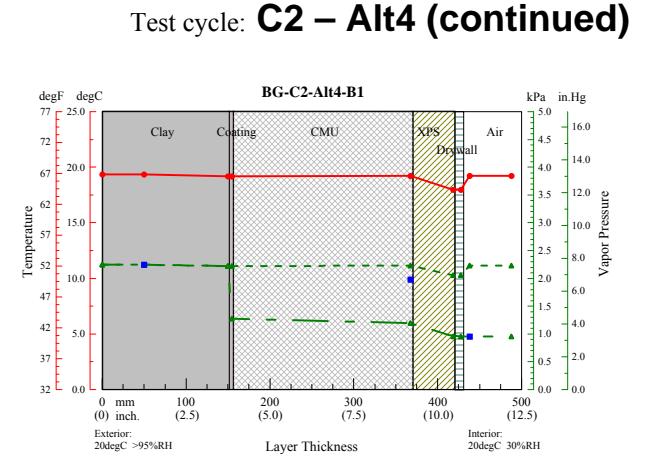


Figure C-206: Wall diagram of C2-Alt4-B1

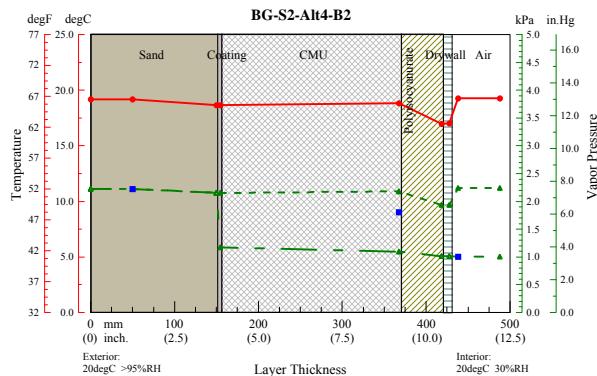


Figure C-207: Wall diagram of S2-Alt4-B2

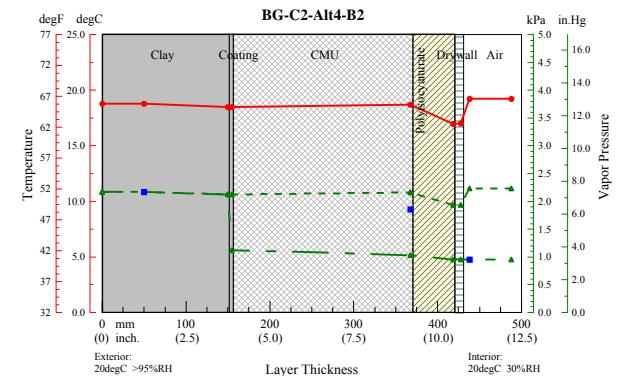


Figure C-208: Wall diagram of C2-Alt4-B2

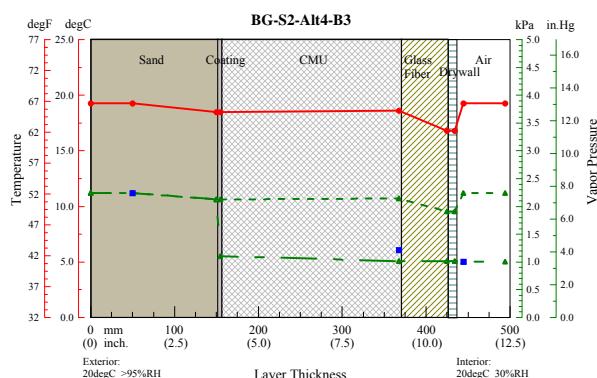


Figure C-209: Wall diagram of S2-Alt4-B3

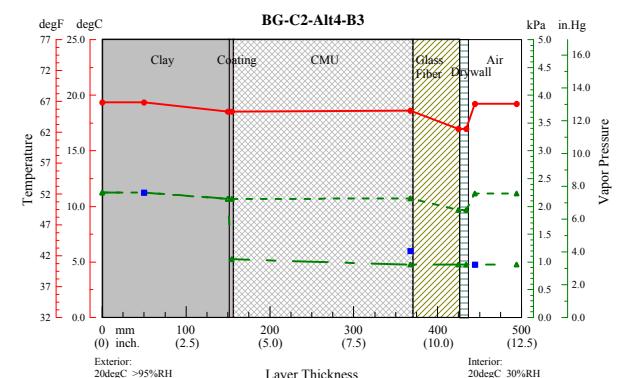


Figure C-210: Wall diagram of C2-Alt4-B3

Test cycle: **S2 – Alt4 (continued)**

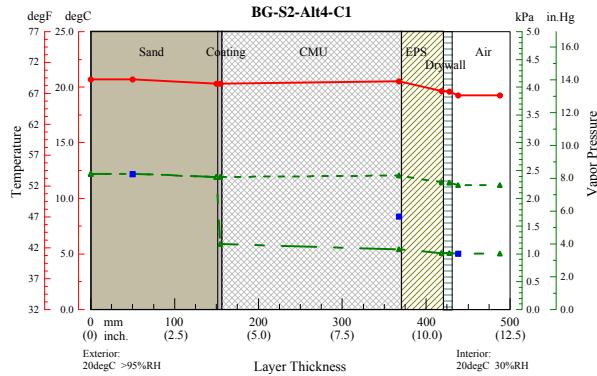


Figure C-211: Wall diagram of S2-Alt4-C1

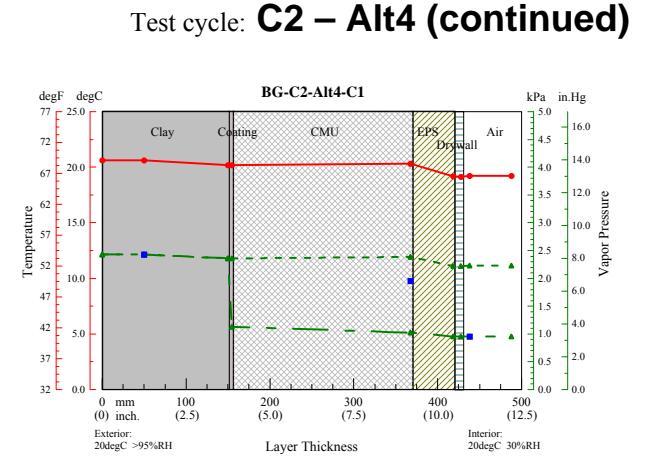


Figure C-212: Wall diagram of C2-Alt4-C1

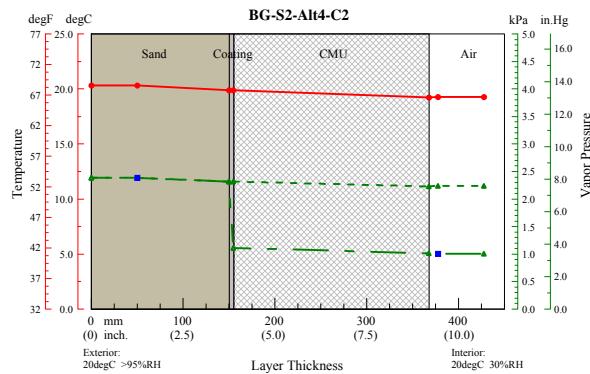


Figure C-213: Wall diagram of S2-Alt4-C2

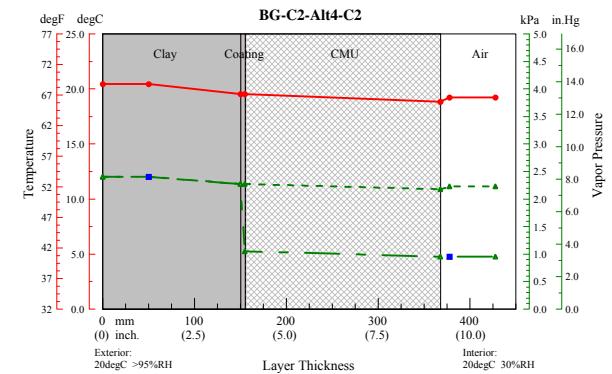
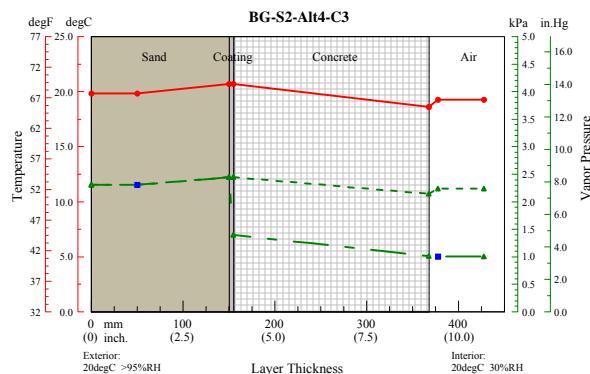


Figure C-214: Wall diagram of C2-Alt4-C2



F Figure C-215: Wall diagram of S2-Alt4-C3

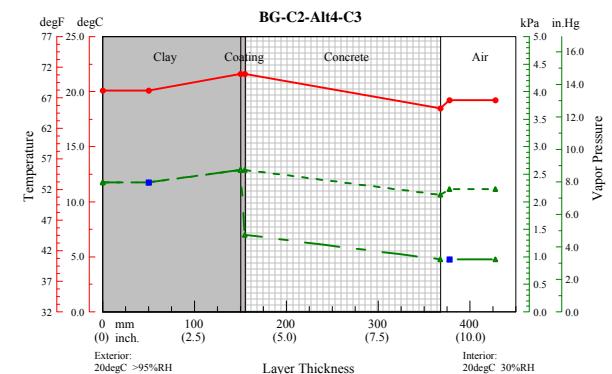


Figure C-216: Wall diagram of C2-Alt4-C3

Appendix D – Moisture content vs. relative humidity charts

The setup moisture content vs. relative humidity charts are summarized in appendix D.

The moisture content of the specimens of below-grade structure is shown below as follows:

5. Measurement series: S1 (Sand; no dampproofing)
 - 5.1. Test cycle: S1-Alt1 (cold climate)
 - 5.2. Test cycle: S1-Alt2 (cold climate)
 - 5.3. Test cycle: S1-Alt3 (cold climate)
 - 5.4. Test cycle: S1-Alt4 (cold climate)
 - 5.5. Test cycle: S1-Alt5 (mild climate)
 - 5.6. Test cycle: S1-Alt6 (mild climate)
 - 5.7. Test cycle: S1-Alt7 (mild climate)
 - 5.8. Test cycle: S1-Alt8 (mild climate)
6. Measurement series: C1 (Clay; no dampproofing)
 - 6.1. Test cycle: C1-Alt1 (cold climate)
 - 6.2. Test cycle: C1-Alt2 (cold climate)
 - 6.3. Test cycle: C1-Alt3 (cold climate)
 - 6.4. Test cycle: C1-Alt4 (cold climate)
 - 6.5. Test cycle: C1-Alt5 (mild climate)
 - 6.6. Test cycle: C1-Alt6 (mild climate)
 - 6.7. Test cycle: C1-Alt7 (mild climate)
 - 6.8. Test cycle: C1-Alt8 (mild climate)
7. Measurement series: S2 (Sand; with dampproofing)
 - 7.1. Test cycle: S2-Alt1 (cold climate)
 - 7.2. Test cycle: S2-Alt2 (cold climate)
 - 7.3. Test cycle: S2-Alt3 (mild climate)
 - 7.4. Test cycle: S2-Alt4 (mild climate)
8. Measurement series: C2 (Clay; with dampproofing)
 - 8.1. Test cycle: C2-Alt1 (cold climate)
 - 8.2. Test cycle: C2-Alt2 (cold climate)
 - 8.3. Test cycle: C2-Alt3 (mild climate)
 - 8.4. Test cycle: C2-Alt4 (mild climate)

Measurement series: **S1** (Sand; no dampproofing)

Test cycle: **S1 – Alt1 to Alt4** (cold climate)

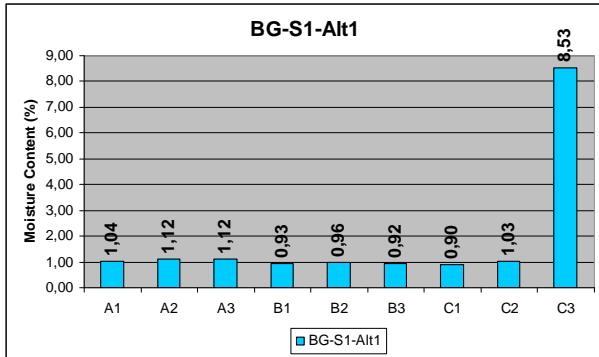


Figure D-1: Moisture contents of S1-Alt1

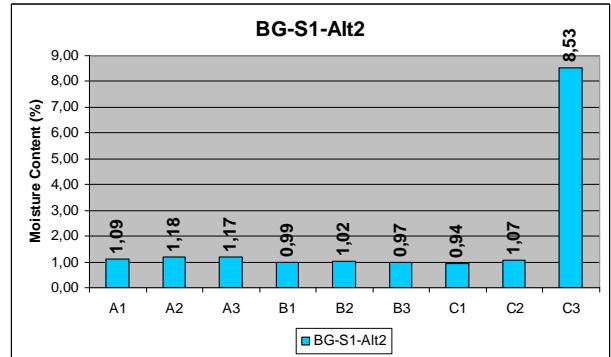


Figure D-2: Moisture contents of S1-Alt2

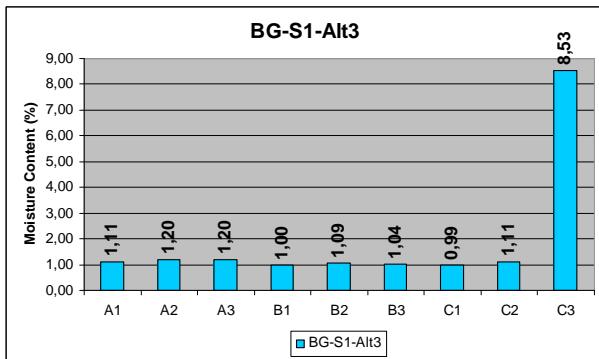


Figure D-3: Moisture contents of S1-Alt3

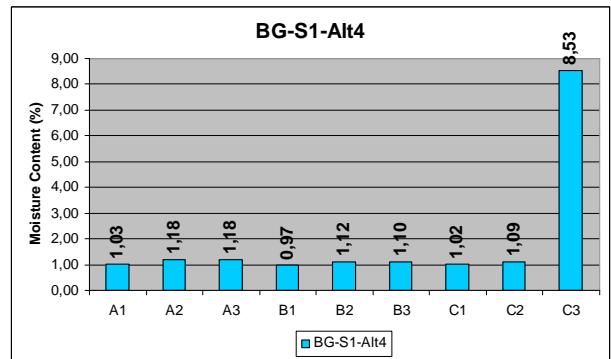


Figure D-4: Moisture contents of S1-Alt4

Measurement series: **S1** (Sand; no dampproofing) - continued

Test cycle: **S1 – Alt5 to Alt8** (mild climate)

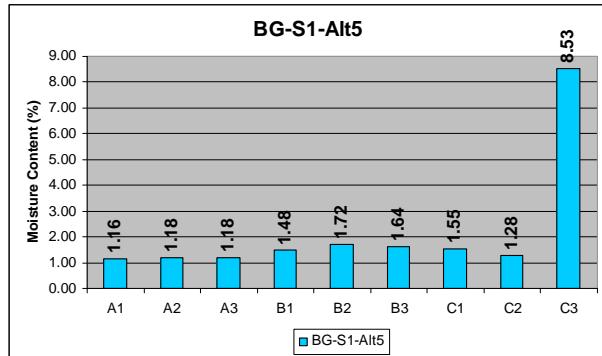


Figure D-5: Moisture contents of S1-Alt5

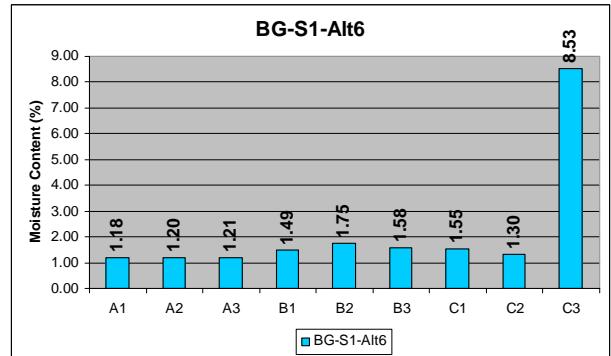


Figure D-6: Moisture contents of S1-Alt6

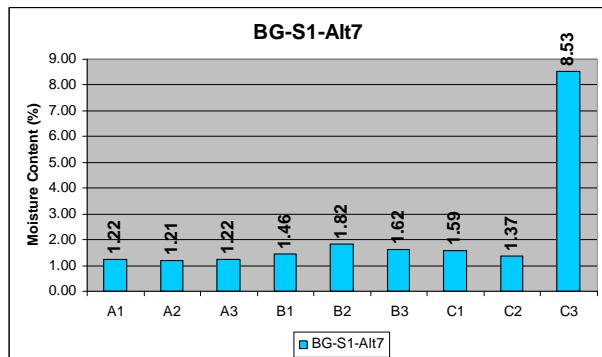


Figure D-7: Moisture contents of S1-Alt7

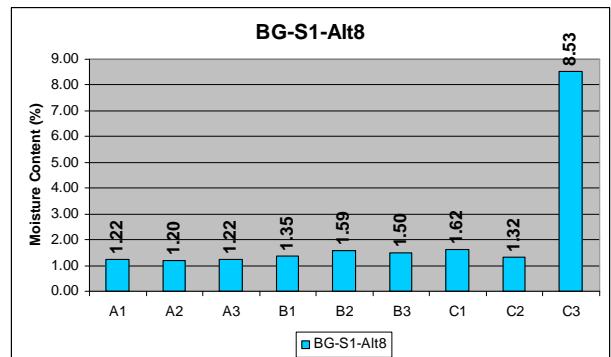


Figure D-8: Moisture contents of S1-Alt8

Measurement series: **C1 (Clay; no dampproofing)**

Test cycle: **C1 – Alt1 to Alt4 (cold climate)**

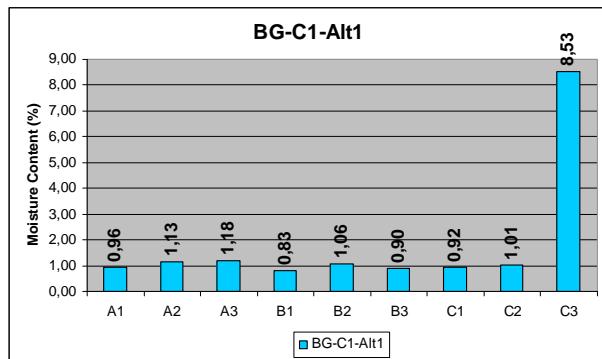


Figure D-9: Moisture contents of C1-Alt1

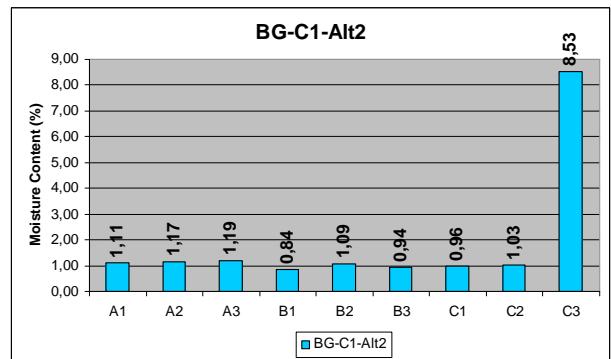


Figure D-10: Moisture contents of C1-Alt2

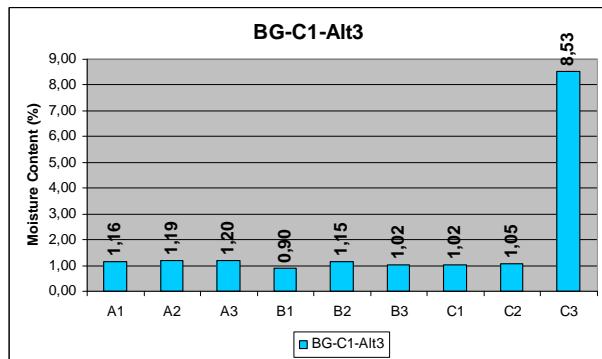


Figure D-11: Moisture contents of C1-Alt3

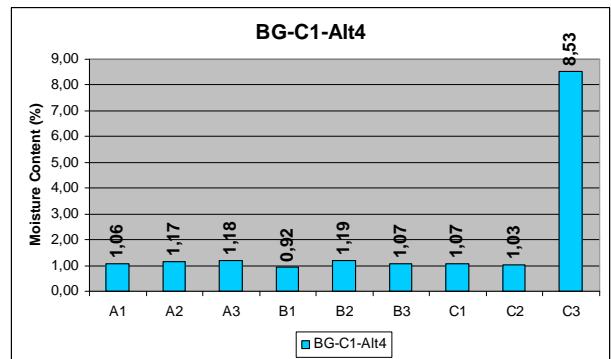


Figure D-12: Moisture contents of C1-Alt4

Measurement series: **C1 (Clay; no dampproofing)** - continued

Test cycle: **C1 – Alt5 to Alt8 (mild climate)**

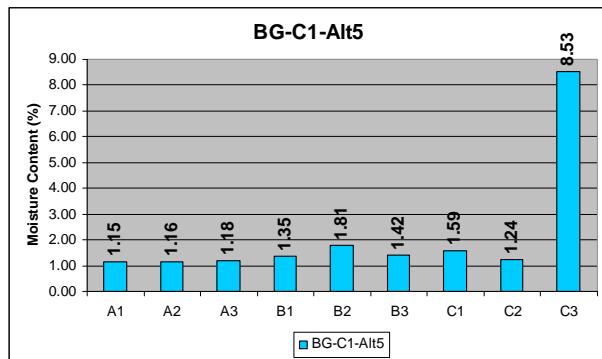


Figure D-13: Moisture contents of C1-Alt5

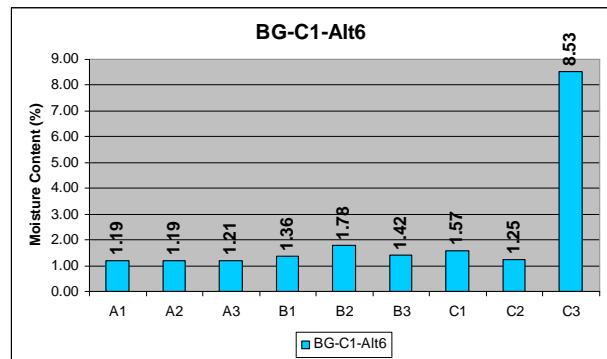


Figure D-14: Moisture contents of C1-Alt6

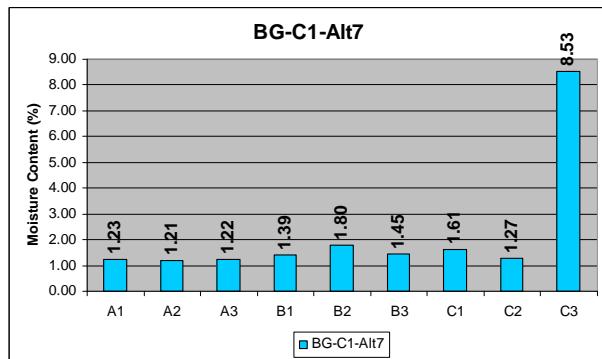


Figure D-15: Moisture contents of C1-Alt7

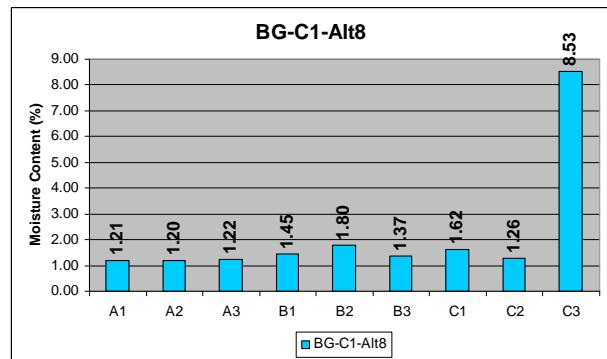


Figure D-16: Moisture contents of C1-Alt8

Measurement series: **S2 (Sand; with dampproofing)**

Test cycle: **S2 – Alt1 to Alt2 (cold climate)**

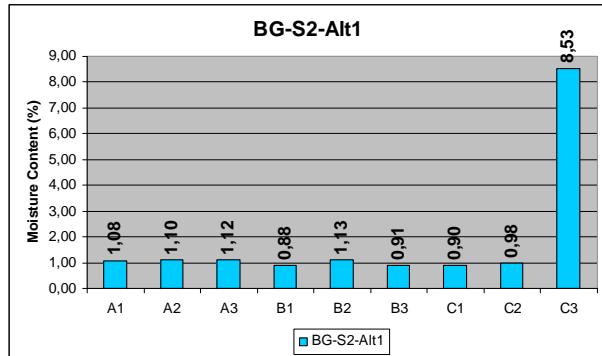


Figure D-17: Moisture contents of S2-Alt1

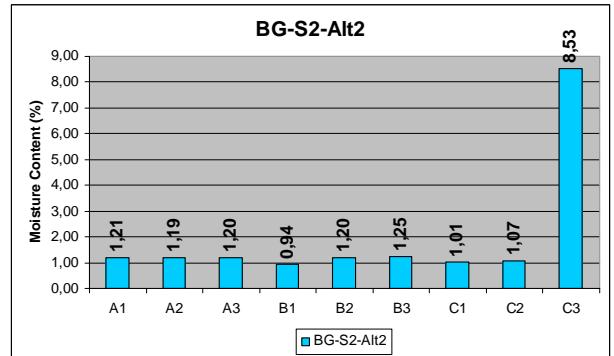


Figure D-18: Moisture contents of S2-Alt2

Test cycle: **S2 – Alt3 to Alt4 (mild climate)**

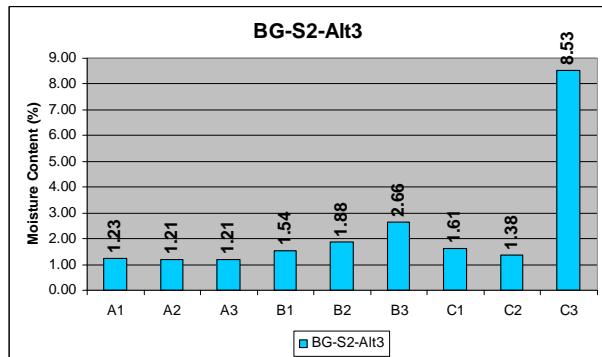


Figure D-19: Moisture contents of S2-Alt3

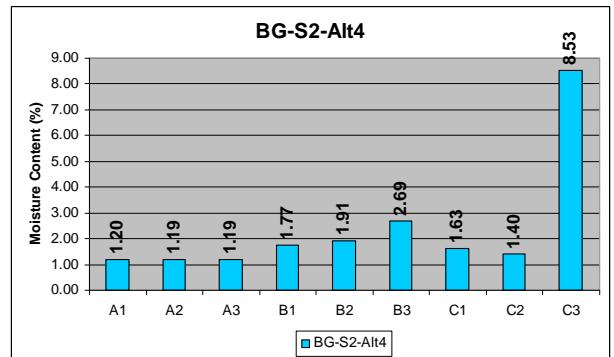


Figure D-20: Moisture contents of S2-Alt4

Measurement series: **C2 (Clay; with dampproofing)**

Test cycle: **C2 – Alt1 to Alt2 (cold climate)**

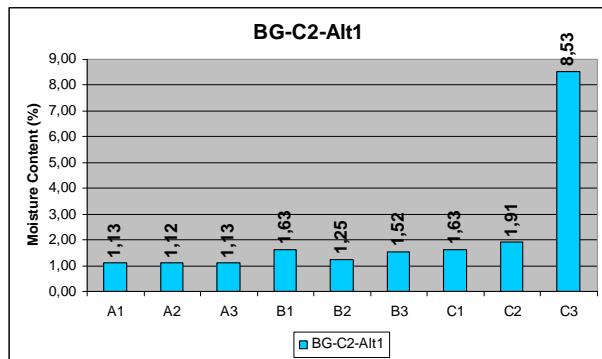


Figure D-21: Moisture contents of C2-Alt1

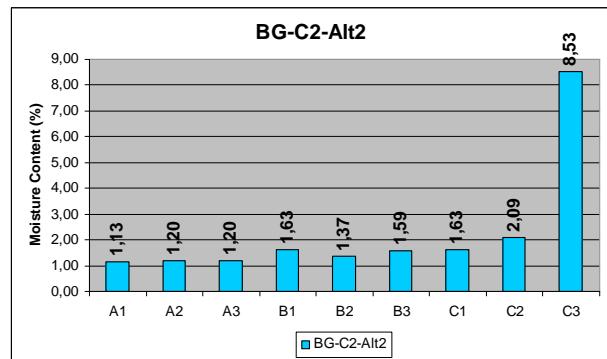


Figure D-22: Moisture contents of C2-Alt2

Test cycle: **C2 – Alt3 to Alt4 (mild climate)**

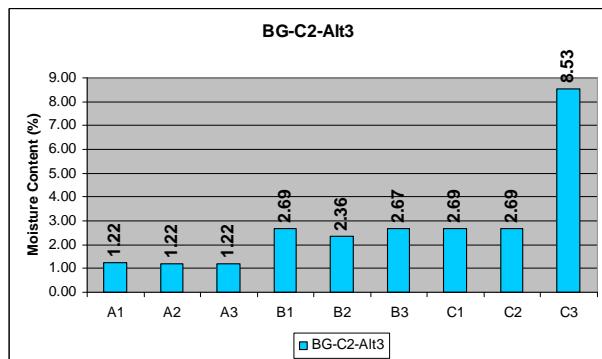


Figure D-23: Moisture contents of C2-Alt3

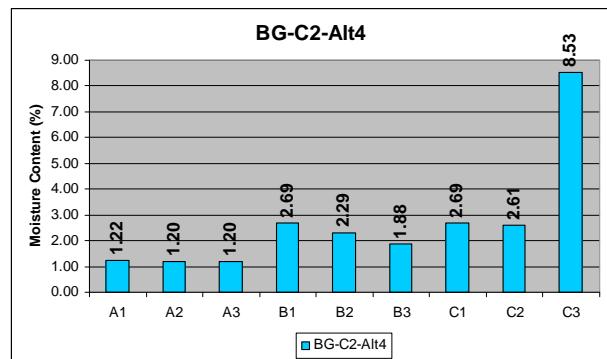


Figure D-24: Moisture contents of C2-Alt4